

CIVIL ENGINEERING • SURVEYING • LANDSCAPE ARCHITECTURE

# Town of Raymond Preliminary Major Subdivision Application

For:

Raymond Cape Subdivision 78 Raymond Cape Road Raymond, Maine

> Applicant: Brandon Chase 15 Washington Court Naples, Maine 04055

> > **Prepared by:**

Sebago Technics, Inc. 75 John Roberts Road, Suite 4A South Portland, Maine 04106

# March 2022

21397

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March 9, 2022 21397

Alex Sirois, Code Enforcement Officer Town of Raymond 401 Webbs Mills Road Raymond, ME 04071

#### Major Subdivision Application Raymond Cape Subdivision Raymond Cape Road, Raymond, ME

Dear Alex:

On behalf of our client, Brandon Chase, we are submitting a Major Subdivision Application for a proposed 12-lot subdivision adjacent to Raymond Cape Road. The applicant is proposing to subdivide an approximate 37-acre parcel of undeveloped land that slopes up from Raymond Cape Road. Pursuant to the sketch plan that was reviewed by the Planning Board on December 8, 2021 and the site walk on December 9, 2021, the applicant is proposing an open space cluster subdivision.

We have prepared the enclosed Preliminary Subdivision application, plans and attachments for the subdivision of a single-family development. Of this acreage, 20.06 acres will be area that is set aside for the 12 lots with 14.85 acres proposed in two open space tracts. The balance of the parcel will be utilized for the site access/right-of-way for the development. The property exists with the Limited Residential-Recreational II Zoning District (LRR2) with a small portion of the site in the Resource Protection District (RP).

**Site Location:** The physical address of the property is Raymond Cape Road one half mile south of Hawthorne Road. The property is further identified on the Town's Tax Maps as Map 4, Lot 9. The land is currently unimproved and consists woodlands and wetlands and generally slopes from Raymond Cape to the northeast/north as shown on the existing conditions plan.

**Natural Resources:** On behalf of the applicant, Sebago Technics, Inc. (Sebago) has requested site review for historical/archaeological, botanical, wildlife and fisheries resources from the applicable state agencies. Copies of the letters of inquiry or responses are included in this submittal package. Responses received after the preliminary subdivision plan submission will be included in the final subdivision plan submission. In addition, the site has been reviewed by a Sebago Technics Wetland Scientist for delineation of the jurisdictional wetlands and the excavation of test pits were overseen and reviewed by a licensed Sebago Technics Site Evaluator for determination of suitable soils for subsurface systems.

**Utilities:** The proposed single family lots will be served by individual subsurface wastewater disposal systems and individual wells. Electric and telecommunications will be installed underground and extended from available infrastructure the Raymond Cape Road.

Alex Sirois 21397

**Regulatory Permitting:** The applicant proposes to construct approximately 2,000 LF of roadway for a Minor Street from Raymond Cape Road to rear parcel line with two t-turn around locations. The proposed development of the roadway will include approximately 0.97 acres of new impervious area with a total developed area of 3.27 acres. The applicant is proposing to only develop the roadway and sell the lots for development. Accordingly, the project will need to meet the Maine Department of Environmental Protection (MDEP) stormwater general standards for the right-of-way development; because Sebago Lake is not considered to be severely blooming and the roadway area to be developed, the general standards will be used to satisfy the phosphorus standards. Concurrently, with the Town submission, a Maine stormwater permit application will be submitted to MDEP. The site will also be reviewed under MDEP stormwater standards that incorporate the Maine Construction General Permit (MCGP) review. Copy of the MDEP approval will be provided to the Town upon receipt.

The proposed alignment for the roadway and development for the lots are such that there will be no wetland impacts. Therefore, no submission for permits/approvals under the provisions of the MDEP Natural Resources Protection Act (NRPA) or the U.S. Army Corps of Engineers (ACOE) is anticipated.

**Applicable Standards:** Please refer to the attached narrative demonstrating compliance with the applicable subdivision standards.

<u>Waivers</u>: As part of the submission for subdivision approval, it is requested to waive the requirement for Article 13 – Open Space Subdivisions, c. General Requirements 4. Space Standards, paragraph c: for the dedicated open space tracts to meet or exceed the reduction in lot size for an open space cluster subdivision; the difference for the required area is 1.09 acres. This request is being made because of the substantial area of wetlands and wetland buffers that will be retained on individual lots

*Closure:* On behalf of Mr. Chase, we look forward to working with the staff and Planning Board to permit this project. As you consider the application, please contact us if you have any questions.

Please review and schedule this request for consideration by the Planning Board at the earliest possible meeting date. Thank you for your assistance relative to these requests.

Sincerely,

SEBAGO TECHNICS, INC.

Robert A. McSorley, P.E. Senior Project Manager

RAM:sn

cc. Brandon Chase

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#### Town of Raymond Subdivision Review Requirements Raymond Cape Subdivision

#### **Article 9 - General Requirements**

- Conformity with Comprehensive Plan The project is consistent with the Town's Comprehensive relative to Natural Resources; the project has been designed to avoid wetland impacts and preserve open areas. Relative to housing, the project proposes the development of a cluster subdivision which promotes the preservation of open space. Furthermore, the project has been designed to comply with the development regulations for the Town of Raymond, coordination with the appropriate state agencies relative to historical properties, natural communities and wildlife as well as meet the state stormwater standards.
- 2. Relationship to Community Services The applicant shall complete the roadway construction and stabilization to first lift of pavement, construction of the roadway t-turnarounds, construction and stabilization of the stormwater systems including roadside swales, conveyance culverts for the preservation of drainage ways and the installation of stabilization for disturbed areas and slopes prior to the sale of lots. The applicant is proposing the construction of a Minor Town Street and is intending to dedicate the roadway to the Town. Until the Minor Street is accepted by the Town, the applicant shall be responsible for all maintenance and repairs including snow removal and solid waste removal. The stormwater systems will be maintained by the association of the subdivision with rights to the Town to maintain as necessary.
- 3. Retention of Proposed Public Sites and Open Spaces The project proposes 14.85 acres of open retainage in two specific tracts which comprise 39.8% of the total property area. In addition, wetlands and buffers have been preserved on the individual lots beyond the areas of the open space tracts. The project has sought the review by the State Preservation Office which has indicated that no historical resources have been identified for the property. The property does not contain any public lands or trail ways.
- 4. Preservation of Natural and Historic Features The roadway for the project has been designed to minimize cuts and fills and to avoid any impacts to the wetlands on the property. In addition, the project layout and expected lot development comprise less than 25% of the uplands that surround the on-site wetlands.
- 5. Traffic Sight Distance Traffic site distance was reviewed for the project along the Raymond Cape Road; a memo is submitted as part of this application that indicates compliance with the standard.
- 6. Conformance to Shoreland Zoning The project has been designed to meet the requirements of an open space cluster subdivision within the Limited Residential-Recreational II Zoning District (LRR2). The stormwater Best Management Practices (BMP's) have been designed in accordance with Maine Department of Environmental Protection stormwater requirements to meet the phosphorus standards for the developments.
- 7. Easements for Natural Drainage Ways Culverts have been incorporated into the design and sized to provide for conveyance through the project.

- 8. Net Residential Density The property is in the LRR2 Zoning District which requires 3 acres/unit of development. A net residential calculation for the property was completed by subtracting the rights-of-way, steep slopes, poor soils/wetlands and resources protection areas from the gross acreage for the property resulting in 30.56 net acres. No floodplains exist on the property and surface water bodies were included in the area for wetlands. Because the applicant is proposing an open space cluster subdivision the net area was increased by 20% and divided by allowable density resulting in 12.22 od 12 units.
- 9. Lots Lots will be developed to provide adequate off-street parking for residential dwellings. Lots that have frontage on Raymond Cape Road will have access from the proposed roadway for the project. The lots will meet the minimum 1 ½ acre size for lots within an open space cluster subdivision and no lots are of a flag lot configuration. Test pits have been completed to confirm adequate soils/locations for subsurface wastewater disposal systems (SSWDS). Based upon the lot size, there is adequate suitable for the placement of wells and for SSWDS and meet the applicable setback requirements.
- 10. Utilities As stated in the cover letter above, the proposed single family lots will be served by individual subsurface wastewater disposal systems and individual wells. Electric and telecommunications will be installed underground and extended from available infrastructure the Raymond Cape Road.
- 11. Additional Requirements The layout of the subdivision is such that adequate buffering of adjacent properties is provided to minimize noise pollution form the development. The fact that the property is an open space cluster subdivision no further subdivision is permitted.
- 12. Required Improvements The design of the proposed subdivision provides for the required improvements including monuments, street signs, streets and storm drainage. As stated above, the individual wells and SSWDS will be provided on each lot.
- 13. Impact on Ground Water Based upon the number of test pits performed for the review of SSWDS, additional test pits were performed to create a soils map for the property. This soils map is the basis for the stormwater pre- and post- design plans. In addition, a Class 'C' Medium High Intensity Soil Survey Report has been prepared. Based upon the size of the proposed lots, locations for proposed systems the fact that the SSWDS will be individual systems and not a community disposal, the resulting nitrate plumes form the SSWDS are not expected to extend beyond the boundary of the project. Furthermore, sufficient lot area exists to provide adequate separate between proposed wells and SSWDS. In addition, review of wells within the vicinity of the project indicates that most of the permitted wells have significant capacity (well yield).
- 14. Phosphorous Control As stated above, the subdivision has been designed in accordance with Maine Department of Environmental Protection stormwater requirements to meet the phosphorus standards for the developments.

#### **ARTICLE 10 - DESIGN STANDARDS**

1. Monuments – The proposed subdivision plan indicates the installation of property monuments to comply with the Town requirements.

- 2. Street Signs A proposed street name for the project will be provided to the Town for review and approval prior to the Final Subdivision Plan submission.
- 3. Streets Proposed street will be classified as a Minor Street. The street has been designed based upon the requirements of the Reymond Street Ordinance. The grade of the street has been designed to match existing grade and to minimize/eliminate impacts to on-site wetlands. As depicted on the sketch plan submitted to the Planning Board for review, the development proposes a dead-end street of approximately 1970 If with two t-turn arounds to provide access at approximately the midpoint of the roadway as well as the end of the roadway. A waiver for the length of the street is requested with this application.
- 4. Driveway Construction Driveway will be designed with individual lot construction to provide for a culvert for roadside drainage and to minimize runoff into the proposed street of the subdivision.
- 5. Sidewalks The proposed street will be a minor street in the LRR2 and will not have sidewalks.
- 6. Water Supply Per the sketch plan submission for the project, the proposed residential dwellings will have residential fire suppression systems as part of the building construction. Wells will be constructed for each lot that meet the Maine Department of Heath and Human Services (MDHHS) requirements.
- Sewage Disposal As stated above, test pits for the proposed lots were reviewed and evaluated by a Licensed Site Evaluator. Final design of the systems will be by a Licensed Site Evaluator to meet MDHHS requirements including required setbacks.
- 8. Surface Drainage A part of the submission for this subdivision, a Stormwater Management Report and plan are included to meet the requirements for a drainage plan and to meet the requirements of the Maine Stormwater Law. Included in this design are construction and stormwater BMP's including stabilization to prevent soil erosion for the development.



WS\_\_\_Entered\_\_Completed\_\_\_

# Land Development Permit Application

Permit#	January 10, 2007 re	vision		
			Issue Date	
TYPE OF DEVELOP	'MENT:		RE ID	
Minor Subdivision		ſ		
X Major Subdivision		For Toy	n of Raymond use only:	
Minor Conditional		Date Re		
Major Conditional	Use	Time Re		
Mobile Home Park Campground			ed by	
APPLICATION INFO	ORMATION:			
Development Name:	Raymond Cape Subdivision			
Development Address:	Raymond Cape Road, Raymond, M	E 04071		
Property Owner: Owner Address:	Brandon Chase			
Owner Address.	P.O. Box 37	0.1071		
	Raymond ME	04071		
Applicant:	Brandon Chase			
Applicant Address:	P.O. Box 37			
	Raymond ME	04071		
Applicant Telephone:	(207) 807-6576 Email: bchase	02@yahoo.	com	
ls applicant a corporati	on? Ores Sono If yes, licensed	in which state	) *	
	the corporation license is outside of Maine, p			
	Agent: Sebago Technics, Inc.			
Agent Address:	75 John Roberts Road, Suite 4A			
Agent Address.		4106		
Agent Telephone:	(207) 200-2074 Email rmcs	sorley@seba	agotechnics.com	
Design Professional:	Robert McSorley, P.E.	itle: Senior F	Project Manager	
Preparers Address:	See Agent, Above		<u> </u>	
	ME			
Preparers Telephone:	(207) 200-2074 Registration M	E 8588		
	person to receive all correspondence with	regard to thi	s application:	
	Sebago Technics, Inc. c/o Robert N	1.00 m	and the second	
Application Contact: Contact Address:	75 John Roberts Road, Suite 4A			
Contact Address:		106		page 1 of 3
Contact Telephone:	(207) 200-2074 Email: rmcsorle		echnics.com	

Permit#			Issue Date
LAND INFORM	1ATION:		
1. The prop	osal is located on which City Tax Map/Lot #(s)	? _4	29
2. How larg	e is the subject property (in acres or square feet	)? 37.33 +/-	- Ø Acres O Sq Ft
3. What is t	he current zoning of property to be developed?	LLR2	
4. What are	the existing use(s) of the subject property? $U_{i}$	nimproved, va	acant
5. What wa	ter bodies does the parcel include? Not Appl	icable	
6. Is any po O Yes	rtion of the property within 250' of the normal $\bigotimes$ No or in Stream Protection? Yes		of a pond, river, or salt water body?
	rtion of the property within a special flood haza nent Agency (FEMA): <u>O Yes &amp; No</u>	urd area as identi	fied by the Federal Emergency
	al interest does the applicant have in the subject rship $\bigcirc$ option $\bigcirc$ purchase and sales contributed by the set of the		ach evidence thereof.)
9. What leg	al interest does the applicant have in any abutti	ng property?	None
	Please attach a list of the owners of all prop	erties within 500	0' of the subject property.
10. When wa	is the last time that the subject property was sub	divided? Pri	or to 1993
11 What wa	s the nature of the last subdivision? O building	ng units   🗴 div	ision of land
	f property is in the following classifications for Growth O Farm Use O Open Space	property tax ass	sessment purposes:
<i>NOTE:</i> Contact the City Assessor prior to receiving subdivision approval or change of use approval to determine if there will be a withdrawal penalty from the above programs.			
DEVELOPMEN	T INFORMATION:		
13. Proposed	use(s) of development:		
Number	of existing lots <u>1</u> of existing buildings <u>0</u> type of existing units <u>0</u>	No. of building	to be developed: $12$ gs to be developed: $0$ its to be developed: $0$
What is t	he proposed <i>building gross floor area</i> ? he proposed <i>impervious surface area</i> ? he proposed <i>area of site disturbance</i> ?	0 42,240 142,505	juare feet juare feet res
16. Does this	development require extension of public infras	structure: O	Yes 🐼 No
17. Estimated	d cost for public infrastructure improvements:	\$600,000.0	0
S Indiv O Centr O Conn	nethod of water supply for the proposed develo idual wells al well with distribution lines ection to public water system (Indicate)	pment: Other	
			page 2 of 3
Permit# LD-1	0-4763		Issue Date

19.	Identify method of sewage disposal for the proposed dev Individual septic systems Central on-site disposal with distribution lines Connection to public sewer system O ther (indicate)	velopment: Other	
20.	Identify method of fire protection for the proposed deve O Hydrants connected to the public water system O Dry hydrants located on existing, pond or water body O Existing fire pond O Other (indicate:)	y	sprinklers, well-served
21.	Does the applicant propose to dedicate to the public any <u>O Yes</u> <u>No</u> If answered yes, please sp Description of Street(s) Description of Recreation Area(s) Description of Common Land(s)	ecify all applica	
22.	Indicate the nature of any restrictive covenants to be pla	aced in the deeds	
23.	Does the applicant intend to request waivers of any of the O Yes No If yes, please list them and sta	he submission re te reasons for the	quirements? request)

To the best of my knowledge, all of the information submitted in this application is true and correct.

Signature of Applicant's Authorized Agent

Approved by

3/9/22 Date Date

page 3 of 3

Brandon Chase P.O. Box 37 Raymond, ME 04071

March 9, 2022

Planning Board Town of Raymond 401 Webbs Mills Rd Raymond, Maine 04071

Re: Raymond Cape Subdivision

To Whom It Concern:

I hereby authorize Sebago Technics, Inc. to act as my agent for a subdivision submission to the Town of Raymond. If you have any questions relative to this authorization, do not hesitate to contact me.

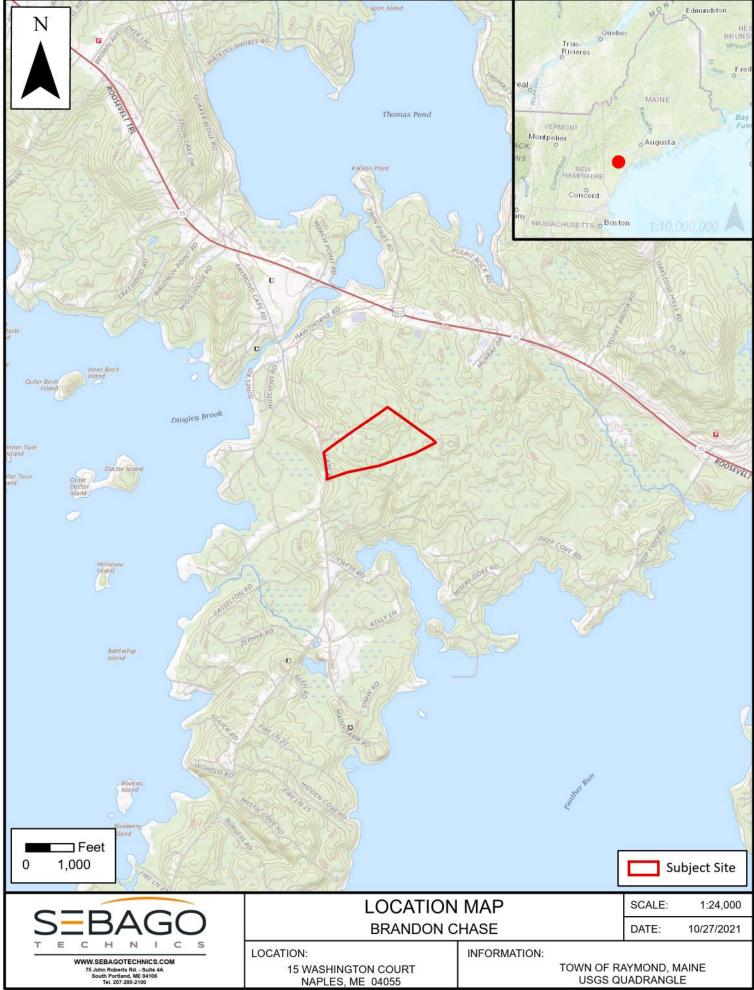
Sincerely, Brandon Chase

# <u>Exhibit 1</u>

**Location Maps** 

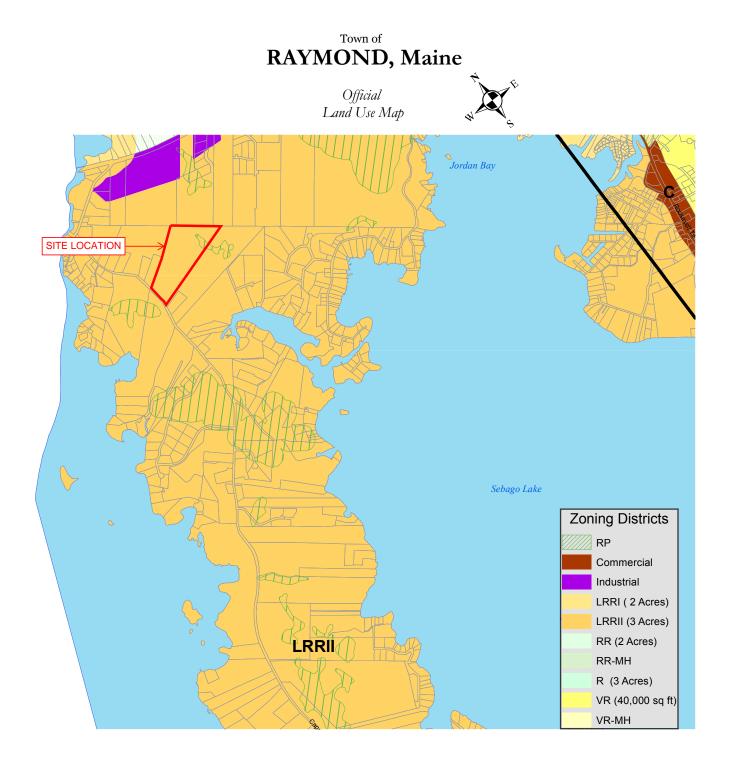
#### EXHIBIT 1: LOCATION MAPS

Reference is made to the USGS Site Location Map and the Town of Raymond Zoning Map excerpt included in this section. Per the official Land Use and Zoning Map, the Applicant's property is located with the Limited Residential-Recreation District II (LLR2); additionally, a portion of the parcel is located within the Resource Protection Zone. The RP will not be impacted as part of this project.



Location Map, 21397.aprx

Project Number: 21397



# Exhibit 2

## Abutter List and Tax Map

#### EXHIBIT 2: ABUTTER LIST AND TAX MAP

As required, we have included a 500-foot radius abutter list and accompanying tax map for Planning Board reference.

Map/Lot: 4-30-A00 GOAN, JENNIFER PO BOX 145 RAYMOND, ME 04071

Map/Lot: 4-28-B00 FRAITES, JOHN R FRAITES, DENISE L 359 S DOWNS WAY FORT MILL, SC 29708

Map/Lot: 4-28-0 MARSH, ROBERT JR & COLLEEN c/o GEORGE & KAREN MOTTA 34 CAPE ROAD RAYMOND, ME 04071

Map/Lot: 4-20-0 SABRE CORP PO BOX 134 SOUTH CASCO , ME 04077 Map/Lot: 3-69-0 HARRISON, ANNE S & WILLIAM B c/o PRIVATE MANAGEMENT SERVICES INC 23 OLD KINGS HIGHWAY S, STE 200 DARIEN, CT 06831

> Map/Lot: 4-28-A00 FOURQUET, VERONICA PO BOX 1125 RAYMOND, ME 04071

Map/Lot: 4-18-0 MARTIN, RICHARD N MARTIN, CYNTHIA 8 RIVER ROAD NAPLES, ME 04055

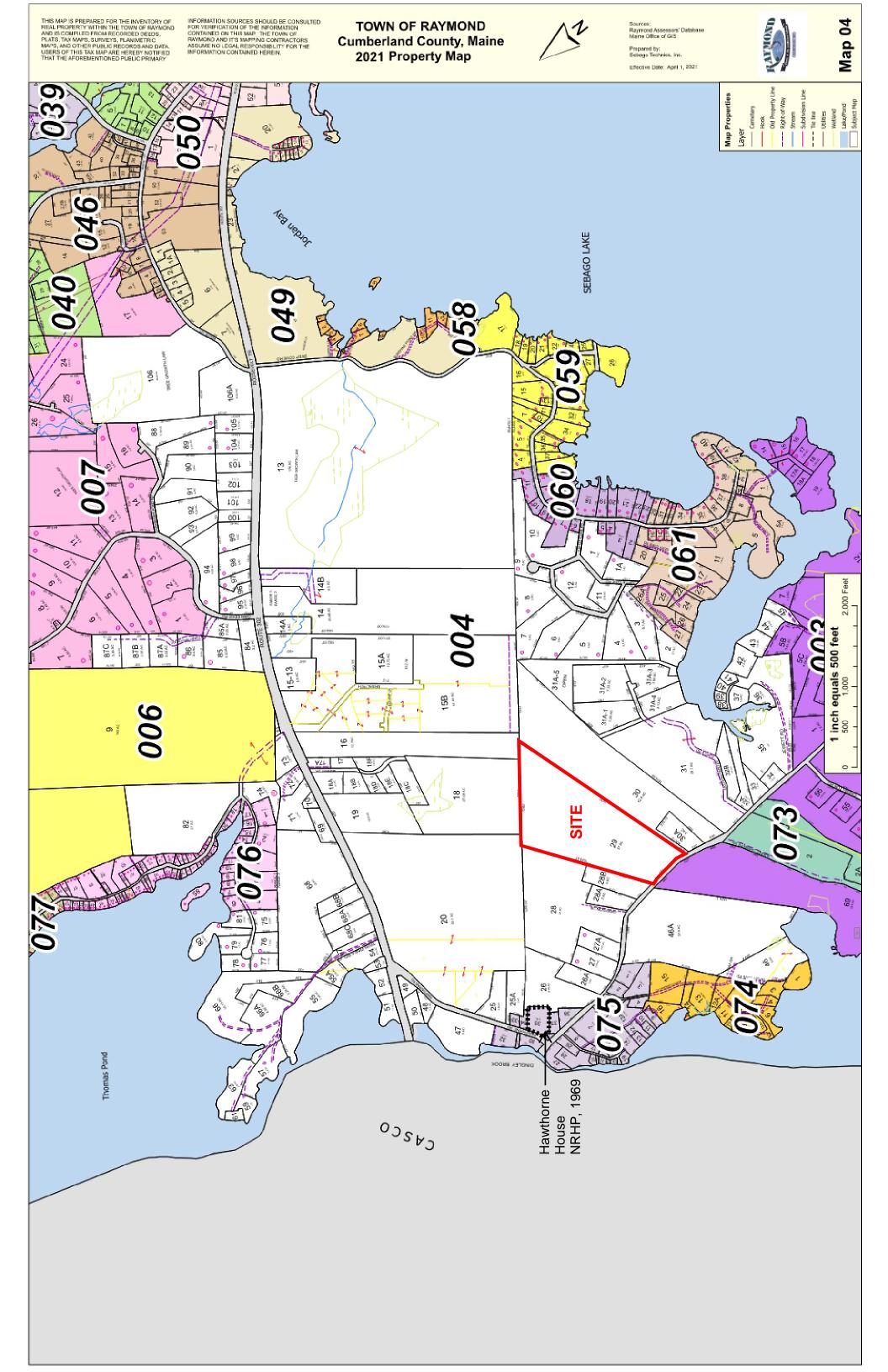
Map/Lot: 73-3-0 SPALDING, HILDEGARDE S & PETER C/O ROBERT & GRETCHEN WETZEL PO BOX 128 LYME, NH 03768 Map/Lot: 4-30-0 POTVIN, DIANE G 8 LEDGE ROAD CUMBERLAND FORESIDE, ME 04110

> Map/Lot: 4-46-A00 ALTMAN, DIANA SIEGEL, RICHARD H 1025 5TH AVE NEW YORK, NY 10028

> Map/Lot: 4-16-0 CHARETTE, JOYCE R PO BOX 103 RAYMOND, ME 04071

Map/Lot: 4-31-0 POTVIN, GARY L POTVIN, DIANE G 78 CAPE RD RAYMOND, ME 04071

LOCUS Map/Lot: 4-29-0 CHASE, BRANDON 15 WASHINGTON COURT NAPLES, ME 04055



# Exhibit 3

Right, Title and Interest

#### EXHIBIT 3: RIGHT, TITLE AND INTEREST

A copy of Cumberland County Registry of Deeds Book 38175/Page 131 indicating that the project applicant, Brandon Chase, is the record owner of the property is included in this section.

#### DLN: 1002140143316

#### WARRANTY DEED

#### (Maine Statutory Short Form - 33 M.R.S.A. §§ 761 et seq.)

KNOW ALL PERSONS BY THESE PRESENTS, that I, Diane G. Potvin of the Town of Cumberland, County of Cumberland and State of Maine, for valuable consideration received, hereby GRANT to Brandon Chase, of the Town of Naples, County of Cumberland and State of Maine, with WARRANTY COVENANTS, a certain lot or parcel of land, together with any buildings or improvements thereupon, situated in the Town of Raymond, County of Cumberland and State of Maine, and being more particularly described as follows:

See Exhibit A, attached hereto and incorporated herein.

Witness my hand and seal this 21st day of April, 2021.

Witness

Diane G. Potvin

STATE OF MAINE COUNTY OF CUMBERLAND, SS.

Then personally appeared this 21st day of April, 2021, the above named Diane G. Potvin and acknowledged the foregoing instrument to be her free act and deed.

Before me,

Notary Public/ Attorney at Law

Notary Public/ Attorney at Law Printed Name: \_\_\_\_\_\_ My Comm. Exp: \_\_\_\_\_

Katherine G. Young Notary Public State of Maine My Commission Expires 5/22/2024

#### EXHIBIT A

#### (Lot 29 Cape Road-Raymond, Maine)

A certain lot or parcel of land situated in the Town of Raymond, Cumberland County, Maine, on the easterly side of Raymond Cape Road, so-called, bounded and described as follows:

Beginning at a 5/8 inch rebar set flush in the northeasterly sideline of said Raymond Cape Road, 6.61 feet northerly from an existing 1/2 inch iron pipe 20 inches high, said rebar being set at the southwesterly corner of land now or formerly of Wayne G. Whitney, et ux, and the northwesterly corner of the land herein conveyed, as shown on standard boundary survey entitled "Designed Homes, Inc. Property", revised date 1/25/94, made for Chiyung Tse by Sebago Technics, 12 Westbrook Common, Westbrook ME 04098-13395;

thence North 54° 54′ 57″ East, along land of said Whitney and a line blazed in 1959 as shown on survey plan entitled "Land of Peter A. Anderson and Lawrence H. Stubbs in Raymond, Maine", as recorded in Cumberland County Registry of Deeds (CCRD) in Plan Book 52, Page 14, a distance of 1,629.87 feet to a point South 54° 54′ 57″ West 1.54 feet from a 1.5 inch iron pipe found leaning in a stone pile, said point being on the southeasterly sideline of land formerly of Roger D. Hewson as described in deed recorded in CCRD Book 4239, Page 8, North 54° 11′ 58″ West, a distance of 221.88 feet from another 1.5 inch pipe set in a stone pile at the southerly corner of ]and of said Hewson;

thence South 54° 11′ 58″ East a distance of 221.88 feet to said 1.5 inch pipe set in a stone pile at the southerly corner of land of said Hewson;

thence South 53° 40′ 50″ East along land now or formerly of Richard N. Martin, et al., as described in deed recorded in CCRD Book 3597 Page 308, a distance of 1,025.30 feet to a 21/4 inch monument 5″ high set in 1989 by Hardes & McAllister;

thence South 71° 25′ 45″ West along land now or formerly of Bruce J. Saunders, et al, as described in deed recorded in CCRD Book 3050, Page 822, a distance of 2,397.16 feet to a 2 1/4 inch monument 5″ high set in 1989 by Hardes & McAllister and the assumed sideline of said Raymond Cape Road;

thence North 00° 39′ 40″ East by said assumed sideline of Raymond Cape Road, a distance of 130.53 feet to a point;

thence North 09° 02′ 50″ West by said assumed sideline of Raymond Cape Road, a distance of 438.62 feet to the point of beginning.

The legal description used herein was prepared pursuant to a standard boundary survey entitled "Designed Homes, Inc. Property", revised 1/25/94, prepared for Chiyung Tse A/K/A Jonathan Tse C. Y. by Sebago Technics, 12 Westbrook Common, Westbrook ME 04098-1339, recorded in said Registry in Plan Book 194, Page 57.

Reference may be made to a Warranty Deed from Chiyung Tse a/k/a Jonathan Tse to Diane G. Potvin dated August 13, 2014 and recorded in Book 31733, Page 231 in the Cumberland County Registry of Deeds.

\* \* \* \* \* \*

Reviewed and Approved:\_\_\_\_\_

# Exhibit 4

# **Technical Capability/Financial Capacity**

#### EXHIBIT 4: TECHNICAL CAPABILITY/FINANCIAL CAPACITY

<u>Technical Capability:</u> The Applicant has retained Sebago Technics to provide engineering, survey, environmental, traffic analysis, and regulatory permitting services. A firm view of Sebago Technics' list of licensed and specialized personnel and the project manager's resume is enclosed in this section.

<u>Financial Capacity</u>: An estimate of probable cost for the site work is \$600,000.00. The Applicant intends to finance the project by a development loan for the project. A letter from the applicaint's financial institution will be provided with the Final Subdivision Plan submission.

### **Civil Engineering**

Site Plans Grading & Drainage Design Utility Design (Water, Sewer) Stormwater Management Permitting (Local, State & Federal) Quarry/Gravel Pit Studies & Permitting Technical Review Construction Inspection

#### **Environmental Services**

NRPA/NEPA Studies Site Assessments (ESAs, VRAPs) Septic Design & Analysis Floodplain Studies & Permitting

#### **Transportation Engineering**

Signal Analysis, Design & Management Traffic Analysis & Permitting Intersection, Road & Highway Design Alternatives Analysis & Route Design Bicycle and Pedestrian Facilities

#### Landscape Architecture

Conceptual & Site Design Park & Public Space Design Urban Design Master and Campus Planning Waterfront Planning Planting Design Visual Impact Assessments

#### Land Surveying/Geomatics

Technical Deed Research Boundary & Topographic Survey ROW Survey & Mapping Land Title Survey Subdivisions GPS Survey & Mapping Construction Layout (Vertical & Horizontal) As-Built Surveys High Definition 3D Laser Scanning Hydrographic Surveying Forensic Surveying Aerial Photogrammetry Tax Map Updates Zoning & Shoreland Zoning Map Updates

#### Soil Sciences

Soil Surveys & Testing Wetland Assessment & Permitting Vernal Pool Mapping

#### **Planning & Permitting**

Industrial/Business Parks Feasibility Assessments Sand, Gravel and Quarry Mining Wetland Assessments and Mitigation NHDES and USACOE Permitting NRPA/NEPA Studies Local Permitting Ordinance Development & Amendments





# LET'S MEET TOGETHER.

75 John Roberts Road, Suite 4A South Portland, Maine 04106 (207) 200.2100

# PERSONNEL



CIVIL ENGINEERING Owens McCullough, PE, LEED-AP Sr. VP., Strategy & Client Development

Shawn Frank, PE Sr. Vice President, Commercial Development

Daniel Riley, PE, CFM Vice President, Engineering

James Seymour, PE Senior Project Manager

Robert McSorley, PE Senior Project Manager

Stephen Harding, PE Senior Project Manager

Craig Burgess, PE Senior Project Manager

Paul Ostrowski, PE Senior Project Engineer

Aaron Hunter, PE Project Engineer

Christopher Taylor, PE Senior Project Engineer

ENVIRONMENTAL Cole Peters, CG, PWS

Environmental Services Manager

Gary Fullerton, LSS, LSE, CWS Director of Natural Resources

Anna Biddle, LSS Environmental Scientist/Permitting Specialist LAND SURVEYING

Terry Bennett, PLS LPF MRICS ENV SP LEED AP Vice President, Survey-Geomatics

Mathew Ek, PLS, LLS Director of Survey/GIS Advancement

Jacob Bartlett, PLS Survey Operations Manager

Charles Marchese, PLS Director of Survey Operations

David Titcomb, PLS Principal Surveyor

Joshua Eon, PLS Project Surveyor/Chief sUAS Pilot

Brian Stoddard, PLS Project Surveyor

Christopher LaMotte, PLS Project Surveyor

David Jacques, PLS Project Surveyor

Justin Brown, PLS Project Surveyor

Nicholas Elliston, PLS Project Surveyor

#### PERMITTING

Rebecca Gabryszewski Permitting Coordinator

**Stefanie Nichols** Permitting Specialist/Project Coordinator

#### LANDSCAPE ARCHITECTURE Kylie Mason, RLA, LEED-AP Chief Operations Officer

Stephen Doe, RLA, LEED-AP Senior Landscape Architect

Amy Bell Segal, RLA Senior Landscape Architect

Henry Hess, RLA Landscape Architect

#### TRANSPORTATION ENGINEERING

**Bradley Lyon, PE, PTOE** Director, Transportation Services

Curtis Thompson, PE, PTOE Transportation Engineer

Derek Caldwell, PE, PTOE Transportation/Traffic Engineer

Shane Kelly, PE Transportation Engineer

Nicole Conant, PE Transportation Engineer

#### **GEOGRAPHIC INFO. SYSTEMS**

Jake Hansen GIS Specialist

Maria Morris GIS Specialist

CONSTRUCTION INSPECTION Mike Kane, LPA, CPESC Senior Inspector

# ROBERT A. MCSORLEY, PE

Senior Project Manager



Mr. McSorley joined Sebago Technics, Inc. (STI) in 2006. He has worked in the Civil Engineering field since 1986 and is a Senior Project Manager specializing in project management for government, commercial and residential projects. He is responsible for client contact, proposals, financial aspects of projects, preparation of reports, bid documents, permitting issues, and construction coordination on a variety of public and private projects. He is also active in the community having served on the Portland Water District Board of Trustees and on the Scarborough Sanitary District Board of Trustees and currently serves as a Board member for Camp Scarborough.

## EXPERIENCE

Mr. McSorley has completed and is working on several commercial and residential projects in New Hampshire and Massachusetts. In addition, he assists in QA/QC oversight of other projects, marketing of firm's services and technical guidance and training staff.

Rob has also performed peer reviews of projects and was the Assistant District Engineer for a 4800 acre Special Services District. In that capacity, he was responsible for civil engineering and water management reviews for new projects. In addition, he was responsible for the design of the District's infrastructure including water, IQ and gravity sanitary, force mains, pump stations, drainage roadways and water management systems.

#### Some of his most notable work experience includes:

- Gorham Road Drainage Improvements South Portland, ME
- · Maine Mall Road Drainage Improvements South Portland, ME
- Maine Mall Road Sanitary Sewer Replacement South Portland, ME
- Maine Street Drainage & Sidewalk Improvements Town of Kennebunkport, ME
- Bedford Street Sewer Separation Project & Portland Water District Main Project Portland, ME
- Mast Road Culvert Replacement Town of Waterboro, ME
- Pine Street Bridge Replacement (Box Culvert) Porter, ME
- USPS FSS Building Expansion North Reading, MA
- Sunbury Retirement Residence Bangor, ME
- Derry Retirement Residence Derry, NH
- Beverly Retirement Community Beverly, MA
- Tewksbury Retirement Residence Tewksbury, MA
- Portland Retirement Residence Portland, ME
- Billerica Retirement Residence Billerica, MA
- Mountain View Estates North Conway, NH
- · Veteran's Administration Medical Center Cogeneration Facility Canandaigua, NY
- Synchronous Condenser, Green Mountain Power Jay, VT
- Veterans Administration Hospital Palm Beach County, FL

## EDUCATION

Florida Atlantic University Boca Raton, FL Bachelor of Science, Mechanical Engineering, 1995

University of Maine - Orono, ME Majored in Mechanical Engineering 1980-1983

## REGISTRATIONS

Professional Engineer: Maine, New Hampshire, Massachusetts, Vermont

National Council of Examiners for Engineering and Surveying

### MEMBERSHIPS

American Society of Civil Engineers

National Society of Professional Engineers

Maine Engineering Society

## CERTIFICATIONS

Maine DEP Maintenance & Inspection of Stormwater BMPs



# JEFFREY B. POLLARD, EI

**Civil Engineer** 



Mr. Pollard joined Sebago Technics, Inc., (STI) in August of 2020. Mr. Pollard was an intern with Sebago in the summer of 2019 and is a recent graduate from UMaine with a degree in Civil Engineering. In his current role as Civil Engineer, Jeff is a member of a design team within the Project Delivery Group at Sebago Technics. He focuses on the technical aspects of site design, including complex grading, treatment and control of stormwater, utility layout, and roadway design.

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## EXPERIENCE

**The Edge at Berwick – Berwick, ME:** As one of the design engineers for the project, performed grading design, utility layout, and stormwater analysis for the project. The project is proposing a total of 12 mixed-use commercial and residential buildings with associated roadways, parking, and utility infrastructure.

**The Maine Stay Inn & Cottages – Kennebunkport, ME:** Design engineer for the redevelopment of the site for renovated cottages, a new parking lot, and redesigned common space. Work included grading of the site and stormwater analysis and improvements.

**Bowden Point Road Extension – Prospect, ME:** Design engineer for the conversion of a private gravel road to a town accepted paved road. Work included layout design and grading of dead-end turnaround and cost estimate.

**Morong Falmouth Porsche – Falmouth, ME:** Design engineer for the project, which includes a new dealership building and overflow parking lot. Performed grading of site, stormwater analysis and improvements, and assisted with layout of new utilities.

## EDUCATION



University of Maine - Orono, ME B.S., Civil Engineering 2020



# BRIAN A. MCMAHON Landscape Designer



Mr. McMahon joined Sebago Technics, Inc., (STI) in July of 2021. Brian is a recent graduate from the University of Rhode Island with a degree in Landscape Architecture and a minor in Community Planning. While in college, he was part of the Sigma Lambda Alpha Honor Society and the recipient of the University of Rhode Island Centennial Scholarship and Red Sox Scholar. He is a Maine resident and interned with Sebago Technics during the winter of 2021.

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## EXPERIENCE

#### Sebago Technics Inc. - South Portland, ME

Landscape Architecture Intern Dec. 2020 – Jan. 2021

- Range of work included rendering a variety of conceptual site plans and developing preliminary sketches for new projects.
- Familiarized with professional environment, in which multiple teams collaborated amongst one another.
- · Acquired valuable skills with Adobe PhotoShop.

#### Gogan Landscaping & Masonry - Wells, ME

Mason & Landscape Installer May 2018 – Aug. 2020

- Assisted in redesigns and installs of custom landscapes mostly on a residential scale.
- Facilitated landscape installs ranging from planting designs and small hardscapes.
- Led a small crew in numerous projects ranging from large patios, dry stack rock wall installations, and stone veneer applications.

#### Winn Contracting - Ogunquit, ME

Home Construction *Apr. 2015 – Sep. 2017* 

- Assisted in construction of two different houses.
- · Acquired valuable skills and an understanding of contracting.

## EDUCATION

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University of Rhode Island, Kingston, Rhode Island Bachelor of Landscape Architecture Minor: Community Planning

## SKILLS

Experienced landscape installer and mason

Proficient in AutoCAD, SketchUp & Lumion

Proficient in Adobe PhotoShop, InDesign, & Illustrator

Deciduous & coniferous plant identification



# JACOB L. HANSEN GIS Specialist



Mr. Hansen joined Sebago Technics, Inc., (STI) in October of 2020 as a GIS Specialist. Jacob is experienced in GIS, field mapping and geoscientific methods with a strong research background. He is a skilled cartographer who excels at finding innovative ways to answer problems with GIS, and has ample experience performing and troubleshooting geospatial data maintenance and analysis in various desktop and web applications. Jacob is also proficient in scientific analysis, data management, the use of specialized equipment and programs, and the production of high-quality maps and deliverables.

Providing direct support to the engineers at Sebago Technics, Jacob ensures the locational integrity of land data used in civil design. Best practice skills and resources are applied to collect, manipulate, and assemble high-accuracy geospatial data. Mr. Hansen's unique blend of field surveying, digital mapping and geoscientific training provides an excellent resource to the whole team.

## EXPERIENCE

**Ground Surface Modeling:** With the use of remote sensing technology such as LiDAR and High-Definition Laser Scanning, ground surface models can be developed from three dimensional points clouds without the need for conventional survey. These point clouds capture ground surface elevation as well as building and vegetation heights. Mr. Hansen utilizes specialized software to create Digital Terrain Models (DTMs) and Digital Surface Models (DSMs) from the point clouds, allowing for the creation of highly-accurate models with reduced time in the field. Mr. Hansen utilizes these products to conduct various analyses, including viewshed, hydrographical and slope, and to provide surface models to the engineers.

**Environmental Permitting and Services:** Mr. Hansen provides maps, analyses, general information, and technical write-ups for various environmental projects, including viewshed analysis, portions of Phase I Environmental Site Assessments, and high-quality maps and deliverables for a multitude of project types.

**Tax Mapping:** Sebago Technics contracts with the Towns of Poland and Raymond, ME, providing tax mapping and other GIS services. This includes the routine maintenance and update of the cadastre, providing deliverables in the form of maps and digital data. Mr. Hansen brings his Land Records experience from North Carolina, where he is a Certified Property Mapper well-versed in property mapping and title research.

**Broadband Connectivity Dataset – Town of Poland, ME:** The Town of Poland requested the services of Mr. Hansen to map internet broadband connectivity within the town boundaries. The dataset provides street-level detail broadband availability information, including cable and DSL layers and a regional fiber optic transport route.

## EDUCATION

East Tennessee State University, Johnson City, TN M.S. Geosciences - Geospatial Analysis Concentration, 2020

University of Maine at Farmington -Farmington, ME B.A., Geology, 2011

## CERTIFICATIONS

North Carolina Certified Property Mapper

### AWARDS

Michael D. Wilson Fellow, 2010-2011

Best Student Poster – 37th Annual Colloquium of the Atlantic Geoscience Society, 2011



# Exhibit 5

Stormwater Management/ Phosphorus Control

#### EXHIBIT 5: STORMWATER MANAGEMENT/PHOSPHORUS CONTROL

Per the requirements of the Town of Raymond Subdivision Regulations, Article 5-Preliminary Plan, a copy of the formal Stormwater Management Report, calculations, drawings, inspection, maintenance, housekeeping, and phosphorus control narrative is included in this section. The appended plan set shows the erosion and sedimentation control notes, details, and locations.



CIVIL ENGINEERING . SURVEYING . LANDSCAPE ARCHITECTURE

# **STORMWATER MANAGEMENT REPORT**

For

# RAYMOND CAPE ROAD SUBDIVISION RAYMOND, MAINE

Prepared for:

Brandon Chase 15 Washington Court Naples, Maine 04055

Prepared by:

Sebago Technics, Inc. 75 John Roberts Rd, Suite 4A South Portland, ME 04106

# March, 2022



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Appendix 4:	Subsurface Investigations
Appendix 5:	Flood Insurance Rate Map
Appendix 6:	Stormwater Management Plans

#### 21397

# STORMWATER MANAGEMENT REPORT RAYMOND CAPE ROAD SUBDIVISION RAYMOND, MAINE

#### 1. Introduction

This Stormwater Management Plan Report has been prepared to present analyses performed to address the potential impacts associated with the project due to proposed modification in stormwater runoff characteristics and land cover changes. The stormwater management controls that are outlined in this report have been designed to suit the proposed development and to comply with applicable regulatory requirements.

#### 2. Existing Conditions

The project site is an approximately 37-acre parcel of undeveloped land on Raymond Cape Road, Raymond. The parcel consists of undeveloped woodland and is located on the eastern side of Raymond Cape Road. The proposed site is identified on the Town of Raymond Tax Map 04 as lot 29. The site generally slopes up from Raymond Cape Road, and typical slopes on the site range from approximately 5-35%.

The proposed site is tributary to Sebago Lake. Sebago Lake is listed as most at risk from new development in the Maine DEP Chapter 502.

The proposed development area of the site is not located in an identified flood zone per the FEMA Flood Insurance Rate Map for the Town of Raymond, Community Panel 2302050020B with an effective date of May 5, 1981. A copy of the flood insurance rate map is attached in Appendix 5.

### 3. <u>Soils</u>

Soil information for the site was obtained via the USDS United States Department of Agriculture and Natural Resource Conservation Services (NRCS) Web Soil Survey. The Hydrologic Soil Groups (HSG) of the soils on site as classified by the Soil Conservation Service are delineated on the stormwater management plans and are as follows:

Soil Map Symbol	Soil Name	Slope (%)	HSG
BeD	Becket	15-25	С
SeA	Sebago	0-3	D
SkB	Skerry	3-8	C
SkC	Skerry	8-15	С
TuC	Tunbridge	8-15	C
TuD	Tunbridge	15-25	C
WeB	Westbury	3-8	D

A copy of the Class C, Medium-High Intensity Soil Survey performed by Sebago Technics, Inc. is included in Appendix 4.

# 4. Proposed Site Improvements

The proposed project is a residential subdivision consisting of 12 lots with an average lot size of approximately 1.7 acres. Access for the proposed subdivision will be provided by a deadend private road that runs through the center of the original 37-acre parcel. The private road will extend approximately 2,000 linear feet from Raymond Cape Road to the rear boundary of the existing parcel. Stormwater runoff will be treated by two grassed underdrained soil filters. The proposed site improvements are for the construction of the subdivision road and stormwater control methods only. Development of the individual house lots is not proposed as part of this project. The proposed site improvements will result in a total developed area of approximately 142,505 square feet, and create approximately 42,240 square feet of new impervious area.

# 5. Existing Conditions Model

The Existing Conditions Stormwater Management Plan consists of five (5) subcatchments labeled 1.0S through 5.0S in the HydroCAD model. Five (5) locations were identified as Points of Analysis (POA) for comparing peak runoff rates.

POA-1 is located in the northwest portion of the site where runoff drains northwest towards the adjacent house lot. Subcatchment 1.0S contributes runoff to this POA with a total runoff area of approximately 4.0 acres. POA-1 and the associated drainage areas are tributary to Sebago Lake.

POA-2 is located at the southwest corner of the parcel in the ditch along Raymond Cape Road. Subcatchment 2.0S contributes runoff to this POA with an overall runoff area of approximately 7.3 acres. POA-2 and the associated drainage area is tributary to Sebago Lake.

POA-3 is located south of the parcel in the existing forested wetland complex. Subcatchment 3.0S contributes runoff to this POA with an overall runoff area of approximately 6.0 acres. POA-3 and the associated drainage area is tributary to Sebago Lake.

POA-4 is located southeast of the parcel in a large existing forested wetland. Subcatchment 4.0S contributes runoff to this POA with an overall runoff area of approximately 23.0 acres. POA-4 and the associated drainage area is tributary to Sebago Lake.

POA-5 is located at the northeast corner of the parcel in the small existing wetland. Subcatchment 5.0S contributes runoff to this POA with an overall runoff area of approximately 1.2 acres. POA-5 and the associated drainage area is tributary to Sebago Lake.

# 6. Proposed Conditions Model

The Proposed Conditions Stormwater Management Plan consists of the same overall area as the Existing Conditions plan, however, the proposed condition subcatchments have been broken into smaller watersheds as a result of the proposed development. Subcatchment areas have been modeled to account for the future development of each lot, with an assumed developed area of 12,500 SF, of which 3,000 SF is assumed to be impervious. The stormwater BMPs have been designed for control of peak runoff rates from this future development, however stormwater quality treatment is provided for the roadway only.

Subcatchment 10.0S is tributary to POA-1 where runoff from undeveloped woodland area drains northwest towards the adjacent property. This subcatchment is relatively unchanged from existing conditions and is approximately 3.7 acres in size.

POA-2 contains subcatchments 20.0S through 20.6S where runoff drains to the Raymond Cape Road ditch located at the southwest corner of the overall site. Subcatchments 20.0S, 20.1S, and 20.2S receive stormwater quality treatment through the proposed BMP located at the entrance to the site. The total area draining to POA-2 in the proposed conditions is approximately 8.3 acres.

POA-3 contains subcatchment 30.0S and consists of two proposed house lots and open space that drain towards the center of the southern boundary of the overall site. The total area of this subcatchment is approximately 5.2 acres.

Subcatchments 40.0S through 40.6S contribute runoff to POA-4, located near the southeast boundary of the overall site. Water quality treatment is provided to subcatchments 40.0S and 40.1S by the second proposed stormwater BMP located near the rear end of the proposed roadway. The overall area of these subcatchments is approximately 23.0 acres.

Subcatchment 50.0S contains the same 1.2-acre area as the Existing Conditions Model subcatchment 5.0S, and drains to POA-5 located at the northeast corner of the site.

The two Best Management Practices (grassed underdrained soil filters) have been designed and sized in accordance with Maine DEP BMP standards contained within Chapter 500 and the BMP Manual. Sizing calculations can be found in Appendix 1.

# 7. Stormwater Management

# Basic Standard - Chapter 500, Section 4(B)

Since the project will disturb more than one (1) acre of land area, MDEP Basic Standards apply, requiring that grading or other construction activities on the site do not impede or otherwise alter drainage ways to have an unreasonable adverse impact. We have avoided adverse impacts by providing an Erosion & Sedimentation Control Plan, and an Inspection, Maintenance and Housekeeping Plan (Appendix 3) to be implemented during construction and post-construction stabilization of the site. These construction requirements have been developed following Best Management Practice guidelines.

# General Standard - Chapter 500, Section 4(C)

Since the project will create more than 20,000 square feet of impervious area in the watershed of a lake most at-risk, MDEP General Standards apply, which require a project's stormwater management system to include treatment measures that will mitigate for the increased frequency and duration of channel erosive flows due to runoff from smaller storms, provide for effective treatment of pollutants in stormwater, and mitigate potential temperature impacts. The General Standards require treatment of no less than 95% of the site's created impervious area and no less than 80% of the site's created developed area (landscaped area and impervious area combined). To mitigate the changes in hydrologic patterns due to the development of this project, two underdrained soil filters have been implemented into the stormwater management infrastructure. Filtration BMPs are very effective at removing a wide range of pollutants through the use of organic soil filter media.

# Linear Portion of a Project - Chapter 500, Section 4(C)5(c)

Since the project is for the construction of a road only, it falls under the linear portion exception of the General Standard. This exception reduces the treatment requirements to no less than 75% of the linear portion's impervious area and 50% of the linear portion's developed area. Through the use of the aforementioned BMP's 85.3% of new impervious area and 80.8% of new developed area will be receiving treatment. This meets the requirements for the Maine DEP General Standards, Linear Portion of a Project Exemption. Treatment and BMP calculations are attached to this report as Appendix 1.

# Phosphorus Standard - Chapter 500, Section 4(D)

Since the proposed roadway will create less than 3 acres of impervious area and less than 5 acres of developed area in a lake watershed that is not severely blooming, the general standards may be used instead of the phosphorus standard.

# Flooding Standard – Chapter 500, Section 4(F)

Since the project results in less than three acres of impervious area and less than 20 acres of developed area, DEP flooding standards do not apply. The flooding standard requires that the peak runoff rates in the proposed conditions do not exceed the existing peak runoff rates in the 24-hour storms of the 2, 10, and 25-year frequencies. However, per Town of Raymond requirements, the peak runoff rates in the fully developed subdivision conditions must be at or below the existing conditions. Since development of the lots is not proposed as part of this project, assumed areas of development had to be used for each lot to analyze these conditions. Lot development was assumed to be 12,500 square feet per lot, with 3,000 square feet assumed to be impervious area. These conditions were modeled using HydroCAD computer software to ensure the proposed stormwater control methods are adequate to maintain peak runoff rates in the fully developed condition that are at or below existing peak rates.

Runoff curve numbers were determined for each of the subcatchment by measuring the area of each hydrologic soil group within each type of land cover. Hydrologic soil groups on the site were determined by the Class C medium-high intensity soil survey performed by Sebago Technics. The type of land cover was determined based on survey data, field reconnaissance, and aerial photography. Times of concentration were determined from site topographic maps in accordance with SCS procedures.

The 24-hour rainfall values utilized in the hydrologic model were obtained from Appendix H of MDEP's Chapter 500: Stormwater Management (effective date August 2015). Rainfall values for Cumberland County are listed in the table below.

	ecipitation (in./24 hr) and County
2-year	3.1
10-year	4.6
25-year	5.8

	Pea	ak Runoff Rate Summary Table	
Analysis Point	Storm Event	Existing Conditions (cfs)	Proposed Conditions (cfs)
	2-year	3.4	3.4
POA-1	10-year	7.5	7.3
	25-year	11.0	10.6
	2-year	4.8	4.7
POA-2	10-year	11.3	11.3
	25-year	17.2	17.2
	2-year	4.0	3.8
POA-3	10-year	10.0	8.9
	25-year	15.5	13.5
	2-year	10.1	9.3
POA-4	10-year	24.3	24.3
	25-year	37.3	37.3
	2-year	0.6	0.6
POA-5	10-year	1.5	1.5
	25-year	2.3	2.3

The following table presents the results of the peak runoff calculations at the analysis points for the existing and proposed conditions.

The HydroCAD Data output sheets from this analysis are appended to this report (Appendix 2) along with the Stormwater Management Plans (Appendix 5). The model predicts that the peak runoff rates in the fully developed subdivision conditions at all Points of Analysis are at or below existing peak runoff rates for the 2, 10, and 25-year storm events with implementation of the proposed stormwater management practices.

# 8. Summary

The proposed development has been designed to manage stormwater runoff through Best Management Practices approved by MDEP. Stormwater BMP's provide treatment to 85.3% (75% required) of impervious areas, and 80.8% (50% required) of the total developed area associated with development of the roadway only. Control of stormwater quantity has been designed for both the proposed roadway development and the future lot development at a limit of 12,500 SF per lot (3,000 SF impervious area). Stormwater discharging from the fully developed subdivision will be at or below existing conditions for the 2, 10, and 25-year storm events at all five Points of Analysis. Additionally, erosion and sedimentation controls along with associated maintenance and housekeeping procedures have been outlined to prevent unreasonable impacts on the site and to the surrounding environment.

Prepared by:

SEBAGO TECHNICS, INC.

Robert A. McSorley, ME PE Senior Project Manager



March 9, 2022

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Jeffrey Pollard, El Civil Engineer

# **Appendix 1**

**Stormwater Quality Calculations** 

		<b>EXISTING ONSITE</b>		<b>EXISTING ONSITE</b>	<b>NEW ONSITE</b>	<b>NET NEW</b>	<b>NET EXISTING</b>		IMPERVIOUS		DEVELOPED	
		<b>IMPERVIOUS AREA</b>	<b>NEW ONSITE</b>	LANDSCAPED AREA	LANDSCAPED	DEVELOPED	DEVELOPED	TREATMENT	AREA	LANDSCAPED	AREA	TREATMENT
AREA ID	WATERSHED SIZE	TO REMAIN	IMPERVIOUS AREA	TO REMAIN	AREA	AREA	AREAS	PROVIDED?	TREATED	AREA TREATED	TREATED	BMP
	(S.F.)	(S.F.)	(S.F.)	(S.F.)	(S.F.)	(S.F.)	(S.F.)		(S.F.)	(S.F.)	(S.F.)	
10.0S	162,904	0	0	0	0	0	0	NO	0	0	0	
20.0S	26,540	0	9,645	0	16,895	26,540	0	YES	9,645	16,895	26,540	UDSF-1
20.1S	31,943	0	8,979	0	22,964	31,943	0	YES	8,979	22,964	31,943	UDSF-1
20.2S	3,333	0	1,046	0	2,287	3,333	0	YES	1,046	2,287	3,333	UDSF-1
20.3S	114,936	0	0	0	0	0	0	NO	0	0	0	
20.4S	36,581	0	0	0	0	0	0	NO	0	0	0	
20.5S	111,066	0	1,301	0	3,062	4,363	0	NO	0	0	0	
20.6S	38,906	0	1,406	0	2,476	3,882	0	NO	0	0	0	
30.0S	224,629	0	1,210	0	1,144	2,354	0	NO	0	0	0	
40.0S	26,154	0	9,523	0	16,631	26,154	0	YES	9,523	16,631	26,154	UDSF-2
40.1S	27,219	0	6,830	0	20,389	27,219	0	YES	6,830	20,389	27,219	UDSF-2
40.2S	15,145	0	0	0	0	0	0	NO	0	0	0	
40.3S	313,659	0	0	0	3,467	3,467	0	NO	0	0	0	
40.4S	104,649	0	0	0	0	0	0	NO	0	0	0	
40.5S	47,186	0	518	0	2,287	2,805	0	NO	0	0	0	
40.6S	469,486	0	1,782	0	8,663	10,445	0	NO	0	0	0	
50.0S	52,286	0	0	0	0	0	0	NO	0	0	0	
TOTAL (S.F.)	1,806,622	0	42,240	0	100,265	142,505	0		36,023	79,166	115,189	

EW IMPERVIOUS AREA (S.F.)	42,240	TOTAL DEVELOPED AREA (S.F.)	142,505
JS AREA RECEIVING TREATMENT (S.F.)	36,023	TOTAL AREA RECEIVING TREATMENT (S.F.)	115,189
OUS AREA RECEIVING TREATMENT	85.28%	% OF AREA RECEIVING TREATMENT	80.83%

# Table 1: MDEP GENERAL STANDARD CALCULATIONS

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TOTAL NEW TOTAL IMPERVIOUS A % OF IMPERVIOUS

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					UNDERDRAIN	ED SOIL FILT	TER						
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				-7									
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Refere	ances	1. Widnie											
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		 • • •											
Tribut	ary to U	nderdraine	ed Filter	UDSF-1									
	Landsca	aped Area		42,146.00	SF								
	Impervi	ous Area		19,670.00	SF								
Minim	num Surf	ace Area											
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				12)2 10100		7.1.00	0.1210	0.					
	Total In	npervious /	Area	19,670.00	SE	Area	983.5	SF					
				13,070.00	51	Aica	505.5	51					
			Poqui	rod Minimur	n Surface Area		1,826.4	SF					
			Requi		I Sui lace Alea		1,020.4	JF					
				Dua talan			2.046.0	65					
				Provided	l Surface Area		2,916.0	SF					
_													
Treatr	nent Vol	ume											
	Require	ed	(0.4" X La	ndscaped + 1	.0" X Impervio	us)							
	Landsca	aped Area		42,146.00	SF	Volume	1,404.9						
	Impervi	ious Area		19,670.00	SF	Volume	1,639.2						
			Т	reatment Vol	ume Required		3,044.0	CF	0.070	AF			

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erence 2, Chapte				•	ded to mir	nimize discha	arge of sed	liment to th	ne soi	l filter"
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Sediment Load:				•	ded to mir	nimize discha	arge of sed	liment to th	ne soi	l filter"
	55 cubic feet	t per acre per y	ear of sanc	led area						
be sanded:	19,670.00	SF								
nt Volume	25	CF								
d	34	CF	6	Inch Deep	Forebay	with area	of	68	sf	
า	t Volume	t Volume 25	t Volume 25 CF	t Volume 25 CF						

#### SEBAGO TECHNICS, INC.

75 John Roberts Road, Suite 4A South Portland, Maine 04106 (207) 856-0277 FAX (207) 856-2206

SHEET NO. 2 OF 2	
CALCULATED BY JBP DATE 3/	/11/2022
СНЕСКЕД ВУ ВАМ	
FILE NAME 21397 WQC PRINT DATE 3/2	11/2022

ORIFICE SIZING CALCULATION

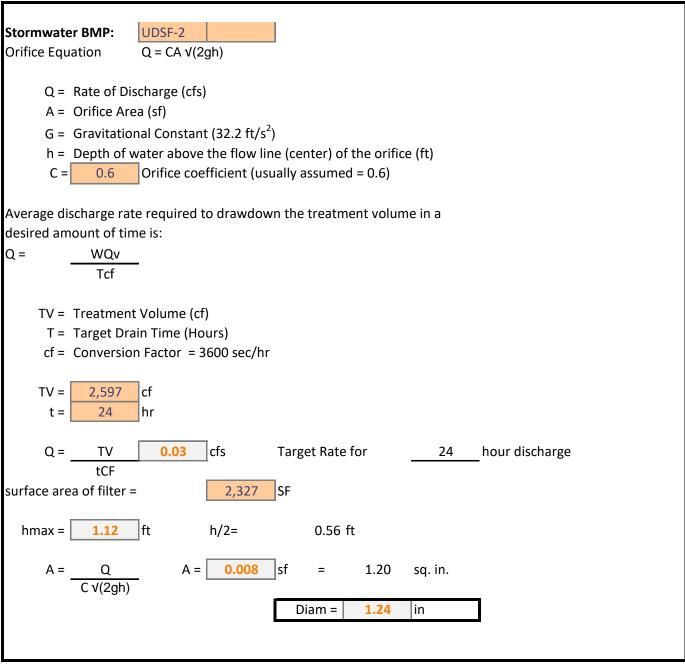
Stormwater BMP: UDSF-1
Orifice Equation $Q = CA \sqrt{2gh}$
Q = Rate of Discharge (cfs)
A = Orifice Area (sf)
G = Gravitational Constant (32.2 ft/s2)
h = Depth of water above the flow line (center) of the orifice (ft)
C = 0.6 Orifice coefficient (usually assumed = 0.6)
Average discharge rate required to drawdown the treatment volume in a desired amount of time is:
Q = WQv
TV = Treatment Volume (cf)
T = Target Drain Time (Hours)
cf = Conversion Factor = 3600 sec/hr
TV = 3,044 cf
t = 24 hr
Q = TV 0.04 cfs Target Rate for 24 hour discharge
surface area of filter = 2,916 SF
hmax = 1.04 ft h/2= 0.52 ft
A = Q $A = 0.010$ sf = 1.46 sq. in.
C √(2gh)
Diam = <b>1.36</b> in

		SEBAC	GO TECHN	ICS, INC.			JOB	21397					
		75 Johi	n Roberts Roa	ad Suite 4A			SHEET NO.	1			OF	2	
		South	Portland, Ma	ine 04106			CALCULATED BY	JBP			DATE	3/11,	/2022
	1	Tel	. (207) 200-	2100		1	FILE NAME	21397 WC	QC		PRNT DATE	3/11/	/2022
					UNDERDRAIN	ED SOIL FIL	FER						
Task:		Calculate	water qua	ility volume p	er MDEP chap	ter 500 regu	lations						
		1. Maine	DEP Chap	ter 500, Secti	on 4.C.(3)(b)								
Refere	ences												
		a.	"must de	tain a runoff	volume equal t	to 1.0 inch ti	mes						
			the subca	atchment's in	pervious area	plus 0.4 incl	n times the s	subcatchm	ent's lands	scaped area	a"		
		2. Maine	DEP Best	Management	Practices Stor	mwater Mai	nual, Sectior	n 7.1					
		a.	"surface :	should repres	ent 5% of imp	ervious area	and 2% of l	andscaped	area"				
												_	
<u>Tribut</u>	ary to Ui	nderdraine	ed Filter	UDSF-2								_	
	Landsca	ped Area		37,020.00	SF								
	Impervi	ous Area		16,353.00	SF								
Minim	num Surf	ace Area											
	Require	d	(2% X Lar	ndscaped + 5%	%" X Imperviou	s)							
	Total La	ndscaped	Area	37,020.00	SF	Area	740.4	SF					
	Total In	pervious /	Area	16,353.00	SF	Area	817.7	SF					
			Requi	red Minimun	n Surface Area		1,558.1	SF					
				Provideo	d Surface Area		2,327.0	SF					
Treatr	ment Vol	ume											
	Require	d	(0.4" X La	ndscaped + 1	0" X Impervio	us)							
	Landsca	ped Area		37,020.00	SF	Volume	1,234.0						
	Impervi	ous Area		16,353.00	SF	Volume	1,362.8						
			Т	reatment Vol	ume Required		2,596.8	CF	0.060	AF			

				Provided Treat	tment Volume		2,629.0	CF					
dime	ent Pre-	Treatment											
	Per Ref	erence 2, C	hapter 7	/.1	"Pretreatmen	t devices sha	all be provid	ed to min	imize discha	arge of sedi	ment to t	he soi	l filter"
	Annual	Sediment L	_oad:	55 cubic feet	t per acre per y	ear of sande	ed area						
	Area to	be sanded	:	16,353.00	SF								
	Sedime	nt Volume		21	CF								
	Provide	ed		54	CF	6	Inch Deep	Forebay	with area	of	107	sf	

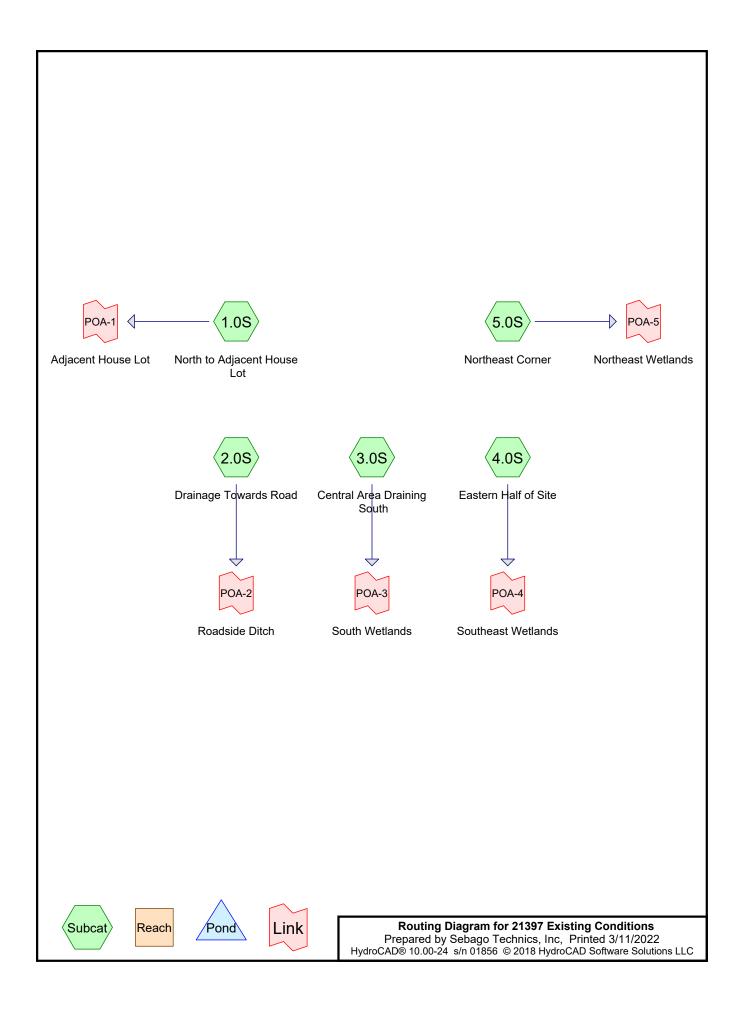
SEBAGO TECHNICS, INC.	JOB	21397		
75 John Roberts Road, Suite 4A	SHEET NO.	2	OF	2
South Portland, Maine 04106	CALCULATED BY	JBP	DATE	3/11/2022
(207) 856-0277   FAX (207) 856-2206	CHECKED BY	RAM	_	
	FILE NAME	21397 WQC	PRINT DATE	3/11/2022

ORIFICE SIZING CALCULATION



# **Appendix 2A**

Existing Conditions HydroCAD Summary



# Area Listing (all nodes)

CN	Description
	(subcatchment-numbers)
70	Woods, Good, HSG C (1.0S, 2.0S, 3.0S, 4.0S, 5.0S)
77	Woods, Good, HSG D (1.0S, 2.0S, 3.0S, 4.0S)
71	TOTAL AREA
	70 77

#### Summary for Subcatchment 1.0S: North to Adjacent House Lot

Runoff = 11.0 cfs @ 12.21 hrs, Volume= 1.033 af, Depth= 3.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

_	A	rea (sf)	CN	Description		
		41,519 31,893		Woods, Go Woods, Go		
-	1	73,412 73,412 73,412	75	Weighted A 100.00% Pe	verage	
	Tc (min)	Length (feet)			Capacity (cfs)	Description
-	2.7	20	/ /	/ /		Sheet Flow, A to B
	0.8	80	0 0.121 <i>°</i>	1.74		Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, B to C
	2.7	110	0 0.0180	0.67		Woodland Kv= 5.0 fps Shallow Concentrated Flow, C to D Woodland Kv= 5.0 fps
	0.7	65	5 0.1000	) 1.58		Shallow Concentrated Flow, D to E
	6.2	190	0 0.0105	5 0.51		Woodland Kv= 5.0 fps <b>Shallow Concentrated Flow, E to F</b> Woodland Kv= 5.0 fps
	0.5	55	5 0.1640	2.02		Shallow Concentrated Flow, F to G
_	1.4	60	0 0.0210	0.72		Woodland Kv= 5.0 fps <b>Shallow Concentrated Flow, G to H</b> Woodland Kv= 5.0 fps
	45.0	<b>_</b>	0 Tatal			

15.0 580 Total

#### Summary for Subcatchment 2.0S: Drainage Towards Road

Runoff = 17.2 cfs @ 12.24 hrs, Volume= 1.722 af, Depth= 2.83"

 Area (sf)	CN	Description
228,817	70	Woods, Good, HSG C
 89,136	77	Woods, Good, HSG D
317,953	72	Weighted Average
317,953		100.00% Pervious Area

#### 21397 Existing Conditions

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Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 HydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solutions LLC Page 4

(	Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.3	15	0.1200	0.11		Sheet Flow, A to B
						Woods: Light underbrush n= 0.400 P2= 3.10"
	8.3	675	0.0741	1.36		Shallow Concentrated Flow, B to C
						Woodland Kv= 5.0 fps
	3.5	105	0.0100	0.50		Shallow Concentrated Flow, C to D
						Woodland Kv= 5.0 fps
	1.1	115	0.1220	1.75		Shallow Concentrated Flow, D to E
						Woodland Kv= 5.0 fps
	2.2	235	0.0640	1.77		Shallow Concentrated Flow, E to F
						Short Grass Pasture Kv= 7.0 fps

17.4 1,145 Total

#### Summary for Subcatchment 3.0S: Central Area Draining South

Runoff 15.5 cfs @ 12.16 hrs, Volume= 1.322 af, Depth= 2.65" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

A	rea (sf)	CN E	Description		
2	44,072 16,877		,	od, HSG C od, HSG D	
	260,949 260,949	70 V	Veighted A	,	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.9	30	0.0750	0.10		Sheet Flow, A to B
1.6	160	0.1125	1.68		Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps
1.5	45	0.0100	0.50		Shallow Concentrated Flow, C to D
0.6	60	0.1167	1.71		Woodland Kv= 5.0 fps Shallow Concentrated Flow, D to E Woodland Kv= 5.0 fps
2.6	145	0.0357	0.94		Shallow Concentrated Flow, E to F Woodland Kv= 5.0 fps
11.2	440	Total			

#### Summary for Subcatchment 4.0S: Eastern Half of Site

37.3 cfs @ 12.53 hrs, Volume= 5.249 af, Depth= 2.74" Runoff =

# **21397 Existing Conditions**

Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 LLC Page 5

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_	A	rea (sf)	CN	Description		
		86,427	70	Woods, Go		
_		15,595	77	Woods, Go	,	
	,	02,022	71	Weighted A		
	1,0	02,022		100.00% Pe	ervious Area	a
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
-	- · · ·	. ,		//	(013)	
	5.0	25	0.0500	0.08		Sheet Flow, A to B Woods: Light underbrush n= 0.400 P2= 3.10"
	1.4	135	0.1038	3 1.61		Shallow Concentrated Flow, B to C
	1.4	100	0.1050	5 1.01		Woodland Kv= 5.0 fps
	2.2	110	0.0273	3 0.83		Shallow Concentrated Flow, C to D
			0.0			Woodland Kv= 5.0 fps
	0.8	65	0.0769	9 1.39		Shallow Concentrated Flow, D to E
						Woodland Kv= 5.0 fps
	13.7	290	0.0050	0.35		Shallow Concentrated Flow, E to F
						Woodland Kv= 5.0 fps
	7.5	560	0.0625	5 1.25		Shallow Concentrated Flow, F to G
	- 4	450	0.00-			Woodland Kv= 5.0 fps
	7.1	150	0.0050	0.35		Shallow Concentrated Flow, G to H
_						Woodland Kv= 5.0 fps
	377	1 2 2 5	Total			

37.7 1,335 Total

# Summary for Subcatchment 5.0S: Northeast Corner

Runoff = 2.3 cfs @ 12.35 hrs, Volume= 0.265 af, Depth= 2.65"

_	A	rea (sf)	CN [	Description		
		52,286	70 \	Voods, Goo	od, HSG C	
		52,286	-	100.00% Pe	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	12.5	50	0.0200	0.07		Sheet Flow, A to B
	1.8	155	0.0840	1.45		Woods: Light underbrush n= 0.400 P2= 3.10" <b>Shallow Concentrated Flow, B to C</b> Woodland Kv= 5.0 fps
	9.4	200	0.0050	0.35		Shallow Concentrated Flow, C to D Woodland Kv= 5.0 fps
	23.7	405	Total			

#### Summary for Link POA-1: Adjacent House Lot

Inflow Area =	3.981 ac,	0.00% Impervious,	Inflow Depth = 3.1	1" for 25-YR event
Inflow =	11.0 cfs @	12.21 hrs, Volume	= 1.033 af	
Primary =	11.0 cfs @	12.21 hrs, Volume	= 1.033 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-2: Roadside Ditch

Inflow Area =	7.299 ac, 0	0.00% Impervious,	Inflow Depth = 2	2.83" for 25-YR event
Inflow =	17.2 cfs @	12.24 hrs, Volume	e= 1.722 a	af
Primary =	17.2 cfs @	12.24 hrs, Volume	e= 1.722 a	af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### **Summary for Link POA-3: South Wetlands**

Inflow Area =	5.991 ac, 0.00% lr	npervious, Inflow Depth =	2.65" for 25-YR event
Inflow =	15.5 cfs @ 12.16 h	rs, Volume= 1.32	2 af
Primary =	15.5 cfs @ 12.16 h	rs, Volume= 1.322	2 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-4: Southeast Wetlands

Inflow Area	=	23.003 ac,	0.00% Impervious,	Inflow Depth =	2.74"	for 25-YR event
Inflow	=	37.3 cfs @	12.53 hrs, Volum	e= 5.249	af	
Primary	=	37.3 cfs @	12.53 hrs, Volum	e= 5.249	af, Att	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-5: Northeast Wetlands

Inflow Area =	1.200 ac,	0.00% Impervious,	Inflow Depth = 2.6	5" for 25-YR event
Inflow =	2.3 cfs @	12.35 hrs, Volume	e= 0.265 af	
Primary =	2.3 cfs @	12.35 hrs, Volume	e= 0.265 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

<b>21397 Existing Conditions</b> Prepared by Sebago Technics, Inc HydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solutions	Type III 24-hr         2-YR Rainfall=3.10"           Printed         3/11/2022           S LLC         Page 7
Time span=0.00-60.00 hrs, dt=0.01 hrs Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond routir	, Weighted-CN
	sf 0.00% Impervious Runoff Depth=1.03" 15.0 min CN=75 Runoff=3.4 cfs 0.341 af
	sf 0.00% Impervious Runoff Depth=0.87" 17.4 min CN=72 Runoff=4.8 cfs 0.528 af
Subcatchment 3.0S: Central Area Draining Runoff Area=260,949 Flow Length=440' Tc=	sf 0.00% Impervious Runoff Depth=0.77" 11.2 min CN=70 Runoff=4.0 cfs 0.385 af
	sf 0.00% Impervious Runoff Depth=0.82" 7.7 min CN=71 Runoff=10.1 cfs 1.569 af
	sf 0.00% Impervious Runoff Depth=0.77" 23.7 min CN=70 Runoff=0.6 cfs 0.077 af
Link POA-1: Adjacent House Lot	Inflow=3.4 cfs 0.341 af Primary=3.4 cfs 0.341 af
Link POA-2: Roadside Ditch	Inflow=4.8 cfs 0.528 af Primary=4.8 cfs 0.528 af
Link POA-3: South Wetlands	Inflow=4.0 cfs 0.385 af Primary=4.0 cfs 0.385 af
Link POA-4: Southeast Wetlands	Inflow=10.1 cfs 1.569 af Primary=10.1 cfs 1.569 af
Link POA-5: Northeast Wetlands	Inflow=0.6 cfs 0.077 af Primary=0.6 cfs 0.077 af

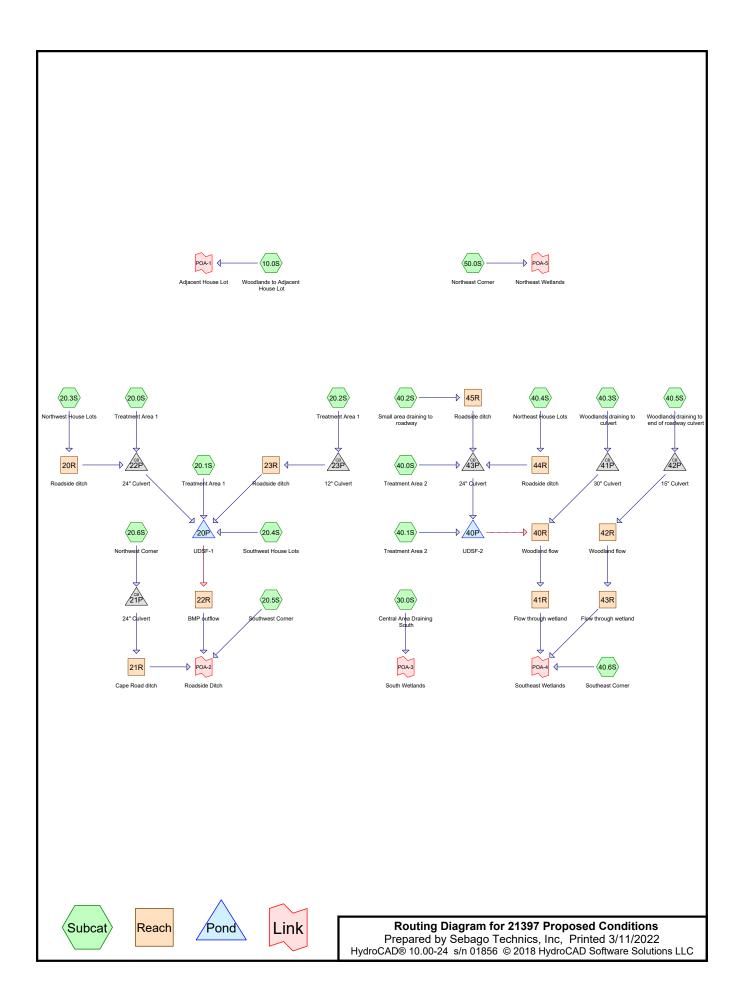
Total Runoff Area = 41.474 acRunoff Volume = 2.900 af<br/>100.00% Pervious = 41.474 acAverage Runoff Depth = 0.84"<br/>0.00% Impervious = 0.000 ac

<b>21397 Existing Conditions</b> Prepared by Sebago Technics, Inc HydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solution	Type III 24-hr         10-YR Rainfall=4.60"           Printed         3/11/2022           ns LLC         Page 8
Time span=0.00-60.00 hrs, dt=0.01 hr Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond rout	S, Weighted-CN
	2 sf 0.00% Impervious Runoff Depth=2.13" =15.0 min CN=75 Runoff=7.5 cfs 0.706 af
	3 sf 0.00% Impervious Runoff Depth=1.89" =17.4 min CN=72 Runoff=11.3 cfs 1.152 af
Subcatchment 3.0S: Central Area Draining Runoff Area=260,949 Flow Length=440' Tc=	9 sf 0.00% Impervious Runoff Depth=1.74" =11.2 min CN=70 Runoff=10.0 cfs 0.871 af
Subcatchment 4.0S: Eastern Half of Site Runoff Area=1,002,022 Flow Length=1,335' Tc=	2 sf 0.00% Impervious Runoff Depth=1.82" =37.7 min CN=71 Runoff=24.3 cfs 3.487 af
	6 sf   0.00% Impervious   Runoff Depth=1.74" c=23.7 min   CN=70   Runoff=1.5 cfs   0.175 af
Link POA-1: Adjacent House Lot	Inflow=7.5 cfs 0.706 af Primary=7.5 cfs 0.706 af
Link POA-2: Roadside Ditch	Inflow=11.3 cfs 1.152 af Primary=11.3 cfs 1.152 af
Link POA-3: South Wetlands	Inflow=10.0 cfs 0.871 af Primary=10.0 cfs 0.871 af
Link POA-4: Southeast Wetlands	Inflow=24.3 cfs 3.487 af Primary=24.3 cfs 3.487 af
Link POA-5: Northeast Wetlands	Inflow=1.5 cfs 0.175 af Primary=1.5 cfs 0.175 af

Total Runoff Area = 41.474 acRunoff Volume = 6.391 af<br/>100.00% Pervious = 41.474 acAverage Runoff Depth = 1.85"<br/>0.00% Impervious = 0.000 ac

# **Appendix 2B**

Proposed Conditions HydroCAD Summary



# Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
2.053	74	House lot >75% Grass cover, Good, HSG C (20.3S, 20.4S, 30.0S, 40.4S, 40.6S)
0.564	80	House lot >75% Grass cover, Good, HSG D (20.3S, 20.4S, 30.0S)
0.826	98	House lot impervious (20.3S, 20.4S, 30.0S, 40.4S, 40.6S)
0.970	98	Pavement (20.0S, 20.1S, 20.2S, 20.5S, 20.6S, 30.0S, 40.0S, 40.1S, 40.5S, 40.6S)
27.676	70	Woods, Good, HSG C (10.0S, 20.3S, 20.4S, 20.5S, 20.6S, 30.0S, 40.2S, 40.3S,
		40.4S, 40.5S, 40.6S, 50.0S)
7.083	77	Woods, Good, HSG D (10.0S, 20.3S, 20.5S, 20.6S, 30.0S, 40.3S, 40.6S)
1.981	72	Woods/grass comb., Good, HSG C (20.0S, 20.1S, 20.2S, 20.5S, 20.6S, 40.0S,
		40.1S, 40.3S, 40.5S, 40.6S)
0.321	79	Woods/grass comb., Good, HSG D (20.0S, 20.1S, 30.0S)
41.474	73	TOTAL AREA

# Summary for Subcatchment 10.0S: Woodlands to Adjacent House Lot

Runoff = 10.6 cfs @ 12.21 hrs, Volume= 1.000 af, Depth= 3.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

_	A	rea (sf)	CN I	Description		
		31,151			od, HSG C	
_		31,753		· · · · ·	od, HSG D	
		62,904		Neighted A		
	1	62,904		100.00% Pe	ervious Are	а
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	2.7	20	0.1500	0.12	<b>`</b>	Sheet Flow, A to B
						Woods: Light underbrush n= 0.400 P2= 3.10"
	0.8	80	0.1211	1.74		Shallow Concentrated Flow, B to C
						Woodland Kv= 5.0 fps
	2.7	110	0.0180	0.67		Shallow Concentrated Flow, C to D
	07	05	0 4 0 0 0	4 50		Woodland Kv= 5.0 fps
	0.7	65	0.1000	1.58		Shallow Concentrated Flow, D to E
	6.2	190	0.0105	0.51		Woodland Kv= 5.0 fps Shallow Concentrated Flow, E to F
	0.2	190	0.0105	0.51		Woodland Kv= 5.0 fps
	0.5	55	0.1640	2.02		Shallow Concentrated Flow, F to G
	0.0	00	5.1010	2.52		Woodland Kv= 5.0 fps
	1.4	60	0.0210	0.72		Shallow Concentrated Flow, G to H
						Woodland Kv= 5.0 fps
_						

15.0 580 Total

#### Summary for Subcatchment 20.0S: Treatment Area 1

Runoff = 2.4 cfs @ 12.14 hrs, Volume= 0.198 af, Depth= 3.91"

	Area (sf)	CN	Description
*	9,645	98	Pavement
	10,780	72	Woods/grass comb., Good, HSG C
	6,115	79	Woods/grass comb., Good, HSG D
	26,540	83	Weighted Average
	16,895		63.66% Pervious Area
	9,645		36.34% Impervious Area

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Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 HydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solutions LLC Page 4

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.3	15	0.0200	0.93		Sheet Flow, A to B
					Smooth surfaces n= 0.011 P2= 3.10"
5.0	335	0.0250	1.11		Shallow Concentrated Flow, B to C
					Short Grass Pasture Kv= 7.0 fps
5.3	625	0.0800	1.98		Shallow Concentrated Flow, C to D
					Short Grass Pasture Kv= 7.0 fps
10.6	975	Total			

#### Summary for Subcatchment 20.1S: Treatment Area 1

Runoff = 2.9 cfs @ 12.12 hrs, Volume= 0.226 af, Depth= 3.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

_	A	rea (sf)	CN [	Description								
*		8,979	98 F	Pavement								
		16,259			/oods/grass comb., Good, HSG C							
_		6,705	79 \	Noods/gras	ss comb., G	Good, HSG D						
		31,943	81 \	Neighted A	verage							
	22,964 71.89% Pervious Area											
		8,979		28.11% Imp	pervious Ar	ea						
	_				_							
	Tc	Length	Slope		Capacity	Description						
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	0.5	40	0.0300	1.33		Sheet Flow, A to B						
						Smooth surfaces n= 0.011 P2= 3.10"						
	2.5	165	0.0250	1.11		Shallow Concentrated Flow, B to C						
						Short Grass Pasture Kv= 7.0 fps						
	5.6	670	0.0800	1.98		Shallow Concentrated Flow, C to D						
						Short Grass Pasture Kv= 7.0 fps						
	8.6	875	Total									

#### Summary for Subcatchment 20.2S: Treatment Area 1

0.3 cfs @ 12.09 hrs, Volume= 0.023 af, Depth= 3.60" Runoff =

	Area (sf)	CN	Description				
*	1,046	98	Pavement				
	2,287	72	Woods/grass comb., Good, HSG C				
	3,333	80	Weighted Average				
	2,287		68.62% Pervious Area				
	1,046		31.38% Impervious Area				

TcLength (fteet)Slope (ft/ft)Velocity (ft/sec)Description (cfs)6.0Direct Entry, Direct EntrySummary for Subcatchment 20.3S: Northwest House LotsRunoff=8.7 cfs @ 12.15 hrs, Volume=0.727 af, Depth= 3.31"Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"0.00-60.00 hrs, dt= 0.01 hrs*12,00098House lot impervious*23,75074House lot >75% Grass cover, Good, HSG C*14,25080House lot >75% Grass cover, Good, HSG D39,74270Woods, Good, HSG D114,93677Weighted Average 89.56% Pervious Area12,00010.44% Impervious AreaTcLength Grass: Dense n= 0.2402.31450.04301.04Shallow Concentrated Flow, B to C WoodlandWoodlandKv= 5.0 fps	Prepare		bago Teo	chnics, Ind		Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 D Software Solutions LLC Page 5
Summary for Subcatchment 20.3S: Northwest House LotsRunoff= $8.7 \text{ cfs} @ 12.15 \text{ hrs}, Volume= 0.727 \text{ af}, Depth= 3.31"Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrsType III 24-hr 25-YR Rainfall=5.80"\frac{\text{Area}(\text{sf})}{2.3,750}CNDescription*12,00098House lot impervious* 23,75074House lot >75% Grass cover, Good, HSG C*14,25080House lot >75% Grass cover, Good, HSG D39,74270Yoods, Good, HSG C25,19477Woods, Good, HSG D114,93677Weighted Average102,93689.56% Pervious Area12,00010.44% Impervious AreaTcLengthSheet Flow, A to BGrass: Dense n = 0.2402.31450.04301.04Shallow Concentrated Flow, B to CWoodland Kv= 5.0 fps$		•		,		Description
$\begin{array}{rcl} {\sf Runoff} &=& 8.7  {\sf cfs} @& 12.15  {\sf hrs},  {\sf Volume} &=& 0.727  {\sf af},  {\sf Depth} = 3.31" \\ \\ {\sf Runoff} \ {\sf by} \ {\sf SCS} \ {\sf TR} - 20 \ {\sf method}, \ {\sf UH} = {\sf SCS}, \ {\sf Weighted} - {\sf CN}, \ {\sf Time} \ {\sf Span} = 0.00-60.00  {\sf hrs}, \ {\sf dt} = 0.01  {\sf hrs} \\ \\ {\sf Type} \ {\sf III} \ 24-{\sf hr} \ 25-{\sf YR} \ {\sf Rainfall} = 5.80" \\ \\ \hline $	6.0					Direct Entry, Direct Entry
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"			Summa	ary for S	ubcatchm	nent 20.3S: Northwest House Lots
Type III 24-hr 25-YR Rainfall=5.80"Area (sf)CNDescription*12,00098House lot impervious*23,75074House lot >75% Grass cover, Good, HSG C*14,25080House lot >75% Grass cover, Good, HSG D39,74270Woods, Good, HSG C25,19477Woods, Good, HSG D114,93677Weighted Average102,93689.56% Pervious Area12,00010.44% Impervious AreaTcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)8.4800.05000.16Sheet Flow, A to BGrass: Densen= 0.240P2= 3.10"2.31450.04301.04Shallow Concentrated Flow, B to C	Runoff	=	8.7 c	fs @ 12.1	5 hrs, Volu	lume= 0.727 af, Depth= 3.31"
*       12,000       98       House lot impervious         *       23,750       74       House lot >75% Grass cover, Good, HSG C         *       14,250       80       House lot >75% Grass cover, Good, HSG D         39,742       70       Woods, Good, HSG C         25,194       77       Woods, Good, HSG D         114,936       77       Weighted Average         102,936       89.56% Pervious Area         12,000       10.44% Impervious Area         Tc       Length       Slope       Velocity       Capacity         Minimital       (ft/ft)       (ft/sec)       (cfs)         8.4       80       0.0500       0.16       Sheet Flow, A to B         Grass: Dense       n= 0.240       P2= 3.10"         2.3       145       0.0430       1.04       Shallow Concentrated Flow, B to C					CS, Weigh	nted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs
*       23,750       74       House lot >75% Grass cover, Good, HSG C         *       14,250       80       House lot >75% Grass cover, Good, HSG D         39,742       70       Woods, Good, HSG C         25,194       77       Woods, Good, HSG D         114,936       77       Weighted Average         102,936       89.56% Pervious Area         12,000       10.44% Impervious Area         Tc< Length	-		CN D	Description		
*       14,250       80       House lot >75% Grass cover, Good, HSG D         39,742       70       Woods, Good, HSG C         25,194       77       Woods, Good, HSG D         114,936       77       Weighted Average         102,936       89.56% Pervious Area         12,000       10.44% Impervious Area         Tc       Length       Slope       Velocity       Capacity         (min)       (feet)       (ft/ft)       (ft/sec)       (cfs)         8.4       80       0.0500       0.16       Sheet Flow, A to B         Grass: Dense       n= 0.240       P2= 3.10"         2.3       145       0.0430       1.04       Shallow Concentrated Flow, B to C						
39,742         70         Woods, Good, HSG C           25,194         77         Woods, Good, HSG D           114,936         77         Weighted Average           102,936         89.56% Pervious Area           12,000         10.44% Impervious Area           Tc         Length         Slope         Velocity         Capacity           (min)         (feet)         (ft/ft)         (ft/sec)         (cfs)           8.4         80         0.0500         0.16         Sheet Flow, A to B           Grass: Dense         n= 0.240         P2= 3.10"           2.3         145         0.0430         1.04         Shallow Concentrated Flow, B to C	*	,				
25,194         77         Woods, Good, HSG D           114,936         77         Weighted Average           102,936         89.56% Pervious Area           12,000         10.44% Impervious Area           Tc         Length         Slope         Velocity         Capacity           (min)         (feet)         (ft/ft)         (ft/sec)         (cfs)           8.4         80         0.0500         0.16         Sheet Flow, A to B           Grass: Dense         n= 0.240         P2= 3.10"           2.3         145         0.0430         1.04         Shallow Concentrated Flow, B to C						
114,936         77         Weighted Average           102,936         89.56% Pervious Area           12,000         10.44% Impervious Area           Tc         Length         Slope         Velocity         Capacity         Description           (min)         (feet)         (ft/ft)         (ft/sec)         (cfs)         Impervious Area           8.4         80         0.0500         0.16         Sheet Flow, A to B         Grass: Dense         n= 0.240         P2= 3.10"           2.3         145         0.0430         1.04         Shallow Concentrated Flow, B to C         Woodland         Kv= 5.0 fps						
102,936         89.56% Pervious Area           12,000         10.44% Impervious Area           Tc         Length         Slope         Velocity         Capacity         Description           (min)         (feet)         (ft/ft)         (ft/sec)         (cfs)            8.4         80         0.0500         0.16         Sheet Flow, A to B         Grass: Dense         n= 0.240         P2= 3.10"           2.3         145         0.0430         1.04         Shallow Concentrated Flow, B to C         Woodland         Kv= 5.0 fps						
TcLengthSlopeVelocityCapacity (cfs)Description(min)(feet)(ft/ft)(ft/sec)(cfs)8.4800.05000.16Sheet Flow, A to B Grass: Dense n= 0.240 P2= 3.10"2.31450.04301.04Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps		,				3
(min)         (feet)         (ft/ft)         (ft/sec)         (cfs)           8.4         80         0.0500         0.16         Sheet Flow, A to B           Grass: Dense         n= 0.240         P2= 3.10"           2.3         145         0.0430         1.04           Shallow Concentrated Flow, B to C         Woodland         Kv= 5.0 fps		12,000	1	0.44% Imp	pervious Are	rea
2.3         145         0.0430         1.04         Grass: Dense         n=         0.240         P2=         3.10"           Shallow Concentrated Flow, B to C         Woodland         Kv=         5.0 fps		•				Description
2.3         145         0.0430         1.04         Shallow Concentrated Flow, B to C           Woodland         Kv= 5.0 fps	8.4	80	0.0500	0.16		
Woodland Kv= 5.0 fps						
	2.3	145	0.0430	1.04		
	10.7	225	Total			

# Summary for Subcatchment 20.4S: Southwest House Lots

Runoff = 3.0 cfs @ 12.13 hrs, Volume= 0.238 af, Depth= 3.40"

	Area (sf)	CN	Description			
*	6,000	98	louse lot impervious			
*	13,489	74	buse lot >75% Grass cover, Good, HSG C			
*	5,511	80	House lot >75% Grass cover, Good, HSG D			
	11,581	70	Woods, Good, HSG C			
	36,581	78	Weighted Average			
	30,581		83.60% Pervious Area			
	6,000		16.40% Impervious Area			

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	30	0.0667	0.10		Sheet Flow, A to B
1.8	170	0.0500	1.57		Woods: Light underbrush n= 0.400 P2= 3.10" <b>Shallow Concentrated Flow, B to C</b> Short Grass Pasture Kv= 7.0 fps
0.2	35	0.2800	2.65		Shallow Concentrated Flow, C to D
1.9	115	0.0200	0.99		Woodland Kv= 5.0 fps Shallow Concentrated Flow, D to E Short Grass Pasture Kv= 7.0 fps

9.0 350 Total

#### Summary for Subcatchment 20.5S: Southwest Corner

Runoff 7.5 cfs @ 12.12 hrs, Volume= 0.582 af, Depth= 2.74" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

A	rea (sf)	CN E	Description		
*	1,301	98 F	Pavement		
	3,062	72 V	Voods/gras	s comb., G	Good, HSG C
1	03,003	70 V	Voods, Go	od, HSG C	
	3,700	77 V	Voods, Go	od, HSG D	
1	11,066	71 V	Veighted A	verage	
1	09,765	9	8.83% Per	vious Area	
	1,301	1	.17% Impe	ervious Area	а
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.0	15	0.0667	0.08		Sheet Flow, A to B
					Woods: Light underbrush n= 0.400 P2= 3.10"
1.9	215	0.1440	1.90		Shallow Concentrated Flow, B to C
					Woodland Kv= 5.0 fps
1.8	65	0.0150	0.61		Shallow Concentrated Flow, C to D
	405		4.05		Woodland Kv= 5.0 fps
1.7	165	0.1091	1.65		Shallow Concentrated Flow, D to E
					Woodland Kv= 5.0 fps
8.4	460	Total			

#### Summary for Subcatchment 20.6S: Northwest Corner

2.9 cfs @ 12.14 hrs, Volume= Runoff = 0.232 af, Depth= 3.11"

Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 LLC Page 7

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	A	rea (sf)	CN [	Description		
*		1,406	98 F	Pavement		
		2,476	72 V	Noods/gras	s comb., G	Good, HSG C
		16,182	70 V	Voods, Go	od, HSG C	
		18,842	77 V	Voods, Go	od, HSG D	
		38,906	75 V	Veighted A	verage	
		37,500	ç	96.39% Per	vious Area	
		1,406	3	3.61% Impe	ervious Area	a
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	5.5	25	0.0400	0.08		Sheet Flow, A to B
						Woods: Light underbrush n= 0.400 P2= 3.10"
	0.4	60	0.2333	2.42		Shallow Concentrated Flow, B to C
						Woodland Kv= 5.0 fps
	2.0	70	0.0143	0.60		Shallow Concentrated Flow, C to D
						Woodland Kv= 5.0 fps
	0.2	40	0.3333	4.04		Shallow Concentrated Flow, D to E
	4.0	405	0 0000	1.00		Short Grass Pasture Kv= 7.0 fps
	1.6	105	0.0238	1.08		Shallow Concentrated Flow, E to F
	0.7		<b>T</b> ( )			Short Grass Pasture Kv= 7.0 fps

9.7 300 Total

# Summary for Subcatchment 30.0S: Central Area Draining South

Runoff = 13.5 cfs @ 12.19 hrs, Volume= 1.216 af, Depth= 2.83"

	Area (sf)	CN	Description
*	1,210	98	Pavement
	1,144	79	Woods/grass comb., Good, HSG D
*	6,000	98	House lot impervious
*	14,173	74	House lot >75% Grass cover, Good, HSG C
*	4,827	80	House lot >75% Grass cover, Good, HSG D
	183,821	70	Woods, Good, HSG C
	13,454	77	Woods, Good, HSG D
	224,629	72	Weighted Average
	217,419		96.79% Pervious Area
	7,210		3.21% Impervious Area

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Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 HydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solutions LLC Page 8

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	55	0.1091	0.13		Sheet Flow, A to B
2.5	130	0.0308	0.88		Woods: Light underbrush n= 0.400 P2= 3.10" <b>Shallow Concentrated Flow, B to C</b> Woodland Kv= 5.0 fps
0.9	95	0.1263	1.78		Shallow Concentrated Flow, C to D Woodland Kv= 5.0 fps
2.9	155	0.0323	0.90		Shallow Concentrated Flow, D to E Woodland Kv= 5.0 fps

13.2 435 Total

#### Summary for Subcatchment 40.0S: Treatment Area 2

Runoff 2.2 cfs @ 12.15 hrs, Volume= 0.185 af, Depth= 3.70" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

_	A	rea (sf)	CN E	escription							
*		9,523	98 F	avement							
		16,631	72 V	Voods/gras	/oods/grass comb., Good, HSG C						
		16,631	6	3.59% Per	vious Area						
		9,523	3	6.41% Imp	ervious Ar	ea					
	Тс	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	0.8	40	0.0100	0.85		Sheet Flow, A to B					
						Smooth surfaces n= 0.011 P2= 3.10"					
	10.6	445	0.0100	0.70		Shallow Concentrated Flow, B to C					
						Short Grass Pasture Kv= 7.0 fps					
	11.4	485	Total								

#### Summary for Subcatchment 40.1S: Treatment Area 2

Runoff = 2.6 cfs @ 12.09 hrs, Volume= 0.182 af, Depth= 3.50"

	Area (sf)	CN	Description			
*	6,830	98	Pavement			
	20,389	72	Woods/grass comb., Good, HSG C			
	27,219	79	Weighted Average			
	20,389		74.91% Pervious Area			
	6,830		25.09% Impervious Area			

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Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 HydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solutions LLC Page 9

_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.3	15	0.0200	0.93		Sheet Flow, A to B Smooth surfaces n= 0.011 P2= 3.10"
	1.2	100	0.0400	1.40		Shallow Concentrated Flow, B to C Short Grass Pasture Kv= 7.0 fps
	2.2	250	0.0700	1.85		Shallow Concentrated Flow, C to D
_	2.3					Short Grass Pasture Kv= 7.0 fps Direct Entry, Direct Entry
	6.0	365	Total			

# Summary for Subcatchment 40.2S: Small area draining to roadway

Runoff = 0.9 cfs @ 12.16 hrs, Volume= 0.077 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

A	rea (sf)	CN D	escription		
	15,145	70 V	Voods, Go	od, HSG C	
	15,145	1	00.00% Pe	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.6	60	0.1000	0.13		Sheet Flow, A to B
3.4	160	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 3.10" <b>Shallow Concentrated Flow, B to C</b> Woodland Kv= 5.0 fps
11.0	220	Total			

#### Summary for Subcatchment 40.3S: Woodlands draining to culvert

Runoff 12.1 cfs @ 12.49 hrs, Volume= 1.643 af, Depth= 2.74" =

Area (sf)	CN	Description
3,467	72	Woods/grass comb., Good, HSG C
262,666	70	Woods, Good, HSG C
47,526	77	Woods, Good, HSG D
313,659	71	Weighted Average
313,659		100.00% Pervious Area

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0.35

1.58

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.7	50	0.0300	0.08		Sheet Flow, A to B
					Woods: Light underbrush n= 0.400 P2= 3.10"
0.6	55	0.1000	1.58		Shallow Concentrated Flow, B to C
					Woodland Kv= 5.0 fps
7.1	400	0.0350	0.94		Shallow Concentrated Flow, C to D
					Woodland Kv= 5.0 fps
0.7	65	0.1000	1.58		Shallow Concentrated Flow, D to E

Woodland Kv= 5.0 fps

Woodland Kv= 5.0 fps

Woodland Kv= 5.0 fps

34.5 1,025 Total

13.7

1.7

#### Summary for Subcatchment 40.4S: Northeast House Lots

Runoff 6.4 cfs @ 12.19 hrs, Volume= =

290 0.0050

165 0.1000

0.585 af, Depth= 2.92"

Shallow Concentrated Flow, E to F

Shallow Concentrated Flow, F to G

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

_	Area (sf) CN Description										
*		9,000	98 H	8 House lot impervious							
*		28,500	74 H	4 House lot >75% Grass cover, Good, HSG C							
_		67,149	70 V	Voods, Go	od, HSG C						
	1	04,649	73 V	Veighted A	verage						
		95,649	9	1.40% Per	vious Area						
		9,000	8	.60% Impe	ervious Area	а					
	Тс	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	9.8	45	0.0300	0.08		Sheet Flow, A to B					
						Woods: Light underbrush n= 0.400 P2= 3.10"					
	2.2	175	0.0714	1.34		Shallow Concentrated Flow, B to C					
						Woodland Kv= 5.0 fps					
	1.6	110	0.0500	1.12		Shallow Concentrated Flow, C to D					
_						Woodland Kv= 5.0 fps					
	13.6	330	Total								

#### Summary for Subcatchment 40.5S: Woodlands draining to end of roadway culvert

2.6 cfs @ 12.19 hrs, Volume= 0.239 af, Depth= 2.65" Runoff =

 Type III 24-hr
 25-YR Rainfall=5.80"

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_	A	rea (sf)	CN [	Description		
*		518	98 F	Pavement		
		2,287	72 V	Voods/gras	s comb., G	Good, HSG C
_		44,381	70 V	Voods, Goo	od, HSG C	
		47,186	70 V	Veighted A	verage	
	46,668 98.90% Pervious Area					
		518 1.10% Impervious Area				
	Тс	Length		Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.5	50	0.0400	0.09		Sheet Flow, A to B
						Woods: Light underbrush n= 0.400 P2= 3.10"
	4.2	350	0.0771	1.39		Shallow Concentrated Flow, B to C
_						Woodland Kv= 5.0 fps
	13.7	400	Total			
_	(min) 9.5 4.2	(feet) 50 350	0.0771	(ft/sec) 0.09	Capacity (cfs)	Woods: Light underbrush n= 0.400 P2= 3.10" Shallow Concentrated Flow, B to C

# Summary for Subcatchment 40.6S: Southeast Corner

2.460 af, Depth= 2.74"

Runoff =	18.9 cfs @	12.47 hrs,	Volume=
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	A	rea (sf)	CN [	Description					
*		1,782	98 F	Pavement					
		8,663	72 \						
*		3,000	98 H	louse lot ir	npervious				
*		9,500	74 H	louse lot >	75% Grass	s cover, Good, HSG C			
	3	78,473	70 \	Voods, Go	od, HSG C				
		68,068	77 \	Noods, Go	od, HSG D				
	4	69,486		Veighted A	0				
	4	64,704	ę	98.98% Pei	vious Area				
		4,782		l.02% Impe	ervious Area	а			
	_		-						
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	9.6	40	0.0250	0.07		Sheet Flow, A to B			
						Woods: Light underbrush n= 0.400 P2= 3.10"			
	1.0	80	0.0690	1.31		Shallow Concentrated Flow, B to C			
		~~~	o o / o <del> 7</del>			Woodland Kv= 5.0 fps			
	1.5	60	0.0167	0.65		Shallow Concentrated Flow, C to D			
	1.0	450	0 0700	4.05		Woodland Kv= 5.0 fps			
	1.8	150	0.0733	1.35		Shallow Concentrated Flow, D to E			
	17.0	200	0.0050	0.05		Woodland Kv= 5.0 fps			
	17.9	380	0.0050	0.35		Shallow Concentrated Flow, E to F			
_	01.0	740	<b></b>			Woodland Kv= 5.0 fps			
	31.8	710	Total						

#### Summary for Subcatchment 50.0S: Northeast Corner

Runoff = 2.3 cfs @ 12.35 hrs, Volume= 0.265 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=5.80"

A	rea (sf)	CN I	Description		
	52,286	70 \	Woods, Go	od, HSG C	
	52,286		100.00% Pe	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	,	Capacity (cfs)	Description
12.5	50	0.0200	0.07		Sheet Flow, A to B Woods: Light underbrush n= 0.400 P2= 3.10"
1.8	155	0.0840	1.45		Shallow Concentrated Flow, B to C Woodland Kv= 5.0 fps
9.4	200	0.0050	0.35		Shallow Concentrated Flow, C to D Woodland Kv= 5.0 fps
00.7	405	Tatal			

23.7 405 Total

#### Summary for Reach 20R: Roadside ditch

Inflow Area	a =	2.639 ac, 10.44% Impervious	, Inflow Depth = 3.31" for	or 25-YR event
Inflow	=	8.7 cfs @ 12.15 hrs, Volur	ne= 0.727 af	
Outflow	=	8.7 cfs @ 12.16 hrs, Volur	ne= 0.727 af, Atten	= 1%, Lag= 0.9 min

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 7.09 fps, Min. Travel Time= 1.2 min Avg. Velocity = 2.21 fps, Avg. Travel Time= 3.9 min

Peak Storage= 629 cf @ 12.16 hrs Average Depth at Peak Storage= 0.39' Bank-Full Depth= 0.50' Flow Area= 1.8 sf, Capacity= 14.3 cfs

2.00' x 0.50' deep channel, n= 0.025 Earth, clean & winding Side Slope Z-value= 3.0 '/' Top Width= 5.00' Length= 515.0' Slope= 0.0796 '/' Inlet Invert= 355.00', Outlet Invert= 314.00'



#### Summary for Reach 21R: Cape Road ditch

Inflow Area = 0.893 ac, 3.61% Impervious, Inflow Depth = 3.11" for 25-YR event 2.9 cfs @ 12.14 hrs. Volume= Inflow 0.232 af = 2.8 cfs  $\overline{\textcircled{0}}$  12.15 hrs, Volume= Outflow = 0.232 af, Atten= 1%, Lag= 0.9 min Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 4.32 fps, Min. Travel Time= 1.4 min Avg. Velocity = 1.29 fps, Avg. Travel Time= 4.6 min Peak Storage= 234 cf @ 12.15 hrs Average Depth at Peak Storage= 0.19' Bank-Full Depth= 1.00' Flow Area= 6.0 sf, Capacity= 66.1 cfs 3.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 9.00' Length= 355.0' Slope= 0.0479 '/' Inlet Invert= 307.00', Outlet Invert= 290.00' ‡ Summary for Reach 22R: BMP outflow Inflow Area = 4.897 ac, 17.66% Impervious, Inflow Depth = 3.46" for 25-YR event 11.0 cfs @ 12.29 hrs. Volume= Inflow = 1.412 af Outflow = 11.0 cfs @ 12.30 hrs, Volume= 1.412 af, Atten= 0%, Lag= 0.5 min Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 4.89 fps, Min. Travel Time= 0.7 min Avg. Velocity = 1.18 fps, Avg. Travel Time= 3.0 min Peak Storage= 471 cf @ 12.30 hrs Average Depth at Peak Storage= 0.37' Bank-Full Depth= 0.50' Flow Area= 3.3 sf, Capacity= 18.9 cfs 5.00' x 0.50' deep channel, n= 0.035 Earth, dense weeds Side Slope Z-value = 3.0 '/' Top Width = 8.00' Length= 210.0' Slope= 0.0643 '/' Inlet Invert= 304.50', Outlet Invert= 291.00' ‡

#### Summary for Reach 23R: Roadside ditch

Inflow Area = 0.077 ac, 31.38% Impervious, Inflow Depth = 3.60" for 25-YR event 0.3 cfs @ 12.09 hrs. Volume= Inflow 0.023 af = 0.3 cfs @ 12.14 hrs, Volume= Outflow = 0.023 af, Atten= 17%, Lag= 3.3 min Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 2.10 fps, Min. Travel Time= 6.5 min Avg. Velocity = 0.60 fps, Avg. Travel Time= 22.7 min Peak Storage= 104 cf @ 12.14 hrs Average Depth at Peak Storage= 0.06' Bank-Full Depth= 0.50' Flow Area= 1.8 sf, Capacity= 12.6 cfs 2.00' x 0.50' deep channel, n= 0.025 Earth, clean & winding Side Slope Z-value= 3.0 '/' Top Width= 5.00' Length= 820.0' Slope= 0.0622 '/' Inlet Invert= 365.00', Outlet Invert= 314.00' ‡ Summary for Reach 40R: Woodland flow

Inflow Area	=	11.176 ac,	5.21% Imperviou	is, Inflow Depth =	2.87"	for 25-YR event
Inflow =	=	18.2 cfs @	12.46 hrs, Volu	ime= 2.67	3 af	
Outflow =	=	18.1 cfs @	12.48 hrs, Volu	ime= 2.67	3 af, Att	en= 1%, Lag= 1.2 min

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 1.95 fps, Min. Travel Time= 2.7 min Avg. Velocity = 0.43 fps, Avg. Travel Time= 12.3 min

Peak Storage= 2,923 cf @ 12.48 hrs Average Depth at Peak Storage= 0.39' Bank-Full Depth= 0.50' Flow Area= 12.5 sf, Capacity= 28.3 cfs

20.00' x 0.50' deep channel, n= 0.070 Sluggish weedy reaches w/pools Side Slope Z-value= 10.0 '/' Top Width= 30.00' Length= 315.0' Slope= 0.0365 '/' Inlet Invert= 343.50', Outlet Invert= 332.00'

‡

#### Summary for Reach 41R: Flow through wetland

 Inflow Area =
 11.176 ac, 5.21% Impervious, Inflow Depth = 2.87" for 25-YR event

 Inflow =
 18.1 cfs @
 12.48 hrs, Volume=
 2.673 af

 Outflow =
 17.7 cfs @
 12.55 hrs, Volume=
 2.673 af, Atten= 2%, Lag= 4.4 min

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 0.47 fps, Min. Travel Time= 5.3 min Avg. Velocity = 0.09 fps, Avg. Travel Time= 27.8 min

Peak Storage= 5,600 cf @ 12.55 hrs Average Depth at Peak Storage= 0.24' Bank-Full Depth= 0.50' Flow Area= 77.5 sf, Capacity= 58.6 cfs

150.00' x 0.50' deep channel, n= 0.070 Sluggish weedy reaches w/pools Side Slope Z-value= 10.0 '/' Top Width= 160.00' Length= 150.0' Slope= 0.0033 '/' Inlet Invert= 332.00', Outlet Invert= 331.50'



#### Summary for Reach 42R: Woodland flow

 Inflow Area =
 1.083 ac, 1.10% Impervious, Inflow Depth = 2.65" for 25-YR event

 Inflow =
 2.6 cfs @
 12.19 hrs, Volume=
 0.239 af

 Outflow =
 2.6 cfs @
 12.22 hrs, Volume=
 0.239 af, Atten= 2%, Lag= 1.5 min

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 2.05 fps, Min. Travel Time= 2.2 min Avg. Velocity = 0.57 fps, Avg. Travel Time= 7.7 min

Peak Storage= 331 cf @ 12.22 hrs Average Depth at Peak Storage= 0.11' Bank-Full Depth= 0.25' Flow Area= 3.1 sf, Capacity= 10.3 cfs

10.00' x 0.25' deep channel, n= 0.040 Mountain streams Side Slope Z-value= 10.0 '/' Top Width= 15.00' Length= 265.0' Slope= 0.0642 '/' Inlet Invert= 350.00', Outlet Invert= 333.00'

‡

#### Summary for Reach 43R: Flow through wetland

 Inflow Area =
 1.083 ac, 1.10% Impervious, Inflow Depth = 2.65" for 25-YR event

 Inflow =
 2.6 cfs @
 12.22 hrs, Volume=
 0.239 af

 Outflow =
 1.2 cfs @
 12.56 hrs, Volume=
 0.239 af, Atten= 54%, Lag= 20.4 min

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 0.14 fps, Min. Travel Time= 44.1 min Avg. Velocity = 0.03 fps, Avg. Travel Time= 186.8 min

Peak Storage= 3,104 cf @ 12.56 hrs Average Depth at Peak Storage= 0.08' Bank-Full Depth= 0.50' Flow Area= 52.5 sf, Capacity= 24.7 cfs

100.00' x 0.50' deep channel, n= 0.070 Sluggish weedy reaches w/pools Side Slope Z-value= 10.0 '/' Top Width= 110.00' Length= 380.0' Slope= 0.0013 '/' Inlet Invert= 332.00', Outlet Invert= 331.50'



#### Summary for Reach 44R: Roadside ditch

 Inflow Area =
 2.402 ac,
 8.60% Impervious, Inflow Depth =
 2.92" for 25-YR event

 Inflow =
 6.4 cfs @
 12.19 hrs, Volume=
 0.585 af

 Outflow =
 6.4 cfs @
 12.21 hrs, Volume=
 0.585 af, Atten= 1%, Lag= 1.2 min

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 3.93 fps, Min. Travel Time= 1.7 min Avg. Velocity = 1.33 fps, Avg. Travel Time= 4.9 min

Peak Storage= 640 cf @ 12.21 hrs Average Depth at Peak Storage= 0.47' Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 29.6 cfs

2.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 8.00' Length= 395.0' Slope= 0.0152 '/' Inlet Invert= 357.00', Outlet Invert= 351.00'

‡

#### Summary for Reach 45R: Roadside ditch

Inflow Area = 0.348 ac, 0.00% Impervious, Inflow Depth = 2.65" for 25-YR event 0.9 cfs @ 12.16 hrs. Volume= Inflow 0.077 af = Outflow 0.9 cfs @ 12.16 hrs, Volume= = 0.077 af, Atten= 0%, Lag= 0.4 min Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Max. Velocity= 3.57 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.15 fps, Avg. Travel Time= 2.0 min Peak Storage= 35 cf @ 12.16 hrs Average Depth at Peak Storage= 0.11' Bank-Full Depth= 1.00' Flow Area= 5.0 sf, Capacity= 61.4 cfs 2.00' x 1.00' deep channel, n= 0.022 Earth, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 8.00' Length= 138.0' Slope= 0.0652 '/' Inlet Invert= 361.00', Outlet Invert= 352.00' ‡

Summary for Pond 20P: UDSF-1

Inflow Area =	4.897 ac, 17.66% Impervious, Inflow Depth = 3.46" for 25-YR event	
Inflow =	16.9 cfs @ 12.15 hrs, Volume= 1.412 af	
Outflow =	11.0 cfs @ 12.29 hrs, Volume= 1.412 af, Atten= 35%, Lag= 8.9 min	
Primary =	8.1 cfs @ 12.29 hrs, Volume= 1.369 af	
Secondary =	2.8 cfs @ 12.29 hrs, Volume= 0.043 af	

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 311.43' @ 12.29 hrs Surf.Area= 5,382 sf Storage= 14,067 cf

Plug-Flow detention time= 80.3 min calculated for 1.412 af (100% of inflow) Center-of-Mass det. time= 80.3 min ( 904.2 - 823.9 )

Volume	Invert	Avail	.Storage Stor	age Description	
#1	308.00'	1	17,244 cf Cus	tom Stage Data (P	rismatic)Listed below (Recalc)
Elevation (feet)	Sur	f.Area (sq-ft)	Inc.Store (cubic-feet		
308.00		2,916	(	) 0	
309.00		3,565	3,24 <sup>-</sup>	,	
309.50		3,910	1,869	,	
310.00		4,270	2,04	5 7,154	
311.00		5,033	4,652	2 11,806	
311.50		5,435	2,617	7 14,423	
312.00		5,851	2,822	2 17,244	

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Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 Page 18

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Device	Routing	Invert	Outlet Devices
#1	Primary	305.17'	12.0" Round Culvert
	-		L= 65.6' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 305.17' / 304.50' S= 0.0102 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	305.67'	1.4" Vert. Header Pipe Orifice C= 0.600
#3	Device 1	309.00'	18.0" W x 8.0" H Vert. OCS Orifice C= 0.600
#4	Device 1	311.00'	2.5" x 2.5" Horiz. OCS Grate X 6.00 columns X 6 rows C= 0.600
			Limited to weir flow at low heads
#5	Secondary	311.20'	
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=8.1 cfs @ 12.29 hrs HW=311.43' (Free Discharge)

-1=Culvert (Barrel Controls 8.1 cfs @ 10.36 fps)

2=Header Pipe Orifice (Passes < 0.1 cfs potential flow)

-3=OCS Orifice (Passes < 7.0 cfs potential flow)

-4=OCS Grate (Passes < 5.0 cfs potential flow)

Secondary OutFlow Max=2.8 cfs @ 12.29 hrs HW=311.43' (Free Discharge) 5=Emergency Spillway (Weir Controls 2.8 cfs @ 1.21 fps)

#### Summary for Pond 21P: 24" Culvert

Inflow Area =	0.893 ac, 3.61% Impervious, Inflow I	Depth = 3.11" for 25-YR event
Inflow =	2.9 cfs @ 12.14 hrs, Volume=	0.232 af
Outflow =	2.9 cfs @ 12.14 hrs, Volume=	0.232 af, Atten= 0%, Lag= 0.0 min
Primary =	2.9 cfs @ 12.14 hrs, Volume=	0.232 af

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 308.81' @ 12.14 hrs Flood Elev= 311.50'

Device Routing Invert Outlet Devices	
#1 Primary 308.00' <b>24.0" Round Culvert</b> L= 57.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 308.00' / 307.40' S= 0.0105 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf	

**Primary OutFlow** Max=2.9 cfs @ 12.14 hrs HW=308.81' (Free Discharge) **1=Culvert** (Inlet Controls 2.9 cfs @ 2.42 fps)

#### Summary for Pond 22P: 24" Culvert

Inflow Area =	3.248 ac, 15.30% Impervious,	Inflow Depth = 3.42" for 25-YR event
Inflow =	11.0 cfs @ 12.16 hrs, Volume	= 0.925 af
Outflow =	11.0 cfs @ 12.16 hrs, Volume	= 0.925 af, Atten= 0%, Lag= 0.0 min
Primary =	11.0 cfs @ 12.16 hrs, Volume	= 0.925 af

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

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Peak Elev= 312.84' @ 12.16 hrs Flood Elev= 315.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	311.00'	<b>24.0" Round Culvert</b> L= 56.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 311.00' / 310.50' S= 0.0089 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

**Primary OutFlow** Max=11.0 cfs @ 12.16 hrs HW=312.84' (Free Discharge) **1=Culvert** (Inlet Controls 11.0 cfs @ 3.64 fps)

#### Summary for Pond 23P: 12" Culvert

Inflow Area =	0.077 ac, 31.38% Impervious, Inflow I	Depth = 3.60" for 25-YR event
Inflow =	0.3 cfs @ 12.09 hrs, Volume=	0.023 af
Outflow =	0.3 cfs @ 12.09 hrs, Volume=	0.023 af, Atten= 0%, Lag= 0.0 min
Primary =	0.3 cfs @ 12.09 hrs, Volume=	0.023 af

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 366.32' @ 12.09 hrs Flood Elev= 368.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	366.00'	<b>12.0" Round Culvert</b> L= 58.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 366.00' / 365.50' S= 0.0086 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.3 cfs @ 12.09 hrs HW=366.32' (Free Discharge) -1=Culvert (Inlet Controls 0.3 cfs @ 1.51 fps)

#### Summary for Pond 40P: UDSF-2

Inflow Area =	3.975 ac, 14.64% Impervious, Inflow De	epth = 3.11" for 25-YR event
Inflow =	10.9 cfs @ 12.17 hrs, Volume=	1.030 af
Outflow =	6.4 cfs @ 12.42 hrs, Volume=	1.030 af, Atten= 42%, Lag= 14.6 min
Primary =	6.4 cfs @ 12.42 hrs, Volume=	1.030 af
Secondary =	0.0 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 350.29' @ 12.42 hrs Surf.Area= 4,525 sf Storage= 11,092 cf

Plug-Flow detention time= 88.9 min calculated for 1.029 af (100% of inflow) Center-of-Mass det. time= 89.0 min (923.3 - 834.3)

Volume	Invert	Avail.Storage	Storage Description
#1	347.00'	14,521 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

#### 21397 Proposed Conditions

Type III 24-hr 25-YR Rainfall=5.80" Printed 3/11/2022 LLC Page 20

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Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
347.0	)0	2,327	0	0	
348.0	00	2,930	2,629	2,629	
348.5	50	3,252	1,546	4,174	
349.0		3,589	1,710	5,884	
350.0		4,304	3,947	9,831	
351.0	00	5,076	4,690	14,521	
Device	Routing	Invert	Outlet Devices		
#1	Primary	344.17'	12.0" Round (		
					neadwall, Ke= 0.500
					343.75' S= 0.0105 '/' Cc= 0.900
#2	Device 1	244 67	1.2" Vert. Head		poth interior, Flow Area= 0.79 sf
#3	Device 1	348.00'			<b>Drifice</b> C= 0.600
#4	Device 1	350.25'			<b>X 6.00 columns</b> X 6 rows C= 0.600
щr			Limited to weir		
#5	Secondar	y 350.30'	Head (feet) 0.2	20 0.40 0.60	<b>mergency Spillway</b> 0.80 1.00 1.20 1.40 1.60 70 2.69 2.68 2.69 2.67 2.64

**Primary OutFlow** Max=6.3 cfs @ 12.42 hrs HW=350.29' (Free Discharge)

-**1=Culvert** (Passes 6.3 cfs of 8.9 cfs potential flow)

-2=Header Pipe Orifice (Orifice Controls 0.1 cfs @ 11.36 fps)

-3=OCS Orifice (Orifice Controls 5.6 cfs @ 6.72 fps)

-4=OCS Grate (Weir Controls 0.7 cfs @ 0.62 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=347.00' (Free Discharge) 5=Emergency Spillway ( Controls 0.0 cfs)

#### Summary for Pond 41P: 30" Culvert

Inflow Area =	7.201 ac, 0.00% Impe	ervious, Inflow Depth = 2	.74" for 25-YR event
Inflow =	12.1 cfs @ 12.49 hrs,	Volume= 1.643 a	f
Outflow =	12.1 cfs @ 12.49 hrs,	Volume= 1.643 a	f, Atten= 0%, Lag= 0.0 min
Primary =	12.1 cfs @ 12.49 hrs,	Volume= 1.643 a	f

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 349.17' @ 12.49 hrs Flood Elev= 354.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	347.50'	<b>30.0" Round Culvert</b> L= 105.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 347.50' / 346.00' S= 0.0143 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 4.91 sf

**Primary OutFlow** Max=12.1 cfs @ 12.49 hrs HW=349.17' (Free Discharge) **1=Culvert** (Inlet Controls 12.1 cfs @ 3.48 fps)

#### Summary for Pond 42P: 15" Culvert

 Inflow Area =
 1.083 ac, 1.10% Impervious, Inflow Depth = 2.65" for 25-YR event

 Inflow =
 2.6 cfs @ 12.19 hrs, Volume=
 0.239 af

 Outflow =
 2.6 cfs @ 12.19 hrs, Volume=
 0.239 af, Atten= 0%, Lag= 0.0 min

 Primary =
 2.6 cfs @ 12.19 hrs, Volume=
 0.239 af

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 355.45' @ 12.19 hrs Flood Elev= 357.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	354.50'	15.0" Round Culvert
			L= 53.4' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 354.50' / 352.30' S= 0.0412 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=2.6 cfs @ 12.19 hrs HW=355.45' (Free Discharge) -1=Culvert (Inlet Controls 2.6 cfs @ 2.62 fps)

#### Summary for Pond 43P: 24" Culvert

Inflow Area	a =	3.351 ac, 12.69% Impervious, Inflow Depth = 3.03" for 25-YR event
Inflow	=	9.3 cfs @ 12.19 hrs, Volume= 0.847 af
Outflow	=	9.3 cfs @ 12.19 hrs, Volume= 0.847 af, Atten= 0%, Lag= 0.0 min
Primary	=	9.3 cfs @ 12.19 hrs, Volume= 0.847 af

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 351.59' @ 12.19 hrs Flood Elev= 353.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	350.20'	24.0" Round Culvert
			L= 56.5' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 350.20' / 349.50' S= 0.0124 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=9.2 cfs @ 12.19 hrs HW=351.59' (Free Discharge) ☐ 1=Culvert (Barrel Controls 9.2 cfs @ 5.57 fps)

#### Summary for Link POA-1: Adjacent House Lot

Inflow Area =	3.740 ac, 0.00°	% Impervious, Inflov	v Depth = 3.21"	for 25-YR event
Inflow =	10.6 cfs @ 12.2	21 hrs, Volume=	1.000 af	
Primary =	10.6 cfs @ 12.2	21 hrs, Volume=	1.000 af, Att	ten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-2: Roadside Ditch

Inflow Area	ı =	8.340 ac, 1	1.11% Impervious,	Inflow Depth =	3.20"	for 25-YR event
Inflow	=	17.2 cfs @	12.27 hrs, Volum	e= 2.226	af	
Primary	=	17.2 cfs @	12.27 hrs, Volum	e= 2.226	af, At	tten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-3: South Wetlands

Inflow Area =	5.157 ac,	3.21% Impervious,	Inflow Depth = 2.8	3" for 25-YR event
Inflow =	13.5 cfs @	12.19 hrs, Volume	= 1.216 af	
Primary =	13.5 cfs @	12.19 hrs, Volume	= 1.216 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-4: Southeast Wetlands

Inflow Are	a =	23.037 ac,	3.05% Impervious,	Inflow Depth = 2	2.80"	for 25-YR event
Inflow	=	37.3 cfs @	12.50 hrs, Volume	e= 5.371 a	af	
Primary	=	37.3 cfs @	12.50 hrs, Volume	e= 5.371 a	af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

#### Summary for Link POA-5: Northeast Wetlands

Inflow Area	=	1.200 ac,	0.00% Impervious,	Inflow Depth = 2	2.65" for 25-YR	event
Inflow	=	2.3 cfs @	12.35 hrs, Volume	e= 0.265 a	af	
Primary	=	2.3 cfs @	12.35 hrs, Volume	e= 0.265 a	af, Atten=0%, La	ag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment 10.0S: Woodlands to	Runoff Area=162,904 sf 0.00% Impervious Runoff Depth=1.08" Flow Length=580' Tc=15.0 min CN=76 Runoff=3.4 cfs 0.338 af
Subcatchment 20.0S: Treatment Area 1	Runoff Area=26,540 sf 36.34% Impervious Runoff Depth=1.53" Flow Length=975' Tc=10.6 min CN=83 Runoff=0.9 cfs 0.078 af
Subcatchment 20.1S: Treatment Area 1	Runoff Area=31,943 sf 28.11% Impervious Runoff Depth=1.39" Flow Length=875' Tc=8.6 min CN=81 Runoff=1.1 cfs 0.085 af
Subcatchment 20.2S: Treatment Area 1	Runoff Area=3,333 sf 31.38% Impervious Runoff Depth=1.33" Tc=6.0 min CN=80 Runoff=0.1 cfs 0.008 af
Subcatchment 20.3S: Northwest House	Runoff Area=114,936 sf 10.44% Impervious Runoff Depth=1.14" Flow Length=225' Tc=10.7 min CN=77 Runoff=2.9 cfs 0.251 af
Subcatchment 20.4S: Southwest House	Runoff Area=36,581 sf 16.40% Impervious Runoff Depth=1.20" Flow Length=350' Tc=9.0 min CN=78 Runoff=1.0 cfs 0.084 af
Subcatchment 20.5S: Southwest Corner	Runoff Area=111,066 sf 1.17% Impervious Runoff Depth=0.82" Flow Length=460' Tc=8.4 min CN=71 Runoff=2.0 cfs 0.174 af
Subcatchment 20.6S: Northwest Corner	Runoff Area=38,906 sf 3.61% Impervious Runoff Depth=1.03" Flow Length=300' Tc=9.7 min CN=75 Runoff=0.9 cfs 0.076 af
Subcatchment 30.0S: Central Area	Runoff Area=224,629 sf 3.21% Impervious Runoff Depth=0.87" Flow Length=435' Tc=13.2 min CN=72 Runoff=3.8 cfs 0.373 af
Subcatchment 40.0S: Treatment Area 2 Flow Length=485'	Runoff Area=26,154 sf 36.41% Impervious Runoff Depth=1.39" Slope=0.0100 '/' Tc=11.4 min CN=81 Runoff=0.8 cfs 0.070 af
Subcatchment 40.1S: Treatment Area 2	Runoff Area=27,219 sf 25.09% Impervious Runoff Depth=1.26" Flow Length=365' Tc=6.0 min CN=79 Runoff=0.9 cfs 0.066 af
	to Runoff Area=15,145 sf 0.00% Impervious Runoff Depth=0.77" Flow Length=220' Tc=11.0 min CN=70 Runoff=0.2 cfs 0.022 af
Subcatchment 40.3S: Woodlands draining	Runoff Area=313,659 sf 0.00% Impervious Runoff Depth=0.82" ow Length=1,025' Tc=34.5 min CN=71 Runoff=3.3 cfs 0.491 af
	<b>ts</b> Runoff Area=104,649 sf 8.60% Impervious Runoff Depth=0.92" Flow Length=330' Tc=13.6 min CN=73 Runoff=1.9 cfs 0.184 af
Subcatchment 40.5S: Woodlands draining	Runoff Area=47,186 sf 1.10% Impervious Runoff Depth=0.77" Flow Length=400' Tc=13.7 min CN=70 Runoff=0.7 cfs 0.070 af
Subcatchment 40.6S: Southeast Corner	Runoff Area=469,486 sf 1.02% Impervious Runoff Depth=0.82" Flow Length=710' Tc=31.8 min CN=71 Runoff=5.1 cfs 0.735 af

<b>21397 Proposed Conditions</b> Prepared by Sebago Technics, In <u>HydroCAD® 10.00-24 s/n 01856 © 20</u>	
Subcatchment 50.0S: Northeast Co	orner Runoff Area=52,286 sf 0.00% Impervious Runoff Depth=0.77" Flow Length=405' Tc=23.7 min CN=70 Runoff=0.6 cfs 0.077 af
Reach 20R: Roadside ditch	Avg. Flow Depth=0.21' Max Vel=5.10 fps Inflow=2.9 cfs 0.251 af 0.025 L=515.0' S=0.0796 '/' Capacity=14.3 cfs Outflow=2.9 cfs 0.251 af
Reach 21R: Cape Road ditch	Avg. Flow Depth=0.09' Max Vel=2.87 fps Inflow=0.9 cfs 0.076 af 0.022 L=355.0' S=0.0479 '/' Capacity=66.1 cfs Outflow=0.9 cfs 0.076 af
Reach 22R: BMP outflow	Avg. Flow Depth=0.18' Max Vel=3.16 fps Inflow=3.1 cfs 0.506 af 0.035 L=210.0' S=0.0643 '/' Capacity=18.9 cfs Outflow=3.1 cfs 0.506 af
Reach 23R: Roadside ditch	Avg. Flow Depth=0.03' Max Vel=1.38 fps Inflow=0.1 cfs 0.008 af 0.025 L=820.0' S=0.0622 '/' Capacity=12.6 cfs Outflow=0.1 cfs 0.008 af
Reach 40R: Woodland flow n=(	Avg. Flow Depth=0.18' Max Vel=1.24 fps Inflow=5.0 cfs 0.833 af 0.070 L=315.0' S=0.0365 '/' Capacity=28.3 cfs Outflow=4.9 cfs 0.833 af
Reach 41R: Flow through wetland n=(	Avg. Flow Depth=0.11' Max Vel=0.28 fps Inflow=4.9 cfs 0.833 af 0.070 L=150.0' S=0.0033 '/' Capacity=58.6 cfs Outflow=4.6 cfs 0.833 af
Reach 42R: Woodland flow n=(	Avg. Flow Depth=0.05' Max Vel=1.23 fps Inflow=0.7 cfs 0.070 af 0.040 L=265.0' S=0.0642 '/' Capacity=10.3 cfs Outflow=0.6 cfs 0.070 af
Reach 43R: Flow through wetland n=(	Avg. Flow Depth=0.03' Max Vel=0.07 fps Inflow=0.6 cfs 0.070 af 0.070 L=380.0' S=0.0013 '/' Capacity=24.7 cfs Outflow=0.2 cfs 0.070 af
Reach 44R: Roadside ditch n=0	Avg. Flow Depth=0.24' Max Vel=2.74 fps Inflow=1.9 cfs 0.184 af 0.022 L=395.0' S=0.0152 '/' Capacity=29.6 cfs Outflow=1.8 cfs 0.184 af
Reach 45R: Roadside ditch n=0	Avg. Flow Depth=0.05' Max Vel=2.20 fps Inflow=0.2 cfs 0.022 af 0.022 L=138.0' S=0.0652 '/' Capacity=61.4 cfs Outflow=0.2 cfs 0.022 af
Pond 20P: UDSF-1 Prima	Peak Elev=309.74' Storage=6,060 cf Inflow=5.9 cfs 0.506 af ry=3.1 cfs 0.506 af Secondary=0.0 cfs 0.000 af Outflow=3.1 cfs 0.506 af
<b>Pond 21P: 24" Culvert</b> 24.	Peak Elev=308.44' Inflow=0.9 cfs 0.076 af .0" Round Culvert n=0.013 L=57.0' S=0.0105 '/' Outflow=0.9 cfs 0.076 af
Pond 22P: 24" Culvert 24.	Peak Elev=311.94' Inflow=3.8 cfs 0.328 af .0" Round Culvert n=0.013 L=56.0' S=0.0089 '/' Outflow=3.8 cfs 0.328 af
Pond 23P: 12" Culvert 12.	Peak Elev=366.19' Inflow=0.1 cfs 0.008 af .0" Round Culvert n=0.013 L=58.0' S=0.0086 '/' Outflow=0.1 cfs 0.008 af
Pond 40P: UDSF-2 Prima	Peak Elev=348.55' Storage=4,329 cf Inflow=3.3 cfs 0.342 af ry=1.7 cfs 0.342 af Secondary=0.0 cfs 0.000 af Outflow=1.7 cfs 0.342 af
Pond 41P: 30" Culvert 30.0	Peak Elev=348.31' Inflow=3.3 cfs 0.491 af "Round Culvert n=0.013 L=105.0' S=0.0143 '/' Outflow=3.3 cfs 0.491 af
Pond 42P: 15" Culvert 15.	Peak Elev=354.93' Inflow=0.7 cfs 0.070 af .0" Round Culvert n=0.013 L=53.4' S=0.0412 '/' Outflow=0.7 cfs 0.070 af

<b>21397 Proposed Conditio</b> Prepared by Sebago Technic HydroCAD® 10.00-24 s/n 01856	•••	24-hr 2-YR Rainfall=3.10" Printed 3/11/2022 Page 25
Pond 43P: 24" Culvert	Peak Elev=3 24.0" Round Culvert n=0.013 L=56.5' S=0.012	50.90' Inflow=2.8 cfs 0.276 af 24 '/' Outflow=2.8 cfs 0.276 af
Link POA-1: Adjacent House L	_ot	Inflow=3.4 cfs 0.338 af
		Primary=3.4 cfs 0.338 af
Link POA-2: Roadside Ditch		Inflow=4.7 cfs 0.756 af
		Primary=4.7 cfs 0.756 af
Link POA-3: South Wetlands		Inflow=3.8 cfs 0.373 af
		Primary=3.8 cfs 0.373 af
Link POA-4: Southeast Wetlan	hde	Inflow=9.3 cfs 1.638 af
Link i OA-4. Oouncust Wettan		Primary=9.3 cfs 1.638 af
Link POA-5: Northeast Wetlan	de	Inflow=0.6 cfs 0.077 af
LIIK FOA-5. NOI LIEAST WELIAII	uə	Primary=0.6 cfs 0.077 af
		-

Total Runoff Area = 41.474 acRunoff Volume = 3.182 afAverage Runoff Depth = 0.92"95.67% Pervious = 39.678 ac4.33% Impervious = 1.796 ac

Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment 10.0S: Woodlands to	Runoff Area=162,904 sf 0.00% Impervious Runoff Depth=2.21" Flow Length=580' Tc=15.0 min CN=76 Runoff=7.3 cfs 0.689 af
Subcatchment 20.0S: Treatment Area 1	Runoff Area=26,540 sf 36.34% Impervious Runoff Depth=2.81" Flow Length=975' Tc=10.6 min CN=83 Runoff=1.7 cfs 0.143 af
Subcatchment 20.1S: Treatment Area 1	Runoff Area=31,943 sf 28.11% Impervious Runoff Depth=2.63" Flow Length=875' Tc=8.6 min CN=81 Runoff=2.1 cfs 0.161 af
Subcatchment 20.2S: Treatment Area 1	Runoff Area=3,333 sf 31.38% Impervious Runoff Depth=2.55" Tc=6.0 min CN=80 Runoff=0.2 cfs 0.016 af
Subcatchment 20.3S: Northwest House	Runoff Area=114,936 sf 10.44% Impervious Runoff Depth=2.29" Flow Length=225' Tc=10.7 min CN=77 Runoff=6.0 cfs 0.504 af
Subcatchment 20.4S: Southwest House	Runoff Area=36,581 sf 16.40% Impervious Runoff Depth=2.38" Flow Length=350' Tc=9.0 min CN=78 Runoff=2.1 cfs 0.166 af
Subcatchment 20.5S: Southwest Corner	Runoff Area=111,066 sf 1.17% Impervious Runoff Depth=1.82" Flow Length=460' Tc=8.4 min CN=71 Runoff=4.9 cfs 0.387 af
Subcatchment 20.6S: Northwest Corner	Runoff Area=38,906 sf 3.61% Impervious Runoff Depth=2.13" Flow Length=300' Tc=9.7 min CN=75 Runoff=2.0 cfs 0.158 af
Subcatchment 30.0S: Central Area	Runoff Area=224,629 sf 3.21% Impervious Runoff Depth=1.89" Flow Length=435' Tc=13.2 min CN=72 Runoff=8.9 cfs 0.814 af
Subcatchment 40.0S: Treatment Area 2 Flow Length=485	Runoff Area=26,154 sf 36.41% Impervious Runoff Depth=2.63" Slope=0.0100 '/' Tc=11.4 min CN=81 Runoff=1.6 cfs 0.132 af
Subcatchment 40.1S: Treatment Area 2	Runoff Area=27,219 sf 25.09% Impervious Runoff Depth=2.46" Flow Length=365' Tc=6.0 min CN=79 Runoff=1.8 cfs 0.128 af
Subcatchment 40.2S: Small area draining	<b>to</b> Runoff Area=15,145 sf 0.00% Impervious Runoff Depth=1.74" Flow Length=220' Tc=11.0 min CN=70 Runoff=0.6 cfs 0.051 af
Subcatchment 40.3S: Woodlands draining F	Runoff Area=313,659 sf 0.00% Impervious Runoff Depth=1.82" low Length=1,025' Tc=34.5 min CN=71 Runoff=7.9 cfs 1.092 af
Subcatchment 40.4S: Northeast House Lo	<b>ts</b> Runoff Area=104,649 sf 8.60% Impervious Runoff Depth=1.97" Flow Length=330' Tc=13.6 min CN=73 Runoff=4.3 cfs 0.395 af
Subcatchment 40.5S: Woodlands draining	Runoff Area=47,186 sf 1.10% Impervious Runoff Depth=1.74" Flow Length=400' Tc=13.7 min CN=70 Runoff=1.7 cfs 0.158 af
Subcatchment 40.6S: Southeast Corner	Runoff Area=469,486 sf 1.02% Impervious Runoff Depth=1.82" Flow Length=710' Tc=31.8 min CN=71 Runoff=12.4 cfs 1.634 af

# **21397 Proposed Conditions**TypePrepared by Sebago Technics, IncHydroCAD® 10.00-24 s/n 01856 © 2018 HydroCAD Software Solutions LLC

Type III 24-hr 10-YR Rainfall=4.60" Printed 3/11/2022

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Subcatchment 50.0S: Northeast Corner	Runoff Area=52,286 sf 0.00% Impervious Runoff Depth=1.74 Flow Length=405' Tc=23.7 min CN=70 Runoff=1.5 cfs 0.175 at
Reach 20R: Roadside ditch n=0.025	Avg. Flow Depth=0.32' Max Vel=6.37 fps Inflow=6.0 cfs 0.504 at L=515.0' S=0.0796 '/' Capacity=14.3 cfs Outflow=6.0 cfs 0.504 at
Reach 21R: Cape Road ditch n=0.022	Avg. Flow Depth=0.15' Max Vel=3.78 fps Inflow=2.0 cfs 0.158 at L=355.0' S=0.0479 '/' Capacity=66.1 cfs Outflow=1.9 cfs 0.158 at
Reach 22R: BMP outflow n=0.035	Avg. Flow Depth=0.26' Max Vel=4.00 fps Inflow=6.0 cfs 0.990 at L=210.0' S=0.0643 '/' Capacity=18.9 cfs Outflow=6.0 cfs 0.990 at
Reach 23R: Roadside ditch n=0.025	Avg. Flow Depth=0.05' Max Vel=1.83 fps Inflow=0.2 cfs 0.016 at L=820.0' S=0.0622 '/' Capacity=12.6 cfs Outflow=0.2 cfs 0.016 at
Reach 40R: Woodland flow n=0.070	Avg. Flow Depth=0.31' Max Vel=1.70 fps Inflow=12.2 cfs 1.797 at L=315.0' S=0.0365 '/' Capacity=28.3 cfs Outflow=12.1 cfs 1.797 at
Reach 41R: Flow through wetland n=0.070	Avg. Flow Depth=0.19' Max Vel=0.41 fps Inflow=12.1 cfs 1.797 at L=150.0' S=0.0033 '/' Capacity=58.6 cfs Outflow=11.9 cfs 1.797 at
Reach 42R: Woodland flow n=0.040	Avg. Flow Depth=0.09' Max Vel=1.75 fps Inflow=1.7 cfs 0.158 af L=265.0' S=0.0642 '/' Capacity=10.3 cfs Outflow=1.6 cfs 0.158 af
Reach 43R: Flow through wetland n=0.070	Avg. Flow Depth=0.06' Max Vel=0.11 fps Inflow=1.6 cfs 0.158 af L=380.0' S=0.0013 '/' Capacity=24.7 cfs Outflow=0.6 cfs 0.158 af
Reach 44R: Roadside ditch n=0.022	Avg. Flow Depth=0.38' Max Vel=3.50 fps Inflow=4.3 cfs 0.395 at L=395.0' S=0.0152 '/' Capacity=29.6 cfs Outflow=4.2 cfs 0.395 at
Reach 45R: Roadside ditch n=0.022	Avg. Flow Depth=0.08' Max Vel=3.07 fps Inflow=0.6 cfs 0.051 at L=138.0' S=0.0652 '/' Capacity=61.4 cfs Outflow=0.6 cfs 0.051 at
Pond 20P: UDSF-1 Primary=6.0	Peak Elev=310.85' Storage=11,062 cf Inflow=11.8 cfs 0.990 at 0 cfs 0.990 af Secondary=0.0 cfs 0.000 af Outflow=6.0 cfs 0.990 af
Pond 21P: 24" Culvert 24.0" R	Peak Elev=308.66' Inflow=2.0 cfs 0.158 at ound Culvert n=0.013 L=57.0' S=0.0105 '/' Outflow=2.0 cfs 0.158 at
Pond 22P: 24" Culvert 24.0" R	Peak Elev=312.42' Inflow=7.7 cfs 0.647 at ound Culvert n=0.013 L=56.0' S=0.0089 '/' Outflow=7.7 cfs 0.647 at
Pond 23P: 12" Culvert 12.0" R	Peak Elev=366.26' Inflow=0.2 cfs 0.016 at ound Culvert n=0.013 L=58.0' S=0.0086 '/' Outflow=0.2 cfs 0.016 at
Pond 40P: UDSF-2 Primary=4.3	Peak Elev=349.45' Storage=7,579 cf Inflow=7.4 cfs 0.705 at 3 cfs 0.705 af Secondary=0.0 cfs 0.000 af Outflow=4.3 cfs 0.705 af
Pond 41P: 30" Culvert 30.0" Ro	Peak Elev=348.80' Inflow=7.9 cfs 1.092 at und Culvert n=0.013 L=105.0' S=0.0143 '/' Outflow=7.9 cfs 1.092 at
Pond 42P: 15" Culvert 15.0" R	Peak Elev=355.22' Inflow=1.7 cfs 0.158 at ound Culvert n=0.013 L=53.4' S=0.0412 '/' Outflow=1.7 cfs 0.158 at

<b>21397 Proposed Conditions</b> Prepared by Sebago Technics, Inc HydroCAD® 10.00-24 s/n 01856 © 2018 Hydro	<i>Type III 24-hr 10-YR Rainfall=4.60"</i> Printed 3/11/2022 CAD Software Solutions LLC Page 28
Pond 43P: 24" Culvert 24.0" Roun	Peak Elev=351.29' Inflow=6.2 cfs 0.577 af nd Culvert n=0.013 L=56.5' S=0.0124 '/' Outflow=6.2 cfs 0.577 af
Link POA-1: Adjacent House Lot	Inflow=7.3 cfs  0.689 af Primary=7.3 cfs  0.689 af
Link POA-2: Roadside Ditch	Inflow=11.3 cfs 1.535 af Primary=11.3 cfs 1.535 af
Link POA-3: South Wetlands	Inflow=8.9 cfs  0.814 af Primary=8.9 cfs  0.814 af
Link POA-4: Southeast Wetlands	Inflow=24.3 cfs 3.588 af Primary=24.3 cfs 3.588 af
Link POA-5: Northeast Wetlands	Inflow=1.5 cfs 0.175 af Primary=1.5 cfs 0.175 af
Total Dunoff Area = 41 474 a	- Runoff Volume = 6 904 of Average Runoff Denth = 4 07"

Total Runoff Area = 41.474 acRunoff Volume = 6.801 afAverage Runoff Depth = 1.97"95.67% Pervious = 39.678 ac4.33% Impervious = 1.796 ac

### Inspection, Maintenance and Housekeeping Plan



#### INSPECTION, MAINTENANCE, AND HOUSEKEEPING PLAN

For: Raymond Cape Road Subdivision Raymond, Maine

By: Sebago Technics, Inc. 75 John Roberts Road, Suite 4A South Portland, Maine

#### Introduction

The following plan outlines the anticipated inspection and maintenance procedures for the erosion and sedimentation control measures as well as stormwater management facilities for the project. This plan also outlines several housekeeping requirements that shall be followed during and after construction. These procedures shall be followed in order to ensure the intended function of the designed measures and to prevent unreasonably adverse impacts to the surrounding environment.

The procedures outlined in this Inspection, Maintenance and Housekeeping Plan are provided as an overview of the anticipated practices to be used on this site. In some instances, additional measures may be required due to unexpected conditions. For additional detail on any of the erosion and sedimentation control measures or stormwater management devices to be utilized on this project, refer to the most recently revised edition of the "Maine Erosion and Sedimentation Control BMP" manual and/or the "Stormwater Management for Maine: Best Management Practices" manual as published by the Maine Department of Environmental Protection (MDEP).

#### **During Construction**

- 1. **Inspection:** During the construction process, it is the Contractor's responsibility to comply with the inspection and maintenance procedures outlined in this section. These responsibilities include inspecting disturbed and impervious areas, erosion control measures, materials storage areas that are exposed to precipitation, and locations where vehicles enter or exit the site. These areas shall be inspected at least once a week as well as before and after a storm event (0.5" of rainfall), and prior to completing permanent stabilization measures. A person with knowledge of erosion and stormwater control, including the standards and conditions in any applicable permits, shall conduct the inspections.
- 2. **Maintenance:** All measures shall be maintained in an effective operating condition until areas are permanently stabilized. If Best Management Practices (BMPs) need to be maintained or modified, additional BMPs are necessary, or other corrective action is needed, implementation must be completed within 7 calendar days and prior to any storm event (0.5" of rainfall).
- 3. **Documentation:** A log summarizing the inspections and any corrective action taken must be maintained on-site. The log must include the name(s) and qualifications of the person making the inspections, the date(s) of the inspections, and major observations about the operation and maintenance of erosion and sedimentation controls, material storage areas, and vehicle access

points to the site. Major observations must include BMPs that need maintenance, BMPs that failed to operate as designed or proved inadequate for a particular location, and locations where additional BMPs are needed. For each BMP requiring maintenance, BMP needing replacement, and location needing additional BMPs, note in the log the corrective action taken and when it was taken. The log must be made accessible to the appropriate regulatory agency upon request. The permittee shall retain a copy of the log for a period of at least three years from the completion of permanent stabilization.

4. **Specific Inspection and Maintenance Tasks:** The following is a list of erosion control and stormwater management measures and the specific inspection and maintenance tasks to be performed during construction.

#### A. <u>Sediment Barriers:</u>

- Hay bale barriers, silt fences, and filter berms shall be inspected immediately after each rainfall and at least daily during prolonged rainfall.
- If the fabric on a silt fence or filter barrier should decompose or become ineffective prior to the end of the expected usable life and the barrier is still necessary, it shall be replaced.
- Sediment deposits should be removed after each storm event (0.5" of rainfall). They must be removed before deposits reach approximately one-half the height of the barrier.
- Filter berms shall be reshaped as needed.
- Any sediment deposits remaining in place after the silt fence or filter barrier is no longer required should be dressed to conform to the existing grade, prepared, and seeded.

#### B. <u>Riprap Materials:</u>

- Once a riprap installation has been completed, it should require very little maintenance. It shall, however, be inspected periodically to determine if high flows have caused scour beneath the riprap or dislodged any of the stone.
- C. <u>Erosion Control Blankets:</u>
  - Inspect these reinforced areas semi-annually and after significant rainfall events for slumping, sliding, seepage, and scour. Pay close attention to unreinforced areas adjacent to the erosion control blankets, which may experience accelerated erosion.
  - Review all applicable inspection and maintenance procedures recommended by the specific blanket manufacturer. These tasks shall be included in addition to the requirements of this plan.
- D. <u>Stabilized Construction Entrances/Exits:</u>
  - The exit shall be maintained in a condition that will prevent tracking of sediment onto public rights-of-way.
  - When the control pad becomes ineffective, the stone shall be removed along with the collected soil material. The entrance should then be reconstructed.

• Areas that have received mud-tracking or sediment deposits shall be swept or washed. Washing shall be done on an area stabilized with aggregate, which drains into an approved sediment-trapping device (not into storm drains, ditches, or waterways).

### E. <u>Temporary Seed and Mulch:</u>

- Mulched areas should be inspected after rain events to check for rill erosion.
- If less than 90% of the soil surface is covered by mulch, additional mulch shall be applied in bare areas.
- In applications where seeding and mulch have been applied in conjunction with erosion control blankets, the blankets must be inspected after rain events for dislocation or undercutting.
- Mulch shall continue to be reapplied until 95% of the soil surface has established temporary vegetative cover.
- F. <u>Stabilized Temporary Drainage Swales:</u>
  - Sediment accumulation in the swale shall be removed once the cross section of the swale is reduced by 25%.
  - The swales shall be inspected after rainfall events. Any evidence of sloughing of the side slopes or channel erosion shall be repaired and corrective action should be taken to prevent reoccurrence of the problem.
  - In addition to the stabilized lining of the channel (i.e. erosion control blankets), stone check dams may be needed to further reduce channel velocity.
- 5. **Housekeeping:** The following general performance standards apply to the proposed project.
  - A. <u>Spill prevention</u>: Controls must be used to prevent pollutants from being discharged from materials on-site, including storage practices to minimize exposure of the materials to stormwater, and appropriate spill prevention, containment, and response planning and implementation.
  - B. <u>Groundwater protection</u>: During construction, liquid petroleum products and other hazardous materials with the potential to contaminate groundwater may not be stored or handled in areas of the site draining to an infiltration area. An "infiltration area" is any area of the site that by design or as a result of soils, topography and other relevant factors, accumulates runoff that infiltrates into the soil. Dikes, berms, sumps, and other forms of secondary containment that prevent discharge to groundwater may be used to isolate portions of the site for the purposes of storage and handling of these materials.
  - C. <u>Fugitive sediment and dust</u>: Actions must be taken to ensure that activities do not result in noticeable erosion of soils or fugitive dust emissions during or after construction. Oil may not be used for dust control.
  - D. <u>Debris and other materials</u>: Litter, construction debris, and chemicals exposed to stormwater must be prevented from becoming a pollutant source.

E. <u>Trench or foundation dewatering</u>: Trench dewatering is the removal of water from trenches, foundations, cofferdams, ponds, and other areas within the construction area that retain water after excavation. In most cases, the collected water is heavily silted and hinders correct and safe construction practices. The collected water must be removed from the ponded area, either through gravity or pumping, and must be spread through natural wooded buffers or removed to areas that are specifically designed to collect the maximum amount of sediment possible, like a cofferdam sedimentation basin. Avoid allowing the water to flow over disturbed areas of the site. Equivalent measures may be taken if approved.

#### Post-Construction

- 1. **Inspection:** After construction, it is the responsibility of the owner or assigned heirs to comply with the inspection and maintenance procedures outlined in this section. All measures must be maintained in effective operating condition. The owner shall inspect and maintain the BMPs, including but not limited to any parking areas, catch basins, drainage swales, detention basins and ponds, pipes and related structures, in accordance with all municipal and state inspection, cleaning and maintenance requirements of the approved post-construction stormwater management plan.
- 2. **Specific Inspection and Maintenance Tasks:** The following is a list of permanent erosion control and stormwater management measures and the inspection and maintenance tasks to be performed after construction. If the BMP requires maintenance, repair or replacement to function as intended by the approved post-construction stormwater management plan, the owner or operator of the BMP shall take corrective action(s) to address the deficiency or deficiencies as soon as possible after the deficiency is discovered and shall provide a record of the deficiency and corrective action(s) to the local municipality in the annual report.

#### A. <u>Vegetated Areas:</u>

- Inspect vegetated areas, particularly slopes and embankments, early in the growing season or after heavy rains (>0.5") to identify active or potential erosion problems.
- Replant bare areas or areas with sparse growth. Where rill erosion is evident, armor the area with an appropriate lining or divert the erosive flows to on-site areas able to withstand the concentrated flows.
- B. <u>Ditches, Swales and Other Open Channels:</u>
  - Inspect ditches, swales, level spreaders and other open stormwater channels in the spring, in the late fall, and after heavy rains to remove any obstructions to flow. Remove accumulated sediments and debris, remove woody vegetative growth that could obstruct flow, and repair any erosion of the ditch lining.
  - Vegetated ditches must be mowed at least annually or otherwise maintained to control the growth of woody vegetation and maintain flow capacity.
  - Any woody vegetation growing through riprap linings must also be removed. Repair any slumping side slopes as soon as practicable.
  - If the ditch has a riprap lining, replace riprap in areas where any underlying filter

fabric or underdrain gravel is showing through the stone or where stones have dislodged.

- C. <u>Culverts:</u>
  - Inspect culverts in the spring, in the late fall, and after heavy rains (>0.5") to remove any obstructions to flow.
  - Remove accumulated sediments and debris at the inlet, at the outlet, and within the conduit.
  - Inspect and repair any erosion damage at the culvert's inlet and outlet.
- D. <u>Removal of Winter Sand:</u>
  - Clear accumulations of winter sand in parking lots and along roadways at least once a year, preferably in the spring.
  - Accumulations on pavement may be removed by pavement sweeping.
  - Accumulations of sand along road shoulders may be removed by grading excess sand to the pavement edge and removing it manually or by a front-end loader or other acceptable method.

### E. <u>Grassed Underdrained Soil Filter:</u>

- The soil filter outlet structure and outlet of the soil filter should be checked periodically to ensure that flow structures are not blocked by debris. All ditches or pipes connecting soil filters in series should be checked for debris that may obstruct flow. Inspections should be conducted monthly during wet weather conditions from March to November.
- The soil filter and outlet should be inspected bi-annually for erosion, destabilization of side slopes, embankment settling and other signs of structural failure. Any signs of erosion shall be immediately repaired to assure stability and proper function.
- The soil filter will be inspected on a bi-annual basis to assure that significant sediment accumulation has not occurred in the pond outlet structure. Whenever the filter bed is inundated with sediment, the accumulated sediment shall be removed and property disposed of.

### 3. Documentation:

- A. The owner or operator of a BMP or a qualified post-construction stormwater inspector hired by that person, shall, as required by the local municipality, provide a completed and signed certification on a form provided by the local municipality, certifying that the person has inspected the BMP(s) and that they are adequately maintained and functioning as intended by the approved post-construction stormwater management plan, or that they required maintenance or repair, including the record of the deficiency and corrective action(s) taken.
- B. A log summarizing the inspections and any corrective action taken must be maintained. The log must include the name(s) and qualifications of the person making the inspections, the

date(s) of the inspections, and major observations about the operation and maintenance of controls. Major observations must include BMPs that need maintenance, BMPs that failed to operate as designed or proved inadequate for a particular location, and locations where additional BMPs are needed. For each BMP requiring maintenance, BMP needing replacement, and location needing additional BMPs, note in the log the corrective action taken and when it was taken. The log must be made accessible to the appropriate regulatory agency upon request. A sample "Stormwater Inspection and Maintenance Form" has been included as Attachment 1 of this Inspection, Maintenance, and Housekeeping Plan.

4. Duration of Maintenance: Perform maintenance as described and required for any associated permits unless and until the system is formally accepted by a municipality or quasi-municipal district, or is placed under the jurisdiction of a legally created association that will be responsible for the maintenance of the system. If a municipality or quasi-municipal district chooses to accept a stormwater management system, or a component of a stormwater system, it must provide a letter to the MDEP stating that it assumes responsibility for the system. The letter must specify the components of the system for which the municipality or district will assume responsibility, and that the municipality or district agrees to maintain those components of the system in compliance with MDEP standards. Upon such assumption of responsibility, and approval by the MDEP, the municipality, quasi-municipal district, or association becomes a co-permittee for this purpose only and must comply with all terms and conditions of the permit.

#### Attachments:

Attachment 1 – Sample Stormwater Inspection and Maintenance Forms

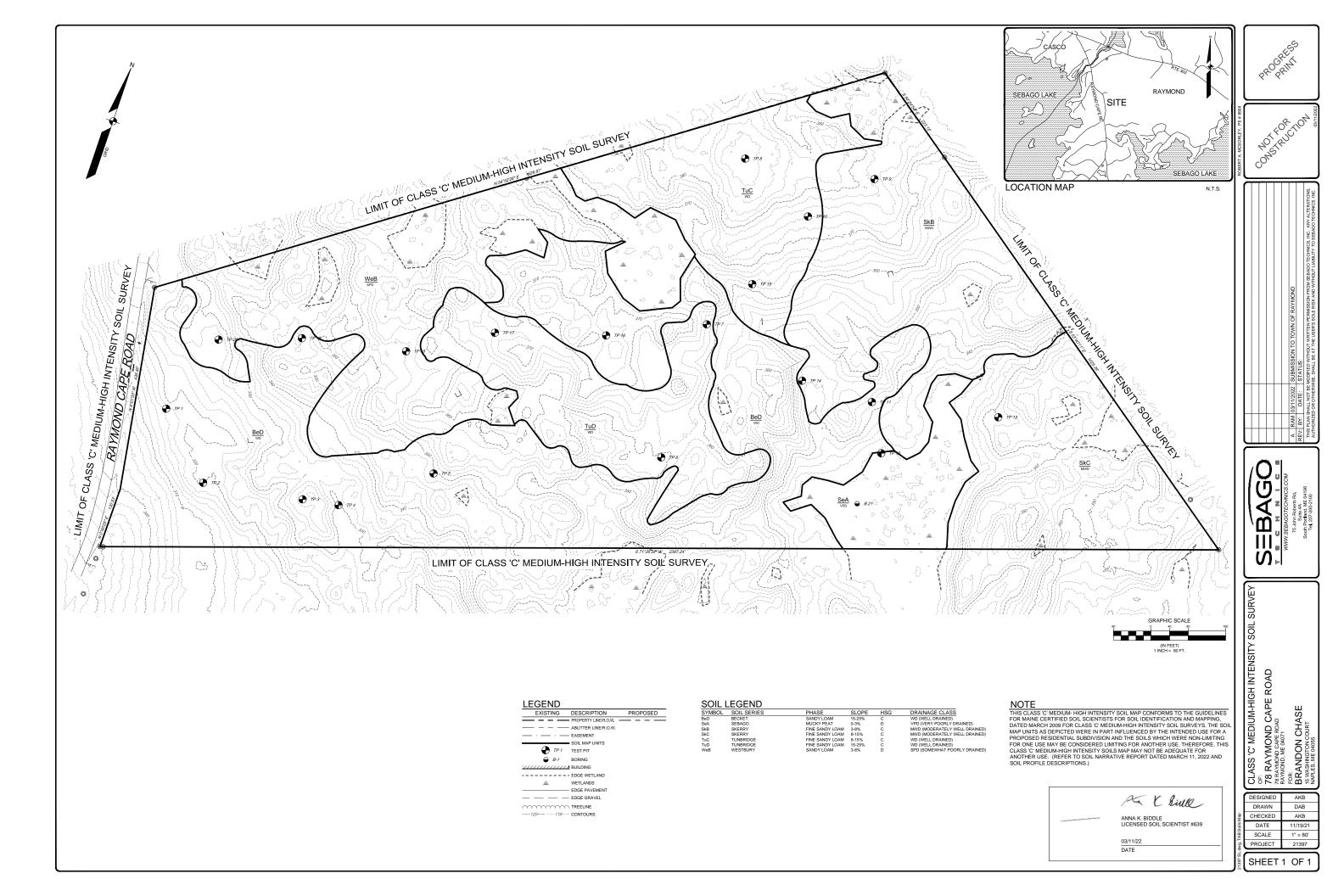
#### **General Site**

	INSPECTION MAINTER	NANCE AND HOUSEKEEPING FORM	
General Information			
Project Name:		Inspection Date:	
Project Location:		Current Weather:	
		Date / Amount Last Precip:	
BMP Owner:		Company conducting inspection:	
Owner Mailing Address:		Company Mailing Address	
Owner Phone #:		Company Phone #:	
Owner Email:		Inspector Name:	
		Inspector Email:	
Inspection Notes			
Site Element	Suggested Maintenance (recm'd frequency)	Observations	Inspection Notes/Recommended Action
	Inspect Slopes/Embankments for erosion		
Vegetated Areas	(annually) Replant bare areas or areas of sparse		
Ditches/Swales	growth (annually) Remove obstructions/debris/sediment (monthly)		
Dicites	Inspect for erosion/repair as needed (annually)		
	Remove woody vegetation (annually)		
	Mow vegetated ditches (annually)		
Catch Basins	Remove sediment/debris from sump (annually)		
	Remove accumulated debris from inlet grate		
Culverts	Remove sediment/debris from inlet/outlet aprons (annually)		
	Inspect inlet/outlet aprons for erosion, repair as needed (annually)		
	Inspect, repair as needed, riprap aprons for dislodged/sparse coverage (annually)		
Pipe Outlets	Remove sediment/debris from outlet aprons (annually)		
	Inspect outlet aprons for erosion, repair as needed (annually)		
	Inspect, repair as needed, riprap aprons for dislodged/sparse coverage (annually)		
Inspector shall reference t Engineers for a full list of ir	ne current edition of the Maine Erosion and nspection items.	Sediment Control Best Management	Practices (BMPs) Manual for Designers and
Additional Notes/Observati	ons:		

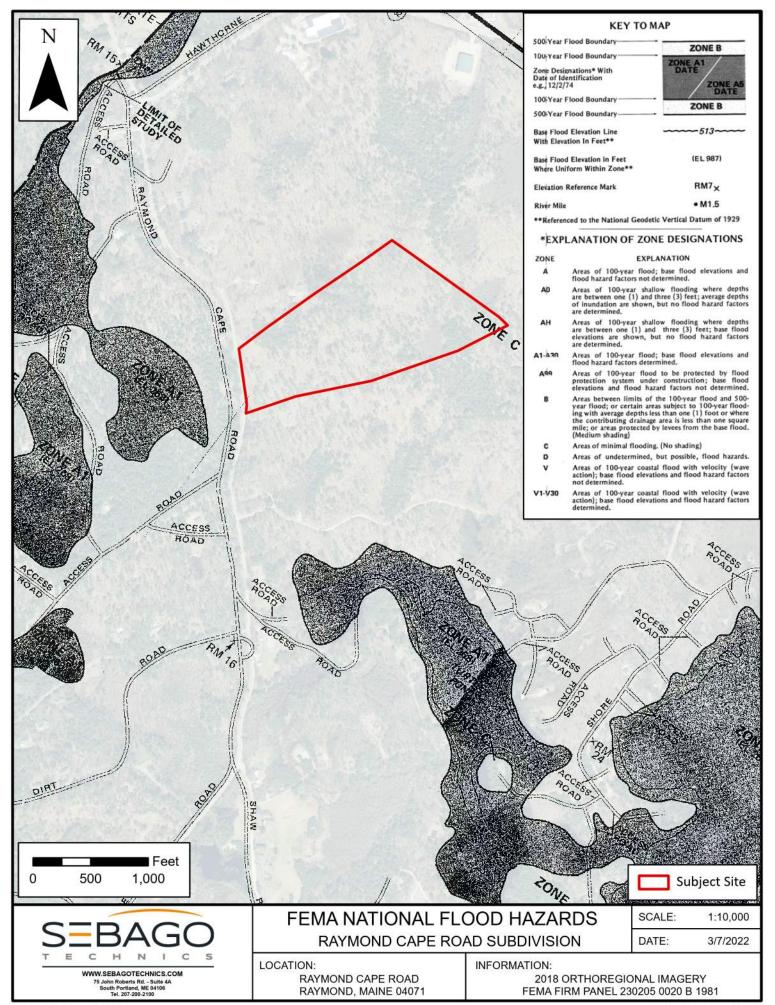
#### **Grass Underdrained Soil Filter**

	INSPECTION MAINTEN	ANCE AND HOUSEKEEPING FORM	
General Information			
Project Name:		Inspection Date:	
Project Location:		Current Weather:	
		Date / Amount Last Precip:	
BMP Owner:		Company conducting inspection:	
Owner Mailing Address:		Company Mailing Address	
Owner Phone #:		Company Phone #:	
Owner Email:		Inspector Name:	
		Inspector Email:	
Inspection Notes	·		
	Suggested Maintenance (recm'd		
BMP Element	frequency)	Observations	Inspection Notes/Recommended Action
Forebay/Pretreatment	Sediment/Debris Removal (Annually)		
	Inspect for bare areas or rill erosion (Annually)		
Outlet Control Structure	Sediment Depth (Annually)		
	Floatables/Debris (Annually)		
Discharge Pipe	Ground Stabilized (>1" rain, Annually)		
Emergency Spillway	Review for signs of erosion (Twice Annually)		
	Review for signs of discharge (>1" rain, twice annually)		
Embankments	Review for signs of erosion (Twice Annually)		
Filter Bed	Trim overgrown vegetation with string trimmer (annually)		
	Review basin for evidence of vehicular traffic or storage of snow within footprint (annually)		
	Confirm pond drains in 24-48 hours for water quality volume (annually)		
Inspector shall reference the and Engineers for a full list o		d Sediment Control Best Managem	ent Practices (BMPs) Manual for Designers
Additional Notes/Observation	-		

**Subsurface Investigations** 



**Flood Insurance Rate Map** 



### **Stormwater Management Plans**

SOIL	LEGEND				
SYMBOL	SOIL SERIES	PHASE	SLOPE	HSG	DRAINAGE CLASS
BeD	BECKET	SANDY LOAM	15-25%	С	WD (WELL DRAINED)
SeA	SEBAGO	MUCKY PEAT	0-3%	D	VPD (VERY POORLY DRAINED)
SkB	SKERRY	FINE SANDY LOAM	3-8%	с	MWD (MODERATELY WELL DRAINED)
SkC	SKERRY	FINE SANDY LOAM	8-15%	С	MWD (MODERATELY WELL DRAINED)
TuC	TUNBRIDGE	FINE SANDY LOAM	8-15%	С	WD (WELL DRAINED)
TuD	TUNBRIDGE	FINE SANDY LOAM	15-25%	С	WD (WELL DRAINED)
WeB	WESTBURY	SANDY LOAM	3-8%	D	SPD (SOMEWHAT POORLY DRAINED)

POA-2

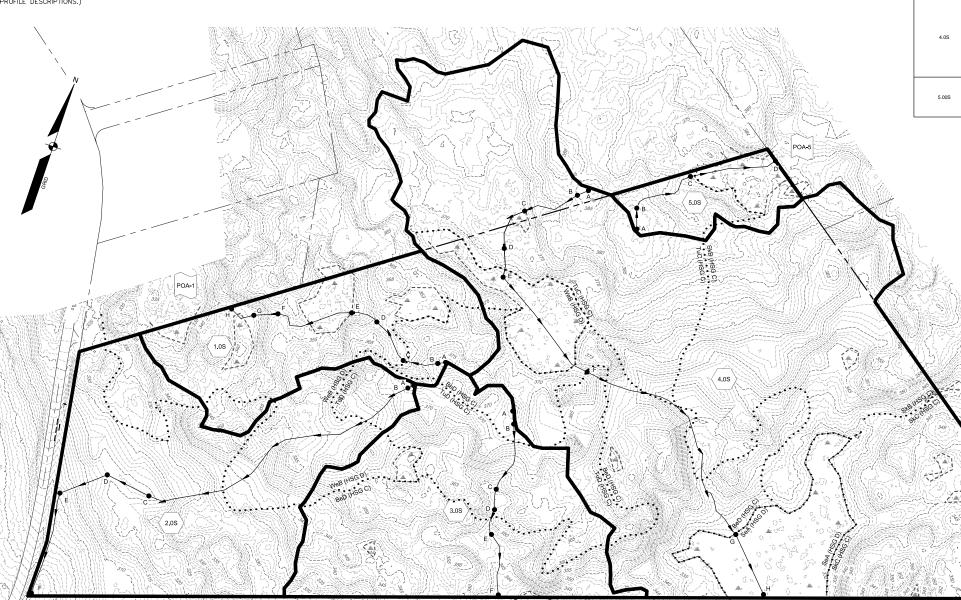
NOTE THIS CLASS 'C' MEDIUM-HIGH INTENSITY SOIL MAP CONFORMS TO THE GUIDELINES FOR MAINE CERTIFIED SOIL SCIENTISTS FOR SOIL IDENTIFICATION AND MAPPING, DATED MARCH 2009 FOR CLASS 'C' MEDIUM-HIGH INTENSITY SOIL SURVEYS. THE SOIL MAP UNITS AS DEPICTED WERE IN PART INFLUENCED BY THE INTENDED USE FOR A PROPOSED RESIDENTIAL SUBDIVISION AND THE SOILS WHICH WERE NON-LIMITING FOR ONE USE MAY BE CONSIDERED LIMITING FOR ANOTHER USE. THEREFORE, THIS CLASS 'C' MEDIUM-HIGH INTENSITY SOILS MAP MAY NOT BE ADEQUATE FOR ANOTHER USE. (REFER TO SOIL NARRATIVE REPORT DATED MARCH 11, 2022 AND SOIL PROFILE DESCRIPTIONS.)

STORMWATER PEAK DISCHARGE SUMMARY TABLE						
POINT OF	2-YEAF	RSTORM	10-YEA	R STORM	25-YEAR STORM	
ANALYSIS	PRE (CFS)	POST (CFS)	PRE (CFS)	PRE (CFS) POST (CFS)		POST (CFS)
POA-1	3.4	3.4	7.5	7.3	11.0	10.6
POA-2	4.8	4.7	11.3	11.3	17.2	17.2
POA-3	4.0	3.8	10.0	8.9	15.5	13.5
POA-4	10.1	9.3	24.3	24.3	37.3	37.3
POA-5	0.6	0.6	1.5	1.5	2.3	2.3

Q

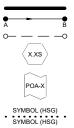
POA-4

	TIME	OF CONCE	NTRATION F	PATH TABLE	
SUBCATCHMENT	PATH	FLOW TYPE	LENGTH	SLOPE	TIME OF CONCENTRATION (MINUTES)
	A TO B	SHEET	20	15.00%	2.7
	B TO C	SHALLOW	80	12.11%	0.8
	C TO D	SHALLOW	110	1.80%	2.7
4.00	D TO E	SHALLOW	65	10.00%	0.7
1.0S	E TO F	SHALLOW	190	1.05%	6.2
	F TO G	SHALLOW	55	16.40%	0.5
	G TO H	SHALLOW	60	2.10%	1.4
	TOTAL	-	-	-	15.0
	A TO B	SHEET	15	12.00%	2.3
	B TO C	SHALLOW	675	7.41%	8.3
2.05	C TO D	SHALLOW	105	10.00%	3.5
2.05	D TO E	SHALLOW	115	12.20%	1.1
	E TO F	SHALLOW	235	6.40%	2.2
	TOTAL	-	-	-	17.4
	A TO B	SHEET	30	7.50%	4.9
	B TO C	SHALLOW	160	11.25%	1.6
3.05	C TO D	SHALLOW	45	1.00%	1.5
3.08	D TO E	SHALLOW	60	11.67%	0.6
	E TO F	SHALLOW	145	3.57%	2.6
	TOTAL	-	-	-	11.2
	A TO B	SHEET	25	5.00%	5.0
Γ	B TO C	SHALLOW	135	10.38%	1.4
	C TO D	SHALLOW	110	2.73%	2.2
4.0S	D TO E	SHALLOW	65	7.69%	0.8
4.00	E TO F	SHALLOW	290	0.50%	13.7
	F TO G	SHALLOW	560	6.25%	7.5
	G TO H	SHALLOW	150	0.50%	7.1
	TOTAL	-	-	-	37.7
	A TO B	SHEET	50	2.00%	12.5
5.005	B TO C	SHALLOW	155	8.40%	1.8
5.005	C TO D	SHALLOW	200	0.50%	9.4
T T	TOTAL	-	-	-	23.7



POA-3

#### EXISTING CONDITIONS LEGEND

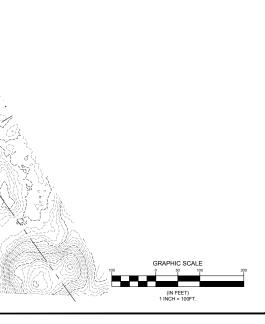


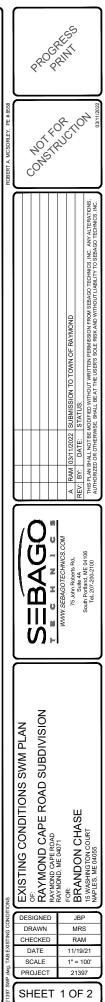
SUBCATCHMENT BOUNDARY TIME OF CONCENTRATION REACH

SUBCATCHMENT LABEL

POINT OF ANALYSIS

SOILS BOUNDARY





#### SOIL LEGEND

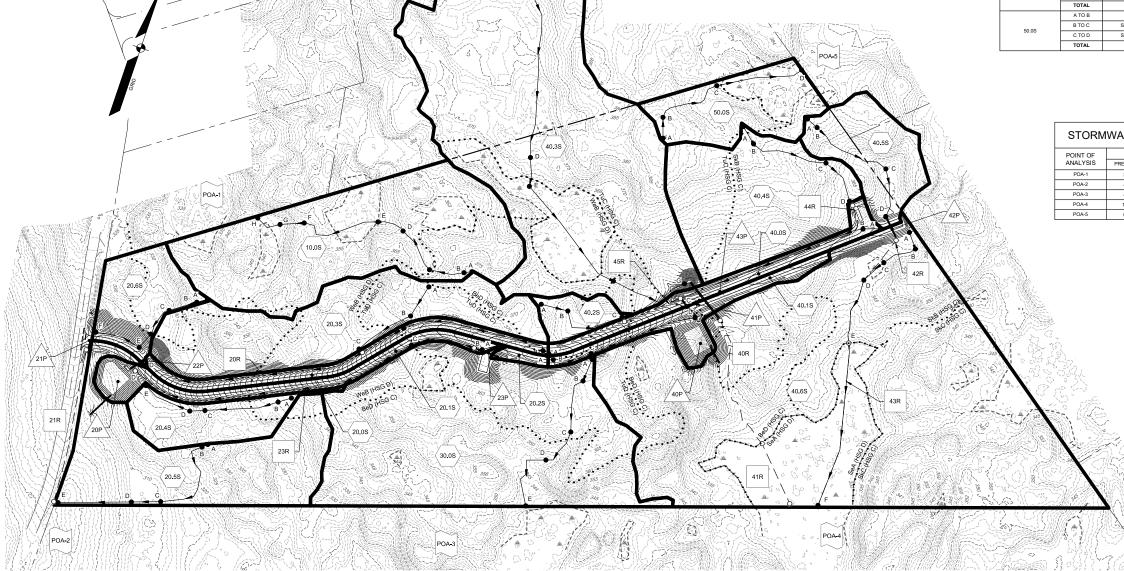
SYMBOL	SOIL SERIES	PHASE	SLOPE	HSG	DRAINAGE CLASS
BeD	BECKET	SANDY LOAM	15-25%	С	WD (WELL DRAINED)
SeA	SEBAGO	MUCKY PEAT	0-3%	D	VPD (VERY POORLY DRAINED)
SkB	SKERRY	FINE SANDY LOAM	3-8%	С	MWD (MODERATELY WELL DRAINED)
SkC	SKERRY	FINE SANDY LOAM	8-15%	С	MWD (MODERATELY WELL DRAINED)
TuC	TUNBRIDGE	FINE SANDY LOAM	8-15%	С	WD (WELL DRAINED)
TuD	TUNBRIDGE	FINE SANDY LOAM	15-25%	С	WD (WELL DRAINED)
WeB	WESTBURY	SANDY LOAM	3-8%	D	SPD (SOMEWHAT POORLY DRAINED)

NOTE THIS CLASS 'C' MEDIUM-HIGH INTENSITY SOIL MAP CONFORMS TO THE GUIDELINES FOR MAINE CERTIFIED SOIL SCIENTISTS FOR SOIL IDENTIFICATION AND MAPPING, DATED MARCH 2009 FOR CLASS 'C' MEDIUM-HIGH INTENSITY SOIL SURVEYS. THE SOIL MAP UNITS AS DEPICTED WERE IN PART INFLUENCED BY THE INTENDED USE FOR A PROPOSED RESIDENTIAL SUBDIVISION AND THE SOILS WHICH WERE NON-LIMITING FOR ONE USE MAY BE CONSIDERED LIMITING FOR ANOTHER USE. THEREFORE, THIS CLASS 'C' MEDIUM-HIGH INTENSITY SOILS MAP MAY NOT BE ADEQUATE FOR ANOTHER USE. (REFER TO SOIL NARRATIVE REPORT DATED MARCH 11, 2022 AND SOIL PROFILE DESCRIPTIONS.)

TIME OF CONCENTRATION PATH TABLE					
SUBCATCHMENT	PATH	FLOW TYPE	LENGTH	SLOPE	TIME OF CONCENTRATION (MINUTES)
	A TO B	SHEET	20	15.00%	2.7
	B TO C	SHALLOW	80	12.11%	0.8
	C TO D	SHALLOW	110	1.80%	2.7
	D TO E	SHALLOW	65	10.00%	0.7
10.0S	E TO F	SHALLOW	190	1.05%	6.2
	F TO G	SHALLOW	55	16.40%	0.5
	G TO H	SHALLOW	60	2.10%	1.4
	TOTAL	-	-	-	15.0
	A TO B	SHEET	15	2.00%	0.3
	B TO C	SHALLOW	335	2.50%	5.0
20.0S	C TO D	SHALLOW	625	8.00%	5.3
	TOTAL		-	-	10.6
	A TO B	SHEET	40	3.00%	0.5
	B TO C	SHALLOW	165	2.50%	2.5
20.1S	C TO D	SHALLOW	670	8.00%	5.6
	TOTAL	-	-	-	8.6
	DIRECT	DIRECT	-	-	6.0
20.2S	TOTAL		-	-	6.0
	A TO B	SHEET	80	5.00%	8.4
20.35	B TO C	SHALLOW	145	4.30%	2.3
	TOTAL		-	-	10.7
	A TO B	SHEET	30	6.67%	5.1
	B TO C	SHALLOW	170	5.00%	1.8
20.4S	C TO D	SHALLOW	35	28.00%	0.2
	D TO E	SHALLOW	115	2.00%	1.9
	TOTAL	-	-	-	9.0
20.58	A TO B	SHEET	15	6.67%	3.0
	B TO C	SHALLOW	215	14.40%	1.9
	C TO D	SHALLOW	65	1.50%	1.8
	D TO E	SHALLOW	165	10.91%	1.7
	TOTAL		-		8.4

20.6S	A TO B	SHEET	25	4.00%	5.5
	B TO C	SHALLOW	60	23.33%	0.4
	C TO D	SHALLOW	70	1.43%	2.0
	D TO E	SHALLOW	40	33.33%	0.2
	E TO F	SHALLOW	105	2.38%	1.6
	TOTAL	-	-	-	9.7
	A TO B	SHEET	55	10.91%	6.9
30.0S	B TO C	SHALLOW	130	3.08%	2.5
	C TO D	SHALLOW	95	12.63%	0.9
	D TO E	SHALLOW	155	3.23%	2.9
	TOTAL	-	-	-	13.2
	A TO B	SHEET	40	1.00%	0.8
40.0S	B TO C	SHALLOW	350	1.00%	8.3
	TOTAL	-	-	-	9.1
	A TO B	SHEET	15	2.00%	0.3
	B TO C	SHALLOW	100	4.00%	1.2
40.1S	C TO D	SHALLOW	250	7.00%	2.2
	DIRECT	DIRECT	-	-	2.3
	TOTAL	-	-	-	6.0
	A TO B	SHEET	60	10.00%	7.6
40.2S	B TO C	SHALLOW	160	2.50%	3.4
	TOTAL	-	-	-	11.0
	A TO B	SHEET	50	3.00%	10.7
	B TO C	SHALLOW	55	10.00%	0.6
	C TO D	SHALLOW	400	3.50%	7.1
40.3S	D TO E	SHALLOW	65	10.00%	0.7
	E TO F	SHALLOW	290	0.50%	13.7
	F TO G	SHALLOW	165	10.00%	1.7
	TOTAL	-	-	-	34.5
	A TO B	SHEET	45	3.00%	9.8
	B TO C	SHALLOW	175	7.14%	2.2
40.4S	C TO D	SHALLOW	110	5.00%	1.6
	TOTAL	-	-	-	13.6
	A TO B	SHEET	50	4.00%	9.5
40.5S	B TO C	SHALLOW	350	7.71%	4.2
	TOTAL	-	-	-	13.7
	A TO B	SHEET	40	2.50%	9.6
	B TO C	SHALLOW	80	6.90%	1.0
	C TO D	SHALLOW	60	1.67%	1.5
40.6S	D TO E	SHALLOW	150	7.33%	1.8
	E TO F	SHALLOW	380	0.50%	17.9
	TOTAL	-	-	-	31.8
	A TO B	SHEET	50	2.00%	12.5
	B TO C	SHALLOW	155	8.40%	1.8
50.0S	C TO D	SHALLOW	200	0.50%	9.4
	TOTAL	-			23.7





TER PEAK DISCHARGE SUMMARY TABLE								
2-YEAR STORM		10-YEAR STORM		25-YEAR STORM				
(CFS)	POST (CFS)	PRE (CFS)	POST (CFS)	PRE (CFS)	POST (CFS)			
.4	3.4	7.5	7.3	11.0	10.6			
.8	4.7	11.3	11.3	17.2	17.2			
.0	3.8	10.0	8.9	15.5	13.5			

24.3

1.5

37.3

2.3

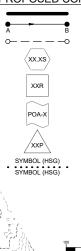
37.3

2.3

24.3

1.5

#### PROPOSED CONDITIONS LEGEND



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9.3

0.6

SUBCATCHMENT BOUNDARY TIME OF CONCENTRATION REACH

SUBCATCHMENT LABEL

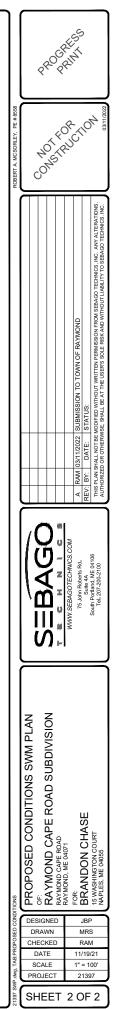
REACH

POINT OF ANALYSIS

STORMWATER TREATMENT/DETENTION POND

SOILS BOUNDARY





### <u>Exhibit 6</u>

### Hydrogeologic Assessment

#### EXHIBIT 6: HYDROGEOLIC ASSESSMENT

Based upon the size of the proposed lots, locations for proposed systems the fact that the SSWDS will be individual systems and not a community disposal, the resulting nitrate plumes from the SSWDS are not expected to extend beyond the boundary of the project. A hydrogeolic assessment will be provided to the Town as part of the Final Subdivision review documentation.

### Exhibit 7

Traffic Memorandum

#### EXHIBIT 7: TRAFFIC MEMORANDUM

Please the attached Traffic Memorandum dated March 10, 2022 prepared by Sebago Technics, the project will not create trip ends that require a MDOT Traffic Movement Permit and the proposed road has the required sight distances required by the assigned speed limits.



CIVIL ENGINEERING • SURVEYING • LANDSCAPE ARCHITECTURE

### Memorandum

21397

To: Robert A. McSorley, P.E., Sebago Technics

From: Nikki Conant, P.E., Sebago Technics

Date: March 10, 2022



Subject: Trip Generation Assessment, Raymond Cape Road Residential Subdivision, Raymond

#### Introduction

The purpose of this memorandum is to provide a trip generation assessment for a proposed residential development in Raymond, Maine. The development is proposed to be made up of 12 single-family lots. Access to the subdivision is proposed via a full movement access to Raymond Cape Road. As such, this assessment details estimated trip generation, provides a crash data review, and evaluates sight distance for the proposed driveway.

### **Trip Generation**

The 11<sup>th</sup> Edition of the Institute of Transportation Engineer's (ITE) *Trip Generation Manual* was utilized to estimate the trip generation for the single-family homes. Land use code (LUC) 210 – Single-Family Detached Housing was utilized on the basis of 12 dwelling units. The trip generation results are summarized in Table 1:

Table 1 – ITE Trip Generation
Land Use Code 210 – Single-Family Detached Housing
12 Dwelling Units

Time Period	Fitted Curve Equation	Trips	Entering	Exiting
Weekday	Ln(T) = 0.92Ln(X) + 2.68	143	71 (50%)	72 (50%)
AM Peak Hour – Adjacent Street (7 – 9 AM)	Ln(T) = 0.91Ln(X) + 0.12	11	3 (26%)	8 (74%)
AM Peak Hour – Generator	T = 0.71(X) + 7.23	16	4 (26%)	12 (74%)
PM Peak Hour – Adjacent Street (4 – 6 PM)	Ln(T) = 0.94Ln(X) + 0.27	14	9 (63%)	5 (37%)
PM Peak Hour – Generator	Ln(T) = 0.93Ln(X) + 0.36	14	9 (64%)	5 (36%)

As shown in Table 1, the single-family detached housing is estimated to generate 16 trips and 14 trips during the AM and PM peak hour periods of the generator, respectively. Given this level of trip generation, a Traffic Movement Permit (TMP) will not be required from the Maine Department of Transportation (MaineDOT) as project trip generation does not exceed the 100-trip threshold to require a permit. Additionally, this level of trip generation would not be expected to have impacts off-site on the adjacent roadway system as the project is estimated to generate a maximum of 12 new trips in a lane in an hour. As such, no additional analysis is recommended.

#### **Crash Data**

The MaineDOT Public Crash Query was utilized to determine if there are any high crash locations within the immediate vicinity of the site. An intersection or section of roadway is deemed an HCL if two criteria are met: a Critical Rate Factor (CRF) greater than 1.0 and a minimum of eight (8) crashes in a three-year period. Crash data for Raymond Cape Road was reviewed from Hawthorne Road south to Shaw Road for the most recent three-year study period from 2018 – 2020. Based on the crash information, Raymond Cape Road in the immediate vicinity of the site, is not designated as a high crash location. As such, there are no recommendations for improvements in conjunction with this project.

#### **Sight Distance Analysis**

Sight distance at the proposed site driveway location on Raymond Cape Road was measured in the field on March 8, 2022. Measurements were conducted from a point 12 feet behind the curb line or edge of the travelway, considering a height of eye of 3.5 feet and a height of object of 4.25 feet, as outlined in the Town of Raymond Subdivision Ordinance. The Ordinance requires a minimum sight distance in each direction of 10 feet per each mile per hour of posted speed limit.

As noted during the field visit, it appears the posted speed limit zones on Raymond Cape Road change in the imemdiate vicinity of the proposed site driveway. This results in a speed limit of 40 MPH south of the site and 25 MPH north of the site, thus requiring 400 feet of sight distance to the left (south) and 250 feet of sight distance to the right (north).

Sight distance to the left, as shown in Figure 1 was measured to be in excess of 600 feet. Sight distance to the right, as shown in Figure 2, was measured to be 350 feet. As such, sight distance from the driveway access location is adequate for the posted speed limit. It is important to note that no landscaping, signage, or other features shall be located within the sight triangle of the proposed driveway.



Figure 1: Sight Distance Looking Left



Figure 2: Sight Distance Looking Right

#### Conclusion

- The residential development on Raymond Cape Road is estimated to generate 16 trips and 14 trips during the AM and PM peak hour periods of the generator, respectively. As such, a TMP would not be required by the MaineDOT, as estimated trip generation for the development does not exceed the 100-trip threshold.
- There were no high crash locations along Raymond Cape Road within the immediate vicinity of the site. As such, there are no recommendations for improvements.
- Sight distance from the proposed driveway location on Raymond Cape Road meets required sight distance, per the Town of Raymond Subdivision Ordinance.

# <u>Exhibit 8</u>

## Natural Resources-Reports, Maps, Inquiries

- Wetland Memorandum a.
- Maine Department of Inland Fisheries & Wildlife b.
  - Maine Natural Areas Program c.
    - Maine Historic Preservation d.
      - NRCS Soils Map e.
      - FEMA Flood Map f.

#### EXHIBIT 8: NATURAL RESOURCES

Per Town requirements, the Applicant solicited input from regulatory agencies, provided wetland and protected natural resource information and maps regarding regulated site conditions as follows:

a. Wetlands

Sebago Technics environmental staff identified natural resources, including freshwater wetlands, and performed soils test pits necessary for septic designs. A copy of the memo is included in this section

b. On behalf of the Applicant, Sebago Technics requested a formal site review by the Maine Department of Inland Fisheries & Wildlife. The enclosed response letter dated February 24, 2022, indicates the presence of a deer wintering area (DWA) and requests that the Applicant avoid impact to the coniferous winter shelter area. No development or other site improvements are located within the mapped wintering area as shown on the appended site plans.

c. The formal response from the Maine Natural Areas Program dated February 22, 2022, included in this section indicates that there are no rare botanical features documented specifically within the project area.

d. To date, a response from the Maine Historic Preservation Commission regarding potential impact to areas or structures of historical value has not been received. A copy of the inquiry letter dated February 21, 2022, is enclosed in this section, and the response will be copied to the Town when available. While there is one historic structure (Nathaniel Hawthorne's childhood home) nearby, we note that there are no views to or from the homestead to proposed subdivision.

e. A copy of the Class 'C' Medium High Intensity Soil Survey Report is included in this section. Suitable test pits were located on each proposed lot in support of subsurface wastewater disposal (septic), and the soils are generally categorized as suitable for the proposed street and residential development.

f. A FEMA Flood Map exhibit indicates that the proposed development site is located in a "C Zone" identified as an area of minimal flooding. The proposed improvements, as proposed, will not cause an increase in flooding or other changes to flood-related conditions.



# Wetland Memo

To: Dan Danvers, RLA ASLA

From: Gary Fullerton, Director, Natural Resources

Date: 12/6/2021

Project: #21397 – Raymond Cape Subdivision, Raymond

#### Methods of Investigation:

The wetlands on the site were delineated by Gary Fullerton and Anna Biddle of Sebago Technics, Inc. on 6/16/2021 and 6/21/2021. This delineation conforms to the standards and methods outlined in the 1987 Wetlands Delineation Manual and 2012 Northeast Regional Supplement authored and published by the U.S. Army Corps of Engineers. The wetlands were marked in the field with alpha numeric pink "wetland delineation" flagging. The flags were then located using a Trimble GPS backpack unit capable of submeter accuracy.

#### Location and Description:

The entire parcel in Raymond, east of the Raymond Cape Road, was surveyed for wetlands. The total site was approximately 40 acres.

#### **Results of Wetland Survey:**

Several wetlands were found on site, mostly located in the eastern portion of the parcel. The most common wetland type found was Palustrine, forested, deciduous as defined by the Classification of Wetlands and Deepwater Habitats (Cowardin, et al., 1979). The dominant vegetation in the wetlands was red maple, cinnamon fern, and sphagnum moss.

None of the wetlands delineated on site appear to be a Wetland of Special Significance (WOSS) per the Maine Department of Environmental Protection. WOSS is defined in the Natural Resources Protection Act, Chapter 310 – Wetlands and Waterbodies Protection, Section 4.

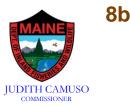
No streams were found on the site. No vernal pool survey has been completed by Sebago Technics, Inc.

Please contact me if you have any questions or need additional information.

Dy Kat



STATE OF MAINE DEPARTMENT OF INLAND FISHERIES & WILDLIFE 353 WATER STREET 41 STATE HOUSE STATION AUGUSTA ME 04333-0041



February 24, 2022

Stefanie Nichols Sebago Technics 75 John Roberts Road, Suite 1A Portland, ME 04101

#### **RE:** Information Request – Raymond Cape Road Subdivision Project, Raymond

Dear Stefanie:

Per your request received on February 22, 2022, we have reviewed current Maine Department of Inland Fisheries and Wildlife (MDIFW) information for known locations of Endangered, Threatened, and Special Concern species; designated Essential and Significant Wildlife Habitats; and inland fisheries habitat concerns within the vicinity of the *Raymond Cape Road Subdivision* project in Raymond.

Our Department has not mapped any Essential Habitats that would be directly affected by your project.

#### Endangered, Threatened, and Special Concern Species

<u>Bat Species</u> – Of the eight species of bats that occur in Maine, the three *Myotis* species are protected under Maine's Endangered Species Act (MESA) and are afforded special protection under 12 M.R.S §12801 - §12810. The three *Myotis* species include little brown bat (State Endangered), northern longeared bat (State Endangered), and eastern small-footed bat (State Threatened). The five remaining bat species are listed as Special Concern: big brown bat, red bat, hoary bat, silver-haired bat, and tri-colored bat. While a comprehensive statewide inventory for bats has not been completed, based on historical evidence it is likely that several of these species occur within the project area during migration and/or the breeding season. However, our Agency does not anticipate significant impacts to any of the bat species as a result of this project.

#### Significant Wildlife Habitat

<u>Deer Wintering Areas (DWAs)</u> – The project search area intersects with a DWA. DWAs contain habitat cover components that provide conditions where deer find protection from deep snow and cold wind, which is important for overwinter survival. MDIFW recommends that development projects be designed to avoid losses or impacts to the continued availability of coniferous winter shelter. Any removal of vegetation should be conducted in such a way that improves the quality and vigor of the coniferous species providing this winter shelter.

<u>Significant Vernal Pools</u> - At this time, MDIFW Significant Wildlife Habitat maps indicate no known presence of Significant Vernal Pools in the project search area; however, a comprehensive statewide inventory for Significant Vernal Pools has not been completed. Therefore, we recommend that surveys for vernal pools be conducted within the project boundary by qualified wetland scientists prior to final project design to determine whether there are Significant Vernal Pools present in the area. These surveys should extend up to 250 feet beyond the anticipated project footprint because of potential performance

#### Letter to Stefanie Nichols, Sebago Technics Comments RE: Raymond Cape Road Subdivision, Raymond February 24, 2022

standard requirements for off-site Significant Vernal Pools, assuming such pools are located on land owned or controlled by the applicant. Once surveys are completed, survey forms should be submitted to our Agency for review <u>well before</u> to the submission of any necessary permits. Our Department will need to review and verify any vernal pool data prior to final determination of significance.

#### Fisheries Habitat

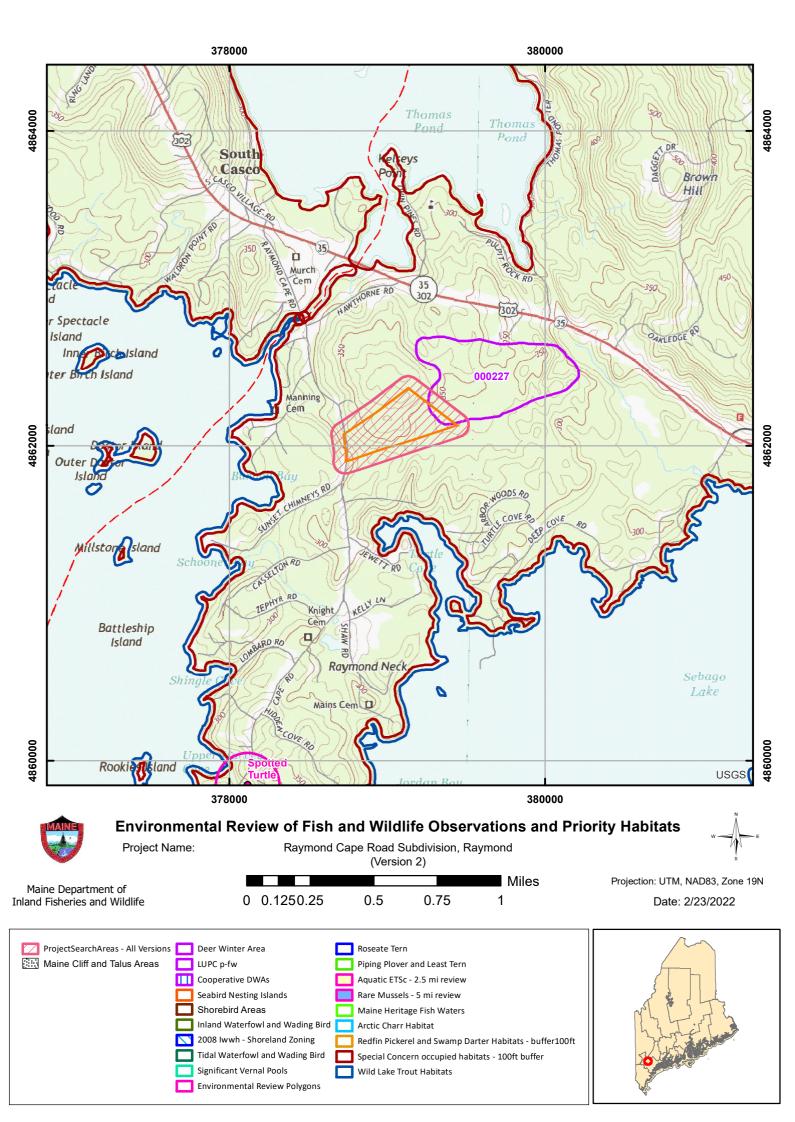
We recommend that 100-foot undisturbed vegetated buffers be maintained along streams. Buffers should be measured from the edge of stream or associated fringe and floodplain wetlands. Maintaining and enhancing buffers along streams that support coldwater fisheries is critical to the protection of water temperatures, water quality, natural inputs of coarse woody debris, and various forms of aquatic life necessary to support conditions required by many fish species. Stream crossings should be avoided, but if a stream crossing is necessary, or an existing crossing needs to be modified, it should be designed to provide full fish passage. Small streams, including intermittent streams, can provide crucial rearing habitat, cold water for thermal refugia, and abundant food for juvenile salmonids on a seasonal basis and undersized crossings may inhibit these functions. Generally, MDIFW recommends that all new, modified, and replacement stream crossings be sized to span at least 1.2 times the bankfull width of the stream. In addition, we generally recommend that stream crossings be open bottomed (i.e. natural bottom), although embedded structures which are backfilled with representative streambed material have been shown to be effective in not only providing habitat connectivity for fish but also for other aquatic organisms. Construction Best Management Practices should be closely followed to avoid erosion, sedimentation, alteration of stream flow, and other impacts as eroding soils from construction activities can travel significant distances as well as transport other pollutants resulting in direct impacts to fish and fisheries habitat. In addition, we recommend that any necessary instream work occur between July 15 and October 1.

This consultation review has been conducted specifically for known MDIFW jurisdictional features and should not be interpreted as a comprehensive review for the presence of other regulated features that may occur in this area. Prior to the start of any future site disturbance we recommend additional consultation with the municipality, and other state resource agencies including the Maine Natural Areas Program, Maine Department of Marine Resources, and Maine Department of Environmental Protection in order to avoid unintended protected resource disturbance.

Please feel free to contact my office if you have any questions regarding this information, or if I can be of any further assistance.

Best regards,

Becca Settele Wildlife Biologist





## STATE OF MAINE DEPARTMENT OF AGRICULTURE, CONSERVATION & FORESTRY

177 STATE HOUSE STATION AUGUSTA, MAINE 04333

Amanda E. Beal Commissioner

**8c** 

JANET T. MILLS GOVERNOR

February 22, 2022

Stefanie Nichols Sebago Technics 75 John Roberts Road, Suite 4A South Portland, ME 04106

Via email: rgabryszewski@sebagotechnics.com

Re: Rare and exemplary botanical features in proximity to: #21397, 13-Lot Residential Subdivision, Cape Road, Raymond, Maine

Dear Ms. Nichols:

I have searched the Maine Natural Areas Program's Biological and Conservation Data System files in response to your request received February 21, 2022 for information on the presence of rare or unique botanical features documented from the vicinity of the project in Raymond, Maine. Rare and unique botanical features include the habitat of rare, threatened, or endangered plant species and unique or exemplary natural communities. Our review involves examining maps, manual and computerized records, other sources of information such as scientific articles or published references, and the personal knowledge of staff or cooperating experts.

Our official response covers only botanical features. For authoritative information and official response for zoological features you must make a similar request to the Maine Department of Inland Fisheries and Wildlife, 284 State Street, Augusta, Maine 04333.

According to the information currently in our Biological and Conservation Data System files, there are no rare botanical features documented specifically within the project area. This lack of data may indicate minimal survey efforts rather than confirm the absence of rare botanical features. You may want to have the site inventoried by a qualified field biologist to ensure that no undocumented rare features are inadvertently harmed.

If a field survey of the project area is conducted, please refer to the enclosed supplemental information regarding rare and exemplary botanical features documented to occur in the vicinity of the project site. The list may include information on features that have been known to occur historically in the area as well as recently field-verified information. While historic records have not been documented in several years, they may persist in the area if suitable habitat exists. The enclosed list identifies features with potential to occur in the area, and it should be considered if you choose to conduct field surveys.

This finding is available and appropriate for preparation and review of environmental assessments, but it is not a substitute for on-site surveys. Comprehensive field surveys do not exist for all natural areas in Maine, and in the absence of a specific field investigation, the Maine Natural Areas Program cannot provide a definitive statement on the presence or absence of unusual natural features at this site.

MOLLY DOCHERTY, DIRECTOR MAINE NATURAL AREAS PROGRAM BLOSSOM LANE, DEERING BUILDING



PHONE: (207) 287-804490 WWW.MAINE.GOV/DACF/MNAP Letter to Sebago Technics Comments RE: Cape Road, Raymond February 22, 2022 Page 2 of 2

The Maine Natural Areas Program (MNAP) is continuously working to achieve a more comprehensive database of exemplary natural features in Maine. We would appreciate the contribution of any information obtained should you decide to do field work. MNAP welcomes coordination with individuals or organizations proposing environmental alteration or conducting environmental assessments. If, however, data provided by MNAP are to be published in any form, the Program should be informed at the outset and credited as the source.

The Maine Natural Areas Program has instituted a fee structure of \$75.00 an hour to recover the actual cost of processing your request for information. You will receive an invoice for \$150.00 for two hours of our services.

Thank you for using MNAP in the environmental review process. Please do not hesitate to contact me if you have further questions about the Natural Areas Program or about rare or unique botanical features on this site.

Sincerely,

Lisa St. Hilaire

Lisa St. Hilaire | Information Manager | Maine Natural Areas Program 207-287-8044 | <u>lisa.st.hilaire@maine.gov</u>

Habitat		Hardwood to mixed forest (forest, upland)	Hardwood to mixed forest (forest, upland)		Hardwood to mixed forest (forest, upland)		Non-tidal rivershore (non-forested, seasonally
Occurrence Number		ъ	11		2		4
Date Last Observed		2010-08-18	2010-08-18		1916-08		1933-08-17
Global Rank		G4?	G4?		G5		G5
State Rank		S2	S2		S1		S1
State Status		⊢	Τ		ш		ш
Common Name	Nodding Pogonia			Scarlet Oak		Wild Coffee	

Rare and Exemplary Botanical Features within 4 miles of Project: #21397, 13-Lot Residential Subdivision, Cape Road, Raymond, Maine

Date Exported: 2022-02-22 15:58

Maine Natural Areas Program

Page 1 of 1

#### **Conservation Status Ranks**

**State and Global Ranks**: This ranking system facilitates a quick assessment of a species' or habitat type's rarity and is the primary tool used to develop conservation, protection, and restoration priorities for individual species and natural habitat types. Each species or habitat is assigned both a state (S) and global (G) rank on a scale of critically imperiled (1) to secure (5). Factors such as range extent, the number of occurrences, intensity of threats, etc., contribute to the assignment of state and global ranks. The definitions for state and global ranks are comparable but applied at different geographic scales; something that is state imperiled may be globally secure.

Rank Definition **S1 Critically Imperiled** – At very high risk of extinction or elimination due to very restricted G1 range, very few populations or occurrences, very steep declines, very severe threats, or other factors. **S2** Imperiled – At high risk of extinction or elimination due to restricted range, few G2 populations or occurrences, steep declines, severe threats, or other factors. **S3 Vulnerable** – At moderate risk of extinction or elimination due to a fairly restricted range, G3 relatively few populations or occurrences, recent and widespread declines, threats, or other factors. **S4** Apparently Secure – At fairly low risk of extinction or elimination due to an extensive G4 range and/or many populations or occurrences, but with possible cause for some concern as a result of local recent declines, threats, or other factors. **S5 Secure** – At very low risk or extinction or elimination due to a very extensive range, G5 abundant populations or occurrences, and little to no concern from declines or threats. SX Presumed Extinct – Not located despite intensive searches and virtually no likelihood of GX rediscovery. SH Possibly Extinct - Known from only historical occurrences but still some hope of GH rediscovery. S#S# **Range Rank** – A numeric range rank (e.g., S2S3 or S1S3) is used to indicate any range of G#G# uncertainty about the status of the species or ecosystem. SU **Unrankable** – Currently unrankable due to lack of information or due to substantially GU conflicting information about status or trends. **GNR** Unranked - Global or subnational conservation status not yet assessed. SNR **SNA Not Applicable** – A conservation status rank is not applicable because the species or **GNA** ecosystem is not a suitable target for conservation activities (e.g., non-native species or ecosystems. Qualifier Definition S#? Inexact Numeric Rank – Denotes inexact numeric rank. G#? Q Questionable taxonomy that may reduce conservation priority – Distinctiveness of this entity as a taxon or ecosystem type at the current level is questionable. The "Q" modifier is only used at a global level. T# **Infraspecific Taxon (trinomial)** – The status of infraspecific taxa (subspecies or varieties) are indicated by a "T-rank" following the species' global rank.

The information supporting these ranks is developed and maintained by the Maine Natural Areas Program (state ranks) and NatureServe (global ranks).

**State Status**: Endangered and Threatened are legal status designations authorized by statute. Please refer to MRSA Title 12, §544 and §544-B.

Status	Definition
E	Endangered – Any native plant species in danger of extinction throughout all or a
	significant portion of its range within the State or Federally listed as Endangered.
Т	Threatened – Any native plant species likely to become endangered within the
	foreseeable future throughout all or a significant portion of its range in the State or
	Federally listed as Threatened.
SC	Special Concern – A native plant species that is rare in the State, but not rare enough to
	be considered Threatened or Endangered.
PE	Potentially Extirpated – A native plant species that has not been documented in the State
	in over 20 years, or loss of the last known occurrence.

**Element Occurrence (EO) Ranks**: Quality assessments that designate viability of a population or integrity of habitat. These ranks are based on size, condition, and landscape context. Range ranks (e.g., AB, BC) and uncertainty ranks (e.g., B?) are allowed. The Maine Natural Areas Program tracks all occurrences of rare plants and natural communities/ecosystems (S1-S3) as well as exemplary common natural community types (S4-S5 with EO ranks A/B).

Rank	Definition
Α	Excellent – Excellent estimated viability/ecological integrity.
В	Good – Good estimated viability/ecological integrity.
С	Fair – Fair estimated viability/ecological integrity.
D	Poor – Poor estimated viability/ecological integrity.
E	Extant – Verified extant, but viability/ecological integrity not assessed.
Н	Historical – Lack of field information within past 20 years verifying continued existence of
	the occurrence, but not enough to document extirpation.
Х	Extirpated – Documented loss of population/destruction of habitat.
U	Unrankable – Occurrence unable to be ranked due to lack of sufficient information (e.g.,
	possible mistaken identification).
NR	Not Ranked – An occurrence rank has not been assigned.

Visit the Maine Natural Areas Program website for more information <u>http://www.maine.gov/dacf/mnap</u>







February 21, 2022 21397

Mr. Kirk Mohney, Director and State Historic Preservation Officer
Maine Historic Preservation Commission
65 State House Station
Augusta, Maine 04333

Email submittal: claudette.coyne@maine.gov

Re: Proposed Residential Subdivision 78 Cape Road, Raymond Tax Map 4/Lot 29

Dear Mr. Mohney:

On behalf of our client, Brandon Chase, Sebago Technics respectfully requests a site review for a proposed 13-lot residential subdivision on a 37-acre parcel at 78 Raymond Cape Road, Raymond. The site improvements will consist of a private road, electrical/communications infrastructure, drainage, stormwater management features, and other associated site improvements. Development of the individual house lots is not part of this project phase. As part of the site permitting due diligence, we request a review by the Maine Historic Preservation Commission for any properties, structures, or other areas of historical significance in the vicinity of the proposed site.

The site is primarily wooded and located in a rural area. A review of the Town Comprehensive Plan (2004) and other historical resources identified a boyhood home of Nathaniel Hawthorne (NRHP 1969) located nearby at 40 Hawthorne Road, Raymond (Map 75/Lot 36). No views to the site improvements at 78 Cape Road from the Hawthorne House or other neighboring buildings are anticipated due to the wooded location.

Reference is made to the enclosed USGS Site Location Map, Town of Raymond Comprehensive Plan, *Historic, and Archaeological Resources Map,* and an annotated 11x17 Tax Map.

Please review the material and let me know your findings at your earliest convenience. If you have any questions or require additional information, please do not hesitate to contact me at (207) 200-2120 or directly at snichols@sebagotechnics.com. I look forward to hearing from you.

K. Mohney, MHPC

Sincerely, SEBAGO TECHNICS, INC.

Styanii Clichols

Stefanie Nichols Permitting Specialist/Project Coordinator

enc. USGS Site Location Map Town Historic and Archaeological Map Image Sheet 11x17 Tax Map 4



CIVIL ENGINEERING • SURVEYING • LANDSCAPE ARCHITECTURE

# CLASS 'C' MEDIUM HIGH INTENSITY SOIL SURVEY REPORT

Prepared for: Brandon Chase 15 Washington Court Naples, Maine 04055

Prepared by:

Sebago Technics, Inc. 75 John Roberts Road Suite 4A South Portland, Maine 04106

March 11, 2022

#### CLASS 'C' MEDIUM HIGH INTENSITY SOIL SURVEY

### **Residential Development**

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4.	Site Investigation	2
5.	Soil Characteristics	2
6.	Soil Map and Map Unit Descriptions	3
7.	Conclusions	3
8.	Limitations ERROR! BOOKMARK NOT	۲ DEFINED.

#### APPENDICES

APPENDIX A - Soil Narrative Report
APPENDIX B - Soil Legend/MDEP Form E
APPENDIX C - Soil Survey Interpretations
APPENDIX D - Soil Test Pits/MDEP Form F
APPENDIX E - Class 'C' Medium High Intensity Soil Map

## Section 1 Introduction

Sebago Technics has completed a Class 'C' Medium High Intensity Soil Survey for the proposed Residential Development, located adjacent to Raymond Cape Road in Raymond, Maine. The soils found on the above referenced site have been observed in the field using test pits dug by an excavator, and one boring with a hand auger (see Soil Map for Survey Limits in Appendix E). The test pits were located by Global Positioning Systems (GPS) technology and incorporated into the soil map. The soil map has been merged into the existing base plan prepared by Sebago Technics. Topography is based on 2-foot contour intervals prepared using Lidar DEM from Maine GIS.

The soil map units and soil boundaries have been drawn, reviewed, and forwarded to the Project Manager, Robert McSorley, PE, for consideration during engineering design and layout of the proposed Residential Development. Soils found at the site are described below and were examined and classified to identify potential soil limitations relating to the development of the property. This report has been prepared as part of the project requirements for the Town of Raymond, and may be used to support permitting procedures as required under the Site Location of Development Act, Natural Resources Protection Act (NRPA), Stormwater Management Law, or other pertinent regulation.

## Section 2

### **Purpose of Soil Survey**

The purpose of this Class 'C' Medium High Intensity Soil Survey was to investigate, identify, describe, and map the soils on the above referenced site for the proposed Residential Development. The accompanying soil survey map depicts the location and types of soil found on the project site. The soil information may be used to obtain hydrologic soil group ratings to assist in the calculations for stormwater runoff curve values required by the Maine Department of Environmental Protection (MDEP). This soil information may also be used to evaluate soil suitability relating to development for the proposed Residential site. A separate geotechnical report may be required to address engineering requirements for the construction of the site and structures.

#### Section 3

## Site Location and Description

The site is located adjacent to Raymond Cape Road in Raymond, Maine. The abutting properties are generally wooded and residential properties. The proposed development area includes approximately 40 acres of land. Wetlands were delineated during June 2021 by Sebago Technics, Inc. The entire site was a previously harvested woodlot.

## Section 4 Site Investigation

We collected site-specific soil information at various locations across the site on February 10, 2022. The areas examined were designated with letters from TP 1 to TP 20, and BOR 21. All test pits were dug by an excavator, and the boring was hand augured. Test pit locations were selected based on disturbance areas and topographic relief, which typically are indicative of soil type variations. Excavated test pits were examined for soil colors, rock content, texture, consistence, root depths, redoximorphic features, and depth to restrictive horizons. From this information, soil logs were completed and are included in Appendix E.

The test pits observed in the field were located by a GPS unit capable of submeter accuracy on the date that they were excavated. These points were then incorporated into the topographic survey to aid in the preparation of a soil map of the project area. The provided base map has a scale of 1 inch = 80 feet, with two-foot contour intervals on the site.

Drainage classifications of the soils on the site were determined by parameters found in the Guidelines for Maine Certified Soil Scientists for Soil Identification and Mapping, published by the Maine Association of Professional Soil Scientists in April 1989 and revised in March 2009.

#### Section 5 Soil Characteristics

The soils found on the site are developed from lodgment glacial till, ablation glacial till, and organic materials. The landforms typically associated with these soils are drumlins, uplands, hills, and swamps. They are generally made up of fine sandy loam or sandy loam, with gravel, stones, or boulders.

The lodgment till soils include the well drained Becket, the moderately well drained Skerry, and the somewhat poorly drained Westbury. These soils are all very deep to bedrock. These soils were found on land with slopes of 3 to 25 percent.

The ablation till soils include the well drained and moderately deep Tunbridge. These soils were found on land with slopes of mostly 15 to 25%

The organic soils include the very poorly drained Sebago mucky peat. These soils were found on level land with slopes of 0 to 3 percent.

These soils should respond to use and management as determined and described in the Soil Series of Maine Soil Interpretations published by the Maine Association of Professional Soil Scientists in cooperation with the USDA Natural Resources Conservation Service, dated January 1987 and revised January 1988 and 1989. Soil survey interpretations are enclosed in Appendix C of this report.

This site may contain inclusions of soil types that differ from the soil map units. The areas where these soils were found are too small to be mapped and, for the purpose of this soil survey, there appears to be less than 5 contiguous acres of this soil in any part of the site. It also appears that the total area of this soil type in any given map unit is less than 25 percent, therefore classifying these soil types as inclusions.

One known inclusion is the small wetlands mapped within the upland map units. The soils in these wetlands may be Naumburg variant, Sebago mucky peat, or a poorly or very poorly drained till soil. The areas of wetland soils are very dissimilar to the upland map units, due to lower runoff and greater infiltration, among other characteristics.

# Section 6 Soil Map and Map Unit Descriptions

The attached soil survey map depicts the size and location of the soil map units relative to each other and existing site features. Each soil map unit typically consists of three letters (e.g., AdB), with the first two letters representing a phase of the established soil series found within soil map unit areas as shown on the soil map. This soil map unit phase name is a representation of the soil characteristics, such as texture, stoniness, drainage, and depth to bedrock, all of which may affect the use and management of the soil. The third capitalized letter represents the surface slope gradient of the area within the soil map unit (e.g., B represents 3 to 8 percent slopes). Therefore, in this example "AdB" is interpreted as Adams loamy fine sand on a 3 to 8 percent slope. There may be small areas of different soils within a soil map unit, known as inclusions. Inclusions may exist within a delineated soil map unit, although the size of the inclusion may be too small to stand as a soil map unit alone (<5 acres). The soil map units found at the site are listed with soil potential rating classes in Appendix C of this report.

#### Section 7 Conclusions

The soils found on site consist of lodgment glacial till, ablation till, and organic materials. The landforms typically associated with the lodgment till are drumlins, hills, and uplands. They are generally made up of fine sandy loam and sandy loam, and contain rock fragments ranging in size from gravel to boulders. The landforms associated with the ablation till are uplands and ridges. They are made up of fine sandy loam and sandy loam, and contain gravel, cobbles, and stones. The landforms associated with the organic soils are swamps. They are made up of low-pH, moderately decomposed organic materials with no mineral soil nor rock fragments.

All of these soils are generally suitable for the proposed development. The exception to this is the Sebago mucky peat map unit, which is located within the Open Space 2 parcel of the subdivision, with no disturbance planned. Given the size of the soil survey and extent of the development, soil and topographical conditions may vary across the development area.

Site investigations suggest some limitations typical of glacial till soils and site topography/setting will be encountered. These limitations may be overcome by appropriate planning, engineering and site preparation in these areas. Such site features as the depth to restrictive layers, runoff volumes, seasonal soil saturation depths, potential for frost and erosion activity, and jurisdictional wetland areas were examined. The following is a summary of areas and on-site features identified in the field with potential effects relating to the development of this parcel:

- 1. Jurisdictional wetland areas were identified on the property. Alteration to wetland areas will require regulatory permitting together with appropriate engineering to support buildings, septic systems, and roads. Some of these soils contain deep organic deposits, with ponded water or saturated conditions at or near the surface throughout much of the year.
- 2. Moderately deep to deep bedrock classification areas exist in areas throughout the property. These soils include Tunbridge, Becket Variant, and Skerry Variant soils. Bedrock excavation will typically require blasting to achieve design and subgrade elevations, when encountered.

# Section 8

## Limitations

The scope of this investigation has been limited to this Class 'C' Medium High Intensity Soil Survey in general accordance with standards and guidelines established by the Maine Association of Professional Soil Scientists. The soil survey report and soil map have been prepared for the exclusive use of Brandon Chase and Sebago Technics, Inc. for specific application for the proposed Residential Development on this site located on Raymond Cape Road in Raymond, Maine.

No other warranty, expressed or implied, is made. The conclusions and recommendations presented in this soil report are based on data obtained at the referenced site and our interpretations of this information. This report and soil map may not reflect soil variations that may occur between our observation test pits. Data from this soil report and soil map should not be used for any other purpose. Soils which are considered non-limiting for one use may be considered limiting for another use. The soil mapping units used in the soil report and on the soil map are at least in part influenced by the intended use of the soil survey and information provided may not always be adequate for uses other than that which the soil survey was originally developed.

# **APPENDICES**

# **APPENDIX A**

SOIL NARRATIVE REPORT

#### SOIL NARRATIVE REPORT

#### **Brandon Chase**

#### March 11, 2022

Date: Soil profiles observed February 10, 2022

**Base Map:** Lidar topography

2- (two) foot contour intervals on-site

Map Scale 1 inch = 80 feet

Ground Control: Test pits located by GPS with sub-meter accuracy

The Maine Association of Professional Soil Scientists has adopted standards for soil surveys. Soil surveys are divided into four classes of survey, which are dependent upon the amount of information required for the project. The following is a summary of requirements for this Medium High Intensity Soil Survey.

#### **Class C (Medium High Intensity)**

- 1. Map units will not contain dissimilar limiting individual inclusions larger than 5 acres. Dissimilar limiting inclusions may total more than 5 acres per map unit delineation, in the aggregate, if not contiguous.
- 2. Scale of 1 inch equals 500 feet or larger (e.g. 1" = 400').
- 3. Ground control—as determined by the mapper.
- 4. Base map—as determined by the mapper.

The accompanying soil profile descriptions, soil survey map and this soil narrative report were done in accordance with the standards adopted by the Maine Association of Professional Soil Scientists, March 2009.

This Soil Survey was prepared in relation to a proposed residential development.

Khull

Anna K. Biddle, L.S.S. #639



March 11, 2022 Date

# **APPENDIX B**

SOIL LEGEND/MDEP FORM E

#### CLASS 'C' MEDIUM HIGH INTENSITY SOIL SURVEY

SOIL LEGEND

**Brandon Chase** 

Raymond, Maine

March 11, 2022

### SOIL LEGEND

SYMBOL	SOIL SERIES	PHASE	SLOPE	HSG	DRAINAGE CLASS
BeD	BECKET	SANDY LOAM	15-25%	С	WD (WELL DRAINED)
SeA	SEBAGO	MUCKY PEAT	0-3%	D	VPD (VERY POORLY DRAINED)
SkB	SKERRY	FINE SANDY LOAM	3-8%	С	MWD (MODERATELY WELL DRAINED)
SkC	SKERRY	FINE SANDY LOAM	8-15%	С	MWD (MODERATELY WELL DRAINED)
TuC	TUNBRIDGE	FINE SANDY LOAM	8-15%	С	WD (WELL DRAINED)
TuD	TUNBRIDGE	FINE SANDY LOAM	15-25%	С	WD (WELL DRAINED)
WeB	WESTBURY	SANDY LOAM	3-8%	D	SPD (SOMEWHAT POORLY DRAINED)

Project Name:			Applicant Name:	Applicant Name:			Project Location (municipality):			
		×	Description of subsurf	ace materials by:		Depths to	(inches):			
Lot No.	Exploration Symbol (TP 1, B 2, etc.)	if at SSWD Field	<ul> <li>Soil profile/condition</li> <li>Soil series name (if k</li> <li>Geologic unit (if by C</li> </ul>	(if by S.E.), ov C.S.S.), or by	Redoximorphic Features		Hydraulically Restrictive Layer	Limit of Exploration	Ground Surface Slope (%)	Ground Surface Elevation
1										
										<u> </u>
										84.
									WATE OF	Malle
		IN\	ESTIGATOR INFOR	RMATION AND	SIGNATURE			1	S ANN K	A
Signat	ture /-		Khull		[	Date		1110	BIDDL	E
Name	Printed				0	Cert/Lic/Reg. #		tunnawww.	NO 6	E
Qualif	ication		ensed Site Evaluator rtified Geologist		Certified Soil Sc Other:	ientist		af	SCIE	nul seal

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PAGE \_\_\_\_\_ OF \_\_\_\_

SOIL CONDITIONS SUMMARY TABLE

#### FORM E Rev. 07/11

SUMMARY LOG OF SUBSURFACE

**EXPLORATIONS AT PROJECT SITES** 

# **APPENDIX C**

# SOIL SURVEY INTERPRETATIONS

#### SOIL SURVEY INTERPRETATIONS

Soil survey interpretations are derived from the inherent soil characteristics found within the soil profile. The interpretations are predictions (numeric and descriptive) of soil suitability for a specific use, based on the soil's characteristics. These interpretations have many practical applications, such as estimating costs for land development, calculating storm water runoff, determining structural bearing strengths, estimating erodibility, etc. <u>Soil potential ratings</u> have been developed using soil survey interpretations to compare soil series, based on limitations or potentials, for a given use.

#### Limitations of Soil Interpretations

# Soil interpretations are very useful for many purposes and projects, although they do have limitations, including:

- 1. An interpretation for a specific purpose is rarely adaptable for another use without management considerations.
- 2. Use of interpretations for specific areas has an inherent limitation relating to variability of the soil map unit. As the size of the soil survey area and the soil map units increase, soil interpretations provide a less reliable prediction of actual soil conditions.
- 3. Interpretations are also limited by the natural variability within a soil profile, which directly affects the precision of the soil interpretation.
- 4. Soil interpretations are predictions of potentials or limitations based on soil properties. A soil may possess several limiting factors and therefore all site-specific soil properties must be known for accurate interpretations.
- 5. Soil interpretations are used to predict the costs of development and to ultimately determine feasibility of a project. It should be noted that most soil limitations can be overcome with engineering solutions to make a soil suitable for a proposed use.

#### **Soil Potential Rating Factors**

Soil potential ratings have been developed as a useful form of soil interpretations. These ratings are based on local conditions, local experience and expertise, and laws, codes and rules governing the use of soils for various purposes. Potential ratings include the feasibility of a soil for a particular use relative to other soils within a given area. Factors considered in preparing soil potential ratings are the feasibility of using certain technology and practices to overcome limiting factors and the relative cost of implementing these practices. Some examples of unfavorable soil qualities inherent in Maine soils are listed below:

- 1. **Depth to Water Table** The depth to water table affects the natural drainage of the soil in which in turn affects the soils potential for development. A soil with a shallow depth to seasonal high water table requires construction methods such as added fill and artificial drainage to overcome this limitation. A soil with a seasonal high water table deeper than 6 feet below the soil surface would have higher potential than a soil with a seasonal high water table at 18 inches.
- Flooding Soils are rated on the basis of whether they are subject to flooding or not. Flooding is separated into three categories: none, occasional (floods at least once in ten years), and frequent (floods at least once every two years). Soils subject to flooding have less potential for development than those that do not flood.

- 3. **Slope** Soils are rated on the basis of slope. The less sloping areas require fewer corrective measures than the steeper areas and thus have a greater potential for development.
- 4. **Depth to Bedrock** The presence of bedrock affects the use of soils for development. Soils with shallow depth over bedrock have less potential for development than deep soils.
- 5. **Surface Stones** The presence of stones and boulders on the soil surface affect the use of the soil for development. In preparing a site for a dwelling or septic sewage disposal area, surface stones have to be removed.
- 6. **Depth to Restrictive Layer** Some soils have a restrictive layer that begins at a shallow depth. This layer can impede natural drainage and permeability. This soil factor is important when designing a septic sewage disposal system.
- 7. **Soil Profile and Condition** The Maine Subsurface Wastewater Disposal Rules provides a table by which each soil can be categorized by profile group and soil condition. The profile group is based on parent material or origin of the soil, texture of the soil, and the presence of any restricting layer within the soil profile. The soil condition refers to the depth to bedrock or drainage class.

Low density development includes single family unit residences with basements and comparable buildings and septic tank absorption fields, with or without on-site sources of water. Development may be as a single unit or as a cluster of units in a development. Paved roads in a development are also included in the rating. Soil potentials have been developed by selecting the best soil in a county for low density development. This "reference soil" is the best because it has all the best characteristics for all rated uses with regards to development. For low density urban development, a reference soil has the following properties:

- A water table level greater than 6 feet
- The soil does not flood
- Slope is 0-3 percent
- The soil lacks a restrictive layer
- The depth to bedrock is more than 5 feet
- Surface stone cover is 0.1 to 15 percent
- The soil requires a medium sized rating for a septic sewage disposal field
- There is low potential for groundwater contamination from septic field effluent

This reference soil is assigned a value of 100 index points. Costs are also developed for all other soils in the county for overcoming the various soil limitations. These costs are converted to index points and subtracted from the reference soil. The result is a method of comparing development costs for the soils in a county. Environmental constraints as well as long term maintenance costs are also a factor in developing soil potentials.

The Soil Potential index is a mathematical expression of a soil's position in the overall range of potentials which is 100 to 0. Since the entire range is large, these numerical ratings are separated into Soil Potential Rating Classes of very low to very high.

The composite rating for development was determined by a weighted average of individual soil potential indices as follows: septic tank absorption fields, 45 percent; dwellings with basements, 20 percent; and local roads and streets, 35 percent.

#### **Soil Potential Rating Classes**

Soil Potential Rating Classes are based on the expected performance of a soil if feasible measures are taken to overcome its limitations, the cost of such measures, and the magnitude of the limitations that remain after measures have been applied. The development rating (fourth column in the rating tables) is a weighted sum of the septic, dwelling, and road indices. The septic system has the most restrictive site requirements and the dwelling has the least restrictive site requirements.

**Very High Potential** – Site conditions and soil properties are favorable. Installation costs are lowest for that use and there are no soil limitations. Soils in the group have soil properties similar to the reference soil. The Soil Potential Index for this rating class is 100 for each soil use.

**High Potential** – Site conditions and soil properties are not as favorable as the reference soil condition. The cost of measures for overcoming soil limitations is slight. The index for this rating class ranges from 83 to 99 for each soil use.

**Medium Potential** – Site conditions and soil properties are below soils with high potential. Costs of the measures for overcoming soil limitations are significant. The index for this rating class ranges from 60 to 82.

**Low Potential** – Site conditions and soil properties are significantly below soils with medium potential. Costs of measures required to overcome soil limitations are very high. The index for this rating class ranges from 40 to 59 for each soil use.

**Very Low Potential** – There are severe soil limitations for which economical corrective measures are prohibitive or unavailable and costs of these measures are extremely high. Also, soil limitations which detract from environmental quality may continue even after installation of corrective measures. The index for this rating class is less than 40. They may also be prohibited for use by local or state laws.

#### **Drainage Classes**

Drainage classes are the relative wetness that a soil under normal conditions has relating to the soil water table. The following seven drainage classes are used for the soils found in Maine:

- 1. **Excessively Drained (ED)** soils with water that is removed very rapidly. The occurrence of internal free water is very rare or very deep.
- 2. **Somewhat Excessively Drained (SWED)** soils with water that is removed rapidly through the soil. Internal free water occurrence is very rare or very deep.
- 3. **Well Drained (WD)** soils with water that is removed from the soil readily but not rapidly. Internal free water occurrence commonly is deep or very deep.
- 4. **Moderately Well Drained (MWD)** soils with water that is moved somewhat slowly during some periods of the year. Internal free water is moderately deep and transitory to permanent throughout the soil profile.
- 5. **Somewhat Poorly Drained (SWPD)** soils with water that is removed from the soil slowly and remains wet from significant periods of time during the growing season. The depth to internal free water is shallow to moderately deep, transitory to permanent.
- 6. **Poorly Drained (PD)** soils with water that is removed so slowly that the soil is wet at shallow depths during the growing season or remains in a wet state for long periods.

7. **Very Poorly Drained (VPD)** soils with water that is removed from the soil so slowly that the free water remains at or near the ground surface during the growing season. Internal free water is very shallow and persistent or permanent.

#### Slope Class

Α	Level and nearly level	0-3 percent
В	Gently sloping (undulating)	3-8 percent
С	Strongly sloping (rolling)	8-15 percent
D	Moderately steep (hilly)	15-25 percent
Ε	Steep	25-45 percent
F	Very Steep	45+ percent

#### Depth to Bedrock

1.	Very Shallow	Less than 10-inches to bedrock
2.	Shallow	10-inches to less than 20-inches to bedrock
3.	Moderately Deep	20-inches to less than 40-inches to bedrock
4.	Deep	40-inches to less than 60-inches to bedrock
5.	Very Deep	Greater than 60-inches to bedrock

#### **Classes of Surface Stones**

1.	Stony or bouldery	0.01 to 0.1 percent surface coverage
2.	Very stony/ boulder	0.1 to 3.0 percent surface coverage
3.	Extremely stony/ bouldery	3.0 to 15 percent surface coverage
4.	Rubbly	15 to 50 percent surface coverage
5.	Very Rubbly	More than 50 percent surface coverage

#### CLASS 'C' MEDIUM HIGH INTENSITY SOIL SURVEY

#### SOIL POTENTIAL RATINGS

#### **Brandon Chase**

### Raymond, Maine

#### March 11, 2022

#### SOIL POTENTIAL RATING CLASSES

MAP UNIT	SEPTICS	BUILDINGS	ROADS	DEVELOPMENT	
BeD	VERY LOW	MEDIUM	LOW	LOW	
BECKET, 15-25%			LOW	LOW	
SeA	VERY LOW	VERY LOW	VERY LOW	VERY LOW	
SEBAGO, 0-3%					
SkB	HIGH	HIGH	HIGH	HIGH	
SKERRY, 3-8%	mon				
SkC	MEDIUM	MEDIUM	MEDIUM	MEDIUM	
SKERRY, 8-15%	WIEDIOW	INIEDIOINI	INIEDIOINI		
TuC	MEDIUM	MEDIUM	MEDIUM	MEDIUM	
TUNBRIDGE, 8-15%	WIEDIOW	INIEDIOINI	INIEDIOINI		
TuD	VERY LOW	LOW	LOW	VERY LOW	
TUNBRIDGE, 15-25%		2010	1010		
WeB	VERY LOW	MEDIUM	MEDIUM	LOW	
WESTBURY, 3-8%				2010	

# **BECKET (BeD)**

#### (Frigid Oxyaquic Haplorthods)

#### **SETTING**

Parent Material:	Glacial till			
Landform:	Drumlins and glaciated uplands			
Position in Landscape:	High and intermediate positions			
Slope Gradient Ranges:	(D) 15-25%			
COMPOSITION AND SOIL CHARACTERISTICS				
Drainage Class:	Well drained			
Typical Profile:	Surface layer:	Dark brown sandy loam, 8"		
	Subsurface layer:	Reddish brown, friable, gravelly loamy sand, 24"		
	Subsoil layer:	Light olive brown, friable, gravelly sandy loam, 33"		
	Substratum:	Olive, firm, gravelly sandy loam and sand, 65"		
Hydrologic Group:	С			
Surface Runoff:	Slow			
Permeability:	Moderate in the solum, moderately slow to slow in the substratum			
Depth to Bedrock:	Very deep, greater than 60"			
Hazard to Flooding:	None			
INCLUSIONS WITHIN MAPPING UNIT				
Similar:	Hermon, Becket Variant (with bedrock less than 60")			
Contrasting:	Naumburg			

#### **USE AND MANAGEMENT**

Development with subsurface wastewater disposal is rated "fair" due to the restrictive layer in the substratum. A "fair" rating may be used for building site development. Compaction in this soil is rated "good".

# SEBAGO (SeA)

#### (Frigid Fibric Haplohemists)

#### **SETTING**

Parent Material:	Herbaceous and woody organic deposits			
Landform:	Bogs, swamps			
Position in Landscape:	Depressions on glaciated uplands, glaciofluvial deposits			
Slope Gradient Ranges:	(A) 0-3%			
COMPOSITION AND SOIL CHARACTERISTICS				
Drainage Class:	Very poorly drained			
Typical Profile:	Surface layer:	Black mucky peat, massive, 24"		
	Subsoil layer:	Black mucky peat, massive, 36"		
	Substratum:	Very dark gray peat, massive, 65"		
Hydrologic Group:	D			
Surface Runoff:	Ponded or very slow			
Permeability:	Moderately rapid			
Depth to Bedrock:	Very deep, >60"			
Hazard to Flooding:	None			
	INCLUSIONS WITHIN MAPPING UNIT			
Similar:	Naumburg			
Contrasting:	Skerry			

#### **USE AND MANAGEMENT**

Development with subsurface wastewater disposal is "unsuitable" due to wetness and organic soils. A limiting factor for building site development is that the organic soil is unstable and saturated for all or most of the year. Sebago soils are rated "unsuitable" for road fill materials. These soils have "severe" limitations for foundations, underground piping, and roadways due to wetness and unstable organic soils.

# SKERRY (SkB, SkC)

(Frigid Aquic Haplorthods)

#### **SETTING**

Parent Material:	Glacial till				
Landform:	Level to moderately steep uplands				
Position in Landscape:	Higher to intermediate positions				
Slope Gradient Ranges:	(B) 3-8% (C) 8-15%				
COMPOSITION AND SOIL CHARACTERISTICS					
Drainage Class:	Moderately well drained				
Typical Profile:	Surface layer:	Dark brown fine sandy loam, 8"			
	Subsurface layer:	Reddish brown and dark reddish brown gravelly fine sandy loam, 20"			
	Subsoil layer:	Yellowish brown gravelly fine sandy loam, mottled, 25"			
	Substratum:	Grayish brown firm gravelly fine sandy loam, lenses of light olive brown loose sand, 60"			
Hydrologic Group:	С				
Surface Runoff:	Moderate				
Permeability:	Moderate in the solum, slow or very slow in the compact substratum				
Depth to Bedrock:	Very deep, >60"				
Hazard to Flooding:	None				
	INCLUSIONS WITHIN MAPPING UNIT				
Similar:	Becket				
Contrasting:	Naumburg				

#### **USE AND MANAGEMENT**

Subsurface wastewater disposal is "fair" due to wetness and slow percolation rates in the substratum. A limiting factor for building site development is wetness of the soil. Skerry soils also possess large stones and dense compact substratum layers that may require blasting or large construction equipment. Use of this soil for roadways is "fair" due to the large stones and wetness. Underground piping has "moderate" limitations due to wetness and restrictive layer.

# TUNBRIDGE (TuC, TuD)

(Frigid Coarse-loamy Typic Haplorthods)

### **SETTING**

Parent Material:	Loamy glacial till						
Landform:	Glaciated uplands						
Position in Landscape:	Uppermost landforms, sideslopes, shoulders, ridge crests						
Slope Gradient Ranges:	(C) 8-15% (D) 15-25	(C) 8-15% (D) 15-25%					
<u>cc</u>	OMPOSITION AND SOI	L CHARACTERISTICS					
Drainage Class:	Well drained						
Typical Profile :	Surface layer:	Dark brown fine sandy loam, 2"					
	Subsurface layer:	Grayish brown fine sandy loam, 3"					
	Subsoil layer: Substratum:	Dark reddish brown loam, 14" Dark grayish brown gravelly fine sandy Ioam, 28"					
Hydrologic Group:	С						
Surface Runoff:	Slow to rapid, depen	ding upon slope gradient					
Permeability:	Moderate to modera	itely rapid					
Depth to Bedrock:	Moderately deep, 20	to 40" to bedrock surface					
Hazard to Flooding:	None						
	INCLUSIONS WITHIN	MAPPING UNIT					

Similar: Lyman, Abram, Becket Variant (with less than 60" to bedrock)

Contrasting: Dixfield

## **USE AND MANAGEMENT**

The limiting factor for building site development is the depth to bedrock (<40") within this complex. Blasting or ripping of the bedrock is necessary for deep excavation. This unit also possesses field stones of various sizes which may require special management practices to work in these areas.

## WESTBURY (WeB)

(Frigid Typic Fragiaquods)

## **SETTING**

Parent Material:	Glacial till materials				
Landform:	Low areas on glaciat	ed uplands			
Position in Landscape:	Low to intermediate positions				
Slope Gradient Ranges:	(B) 3-8%				
<u>cc</u>	OMPOSITION AND SOI	L CHARACTERISTICS			
Drainage Class:	Somewhat poorly dr	ained			
Typical Profile:	Surface layer:	Very dark gray gravelly sandy loam, 8"			
	Subsurface layer:	Yellowish brown gravelly sandy loam, 15"			
	Subsoil layer:	Gray gravelly sandy loam, 20"; Brown firm gravelly sandy loam, 41"			
	Substratum:	Yellowish brown firm gravelly loamy sand, 60"			
Hydrologic Group:	D				
Surface Runoff:	Low to moderate				
Permeability:	Moderately in the sc	olum, slow to very slow in the substratum			
Depth to Bedrock:	Very deep, >60"				
Hazard to Flooding:	None				
	INCLUSIONS WITHIN	MAPPING UNITS			
Similar:	Skerry Variant (with	bedrock less than 60"), Becket			
Contrasting:	Naumburg				

### **USE AND MANAGEMENT**

Development with subsurface wastewater disposal is "poor" due to a seasonal high water table within 15 inches. Westbury soils also possess large stones that may require blasting or large construction equipment to remove for building site construction. Proper foundation drainage or site modification is recommended for construction. Use of this soil for roadways is "fair" due to the large stones and wetness.

# **APPENDIX D**

**SOIL TEST PITS** 

Detailed Description of Subsurface Conditions at Project Sites

Project Name: Applicant Name: 78 RAYMOND CAPE ROAD			BRANDON CHASE			Project Location (municipality): RAYMOND				
		SOIL DESCRIPTION ANI	D CLASSIFICATION Test Pit	Boring	-	Exploration Symbol:	SOIL DESCRIPTION AN	Test Pit	Boring	
	1-2	Depth of Organic Horizon Above Consistence	e Mineral Soil Color	Redox		1-2 Texture	_" Depth of Organic Horizon Above Consistence	Mineral Soil Color	Redox	
	GRAVELLY SANDY		10YR 4/6 DARK	NONE OBSERVED		SANDY LOAM	FRIABLE	10YR 4/6 DARK	NONE OBSERVED	
	LOAM	FRIABLE	YELLOWISH BROWN			k k		YELLOWISH BROWN		
ches)					SURFACE (Inches)	k 				
SOIL SURFACE (Inches)					CE (III	5 6 				
IRFAC					IRFAC	2				
			2.5Y 5/6 LIGHT			GRAVELLY		2.5Y 5/6		
OS 74			OLIVE BROWN			LOAMY SAND		LIGHT		
					BELOW MINERAL			BROWN		
M MC	COARSE SAND WITH STONES		2.5Y 5/4 LIGHT		M MC					
BELO			OLIVE BROWN		BELC					
HTT H					DEPTH	i				
<u>م</u>	MEDIUM SAND WITH STONES				<u>a</u>	LOAMY	FIRM	5Y 6/2		
48			2.5Y 6/3		50	FINE SAND WITH		LIGHT OLIVE		
108	WITH STONES		LIGHT YELLOWISH BROWN		65	ROTTEN ROCK		GRAY		
	hydric	LEDGE Slope %	AT 108" Limiting factor	ground water	-	hydric	LIMIT OF EXC Slope %	AVATION = 65" Limiting factor	ground water	
•	non-hydric	<u>8-15</u>	108"	<ul> <li>restrictive layer</li> <li>bedrock</li> </ul>	•	non-hydric	<u>3-8</u>	35"	<ul> <li>restrictive layer</li> <li>bedrock</li> </ul>	
L.S.S	Soil Series / phase name:	HERMON	SED	A	L.S.S	Soil Series / phase name:	BECKET	WD	C	
L.S.E.	Soil Classification:	4	Drainage Class B	Hydrologic Group	L.S.E.	Soil Classification:	3	Drainage Class	Hydrologic Group	
	T	Profile SOIL DESCRIPTION ANI	Drainage Class			1	Profile SOIL DESCRIPTION AN	Drainage Class		
	Exploration Symbol:	TP-3 Depth of Organic Horizon Above	Test Pit	Boring		Exploration Symbol:	TP-4	Test Pit	Boring	
	Texture	Consistence	Color	Redox		Texture	Consistence	Color	Redox	
	SANDY LOAM	FRIABLE	10YR 4/6 DARK	NONE OBSERVED		FINE SANDY LOAM	FRIABLE	10YR 4/6 DARK	NONE OBSERVED	
	LOAM	FRIABLE	YELLOWISH	OBGERVED	4	SANDT LOAM	FRIADLE	YELLOWISH		
s)  " "			BROWN		s)			BROWN		
(Inche					(Inches)					
ACE					ACE					
<u>/ERAL SOIL SURFACE (Inches)</u>   12   26   3   3   15   3   3   2   2   2   3					SURFACE	LOAMY		2.5Y 5/6		
			10YR 5/6					LIGHT		
20 22			YELLOWISH BROWN		ERAL    ∞			BROWN		
	LOAMY		2.5Y 6/2			6				
<u>DEPTH BELOW MII</u>	SAND	FIRM	LIGHT BROWNISH		DEPTH BELOW MI		FIRM	2.5Y 6/2 LIGHT		
			GRAY		TH BE			BROWNISH GRAY		
DEP					DEP					
40					40					
50					50					
60		LIMIT OF EXC	CAVATION = 60"		-		LEDG	E AT 52"		
•	hydric non-hydric	Slope % 	Limiting factor	ground water     restrictive layer     bedrock	•	hydric non-hydric	Slope % 3-8	Limiting factor	ground water     restrictive layer     bedrock	
L.S.S	Soil Series / phase name:	BECKET	 Drainage Class	 Hydrologic Group	L.S.S	Soil Series / phase name:	BECKET VARIANT	 Drainage Class	 Hydrologic Group	
L.S.E.	Soil Classification:	<u>3</u> Profile	 Drainage Class		L.S.E.	Soil Classification:	<b>3</b> Profile	C Drainage Class	, , , , ,	
- '		Tiome	Drainage Class				TIONE	Diamage class		
					_			KE OF M	1.10.	
Profe	essional Endorsement	s (as applicable)					ŠG	ANNA	. An II	
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L.S.S	signature:	ran k	Rill			2/10/22	2	BIDDLE	: =	
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<u> </u>	name printed/typed:	name printed/typed: Anna K. Biddle				639			. E	
	S.E. Der Al			Δ				BIDDLE NO. 639		
L.S.E	signature:	Dy	- R 2			ate: 2/10/22 c.#:	TININ,	SCIEN	ST.	

Sebago Technics, Inc.

21397

Detailed Description of Subsurface Conditions at Project Sites

Proje	ect Name: 78 RAYMOND C/	APE ROAD	Applicant Name:	BRANDON CHAS	SE		Project Location (municipality): RAYMOND		
		SOIL DESCRIPTION AN	D CLASSIFICATION Test Pit	Boring		Exploration Symbol:	SOIL DESCRIPTION AN	Test Pit	Boring
0	1-2	Depth of Organic Horizon Abov Consistence	e Mineral Soil Color	Redox		2-3	Depth of Organic Horizon Above	Mineral Soil	Redox
	FINE SANDY LOAM	FRIABLE	10YR 5/4 YELLOWISH BROWN	NONE OBSERVED		1           2         FINE           3         SANDY           4         LOAM	FRIABLE	10YR 4/4 DARK YELLOWISH	NONE OBSERVED
(s _6					(s)	5		BROWN	
SURFACE (Inches)					SOIL SURFACE (Inches)	7 8			
aCE (					ACE (	9 GRAVELLY		10YR 5/4	
					sure.	IZ FINE		YELLOWISH BROWN	
16 18 SOIL 3					-   -   SOIT 3				
BAL 3	GRAVELLY SANDY		2.5Y 5/6 LIGHT		RAL S	GRAVELLY		2.5Y 5/4	
MINE	LOAM		OLIVE BROWN		MINE	SANDY LOAM		LIGHT OLIVE	
DEPTH BELOW MINERAL           [%          %          %          %          %					DEPTH BELOW MINERAL	WITH STONES		BROWN	
TH BE	GRAVELLY LOAMY	FIRM	2.5Y 6/4 LIGHT		TH BE				
DEP	FINE SAND		YELLOWISH BROWN		DEP	18			
40			2.5Y 6/1 GRAY		_4		LEDGI	E AT 38"	
50					6	50			
60		LIMIT OF EXC	CAVATION = 60"		6	50			
•	hydric non-hydric	Slope % 3-8	Limiting factor 28"	ground water     restrictive layer     bedrock	•	hydric non-hydric	Slope % 	Limiting factor 38"	ground water     restrictive layer     bedrock
L.S.S	Soil Series / phase name:	BECKET	 Drainage Class	 Hydrologic Group	L.S.S	Soil Series / phase name	TUNBRIDGE	WD Drainage Class	 Hydrologic Group
L.S.E.	Soil Classification:	3 Profile	C Drainage Class	, <u>, , , , , , , , , , , , , , , , , , </u>	L.S.E.	Soil Classification:	2 Profile	AllI Drainage Class	
	Exploration Symbol:	SOIL DESCRIPTION AN TP-7	D CLASSIFICATION	Boring		Exploration Symbol:	SOIL DESCRIPTION AN TP-8	ID CLASSIFICATION	Boring
	1-2	Depth of Organic Horizon Abov	e Mineral Soil			1-2	Depth of Organic Horizon Above	Mineral Soil	
1	Texture	Consistence	Color	Redox	_	0 Texture	Consistence	Color	Redox
3 4	SANDY LOAM	FRIABLE	10YR 5/4 YELLOWISH BROWN	NONE OBSERVED		2 FINE 3 SANDY 4 LOAM	FRIABLE	7.5YR 3/3 DARK BROWN	NONE OBSERVED
es)					l	6			
(Inch					(Inch	8			
2FACE			10YR 4/4		RFACE				
<u>JERAL SOIL SURFACE (Inches)</u>    2   3   3   1   2   2   0   0   2   4   2   2   3   3   1   2   0   0   2   2   4   2   2   2   2   2   2   2   2   2   2	SANDY		DARK YELLOWISH BROWN		VERAL SOIL SURFACE (Inches)	GRAVELLY		10YR 4/4 DARK	
10S 71		FIRM	2.5Y 5/6 (VARIES)		10S 71	IB LOAM		YELLOWISH BROWN	
	SANDY LOAM		LIGHT		NERA				
<u>DEPTH BELOW MI</u>	WITH STONES		BROWN		IW MO		LEDGI	E AT 24"	
BELO					I I I I°I I I DEPTH BELOW MI	50			
EPTH					EPTH				
40						10			
50					6	50			
56		ASSUMED I	LEDGE AT 56"			80			
•	hydric non-hydric	Slope %	Limiting factor	ground water     restrictive layer	•	hydric non-hydric	Slope % 0-3	Limiting factor	ground water     restrictive layer
L.S.S	Soil Series / phase name:	BECKET	WD	bedrock    C	L.S.S	Soil Series / phase name			bedrock     C
L.S.E.	Soil Classification:	VARIANT 3	Drainage Class	Hydrologic Group	L.S.E.	Soil Classification:	2	Drainage Class <b>Alli</b>	Hydrologic Group
<b></b> ′		Profile	Drainage Class			/	Profile	Drainage Class	
								NE OF M	111.
Profe	essional Endorsement	s (as applicable)						ANNA	N.L.
L.S.S		TK	Riule			Date: 2/10/22	1111	K	
<u> </u>	signature:					ic.#:	Ĩ	BIDDLE NO, 639	: :
<u> </u>	name printed/typed:	Anna K. Bi	ddle	^		639		110.008	. / 5
L.S.E.	signature:	De	- R 1			Date: 2/10/22	10	CENSE	A LINE
	name printed/typed:	Gary M. Fu	llerton			.ic.#: 355	affix professional seal	" OUEN	1111

Sebago Technics, Inc.

Detailed Description of Subsurface Conditions at Project Sites

	Project Name: Applicant Name: 78 RAYMOND CAPE ROAD BRANDON CHASE					Project Location (municipality):			
	78 RATMOND C			BRANDON CHAS				RAYMOND	
	Exploration Symbol:	SOIL DESCRIPTION AN TP-9	Test Pit	Boring		Exploration Symbol:	SOIL DESCRIPTION AN TP-10	D CLASSIFICATION Test Pit	Boring
		Depth of Organic Horizon Abov	-	Domig			Depth of Organic Horizon Above		
	Texture	Consistence	Color	Redox	0	Texture	Consistence	Color	Redox
-1	2 SANDY	FRIABLE	10YR 4/4		2	FINE	FRIABLE	10YR 4/3	NONE
3	3 LOAM		DARK YELLOWISH		3	SANDY LOAM		BROWN	OBSERVED
5	5		BROWN		4	LOAM			
es)	8				• es)				
SURFACE (Inches)	8		-		(Inches)   *   _				
- GE	GRAVELLY		2.5Y 5/6						
	2 SANDY		LIGHT		SURFACE	0000/5117			
14 15 11			OLIVE BROWN			GRAVELLY FINE		10YR 5/4 YELLOWISH	
S _18						SANDY LOAM		BROWN	
20   20			-			LOAM			
NIW	8				INIW27				
м М		CIDM.	0.5%.5%		BELOW MINERAL 8   2   2   8		LEDGE	AT 27"	
130 32		FIRM	2.5Y 5/4 LIGHT		BEL				
DEPTH 8			OLIVE BROWN	COMMON, MEDIUM,	DEPTH				
H 39	9		BROWN	AND DISTINCT	E E				
40	LOAMY		2.5Y 6/2		40				
50			LIGHT		50				
60	0		BROWNISH GRAY		60				
-	hydric	LIMIT OF EXC Slope %	CAVATION = 60"	ground water		budrio	Slope %	Limiting factor	ground water
	non-hydric	3-8	Limiting factor	<ul> <li>restrictive layer</li> </ul>		hydric non-hydric	3-8	27"	restrictive layer
	Soil Series / phase name:			bedrock     C		Soil Series / phase name		 WD	bedrock     C
L.S.S			Drainage Class	Hydrologic Group	L.S.S	con conce / phace hame		Drainage Class	Hydrologic Group
L.S.E.	Soil Classification:	3_ Profile	 Drainage Class		L.S.E.	Soil Classification:	 Profile	AllI Drainage Class	Design Class
	I	SOIL DESCRIPTION AN	ID CLASSIFICATION				SOIL DESCRIPTION AN	D CLASSIFICATION	
	Exploration Symbol:	TP-11	Test Pit	Boring		Exploration Symbol:	TP-12	Test Pit	Boring
0	Texture	" Depth of Organic Horizon Abov Consistence	ve Mineral Soil Color	Redox	0	Texture	Consistence	Mineral Soil Color	Redox
	1			NONE	1				MANY, COARSE,
3	2 SANDY 3 LOAM	FRIABLE	10R 4/6 DARK	OBSERVED	3	COARSE SAND	FRIABLE	2.5Y 5/2 GRAYISH	AND PROMINENT
4	4		YELLOWISH BROWN		4	WITH STONES		BROWN	
(s)	6		Bitofin		(s)	UT ON LO			
nche	8		+		(Inches)				
SURFACE (Inches)	9								
					<sup>9</sup> SURFACE				
0 14 16			2.5Y 5/6						
OS 18	SANDY				16				
ERAL SOIL	DI LOAM		LIGHT						
18 -	WITH STONES				ERAL SOIL	VERY FINE			
	WITH STONES		LIGHT OLIVE		NERAL	VERY FINE SAND			
			LIGHT OLIVE		NERAL	SAND			
			LIGHT OLIVE		BELOW MINERAL	FINE	FIRM		
		FIRM	LIGHT OLIVE BROWN 2.5Y 6/3		BELOW MINERAL	SAND	FIRM		
		FIRM	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH		NERAL	SAND FINE SANDY	FIRM		
DEPTH BELOW MIN            s                     s	0 0 0 0 0 0 0 0 0 0 0	FIRM	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT		DEPTH BELOW MINERAL            s                    s                    s	SAND FINE SANDY	FIRM		
		FIRM	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4		BELOW MINERAL	SAND FINE SANDY		AVATION = 42"	
DEPTH BELOW MIN           [*  *  *            *                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              <	LOAMY SAND		LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN		DEPTH BELOW MINERAL            s                    s                    s	SAND FINE SANDY		AVATION = 42"	
DEPTH BELOW MIN 8 + 8 + 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	LOAMY SAND	LIMIT OF EXC	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60"		DEPTH BELOW MINERAL	SAND FINE SANDY LOAM	LIMIT OF EXC		
DEPTH BELOW MIN	LOAMY SAND	LIMIT OF EXC Slope %	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor	ground water restrictive layer	DEPTH BELOW MINERAL            s                    s                    s	SAND FINE SANDY	LIMIT OF EXC	Limiting factor	
	LOAMY     SAND     hydric     non-hydric	LIMIT OF EXC Slope % 3-8	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor 30"	<ul> <li>restrictive layer</li> <li>bedrock</li> </ul>	DEPTH BELOW MINERAL	SAND FINE SANDY LOAM hydric non-hydric	LIMIT OF EXC	Limiting factor	<ul> <li>restrictive layer</li> <li>bedrock</li> </ul>
DEPTH BELOW MIN           8         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1		LIMIT OF EXC Slope % 3-8 BECKET	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHTOLIVE BROWN CAVATION = 60" Limiting factor  	<ul> <li>restrictive layer</li> </ul>		SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer
	LOAMY     SAND     hydric     non-hydric	LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor  	restrictive layer     bedrock     C	DEPTH BELOW MINERAL	SAND FINE SANDY LOAM hydric non-hydric	LIMIT OF EXC Slope % 	Limiting factor	restrictive layer     bedrock     D
		LIMIT OF EXC Slope % 3-8 BECKET	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHTOLIVE BROWN CAVATION = 60" Limiting factor  	restrictive layer     bedrock     C	DEPTH BELOW MINERAL DEPTH BELOW MINERAL S''''''''''''''''''''''''''''''''''''	SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock     D
		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor  	restrictive layer     bedrock     C	DEPTH BELOW MINERAL DEPTH BELOW MINERAL B	SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock     D
		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor  	restrictive layer     bedrock     C	DEPTH BELOW MINERAL DEPTH BELOW MINERAL B	SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock     D
DE LLH BEFOM WIV		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor  	restrictive layer     bedrock     C	DEPTH BELOW MINERAL DEPTH BELOW MINERAL B	SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock       Hydrologic Group
VIW MOTAL REPORT		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor  Chainage Class  Drainage Class	restrictive layer     bedrock     C     Hydrologic Group	R     R   S   -   -   -   -   -   -   -   -   -	SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock       Hydrologic Group
DE LLH BEFOM WIV		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor  	restrictive layer     bedrock     C     Hydrologic Group	R     R   S   -   -   -   -   -   -   -   -   -	SAND FINE SANDY LOAM Nydric non-hydric Soil Series / phase name Soil Classification:	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock       Hydrologic Group
VIW MOTAL REPORT		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor 	restrictive layer     bedrock     C     Hydrologic Group	DE D	SAND FINE SANDY LOAM LOAM hydric non-hydric Soil Series / phase name Soil Classification: ate: 2/10/22 c.#:	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock       Hydrologic Group
VIW MOTAL AND A CONTRACT OF A		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor 	restrictive layer     bedrock     C     Hydrologic Group	DE D	SAND FINE SANDY LOAM hydric non-hydric Soil Series / phase name Soil Classification:	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock       Hydrologic Group
Profe		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor 	restrictive layer     bedrock     C     Hydrologic Group		SAND FINE SANDY LOAM LOAM Soll Series / phase name Soll Classification: Soll Classification: 2/10/22 #: 639	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock       Hydrologic Group
VIW MOTAL AND A CONTRACT OF A		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor 	restrictive layer     bedrock     C     Hydrologic Group		SAND FINE SANDY LOAM LOAM hydric non-hydric Soil Series / phase name Soil Classification: Soil Classification: ate: 2/10/22 s:#: 639 ate:	LIMIT OF EXC Slope % 	Limiting factor 	restrictive layer     bedrock     D     Hydrologic Group
Profe		LIMIT OF EXC Slope % 	LIGHT OLIVE BROWN 2.5Y 6/3 LIGHT YELLOWISH BROWN 2.5Y 5/4 LIGHT OLIVE BROWN CAVATION = 60" Limiting factor 	restrictive layer     bedrock     C     Hydrologic Group		SAND FINE SANDY LOAM LOAM Soll Series / phase name Soll Classification: Soll Classification: 2/10/22 #: 639	LIMIT OF EXC Slope % 	Limiting factor  	restrictive layer     bedrock       Hydrologic Group

21397

Sebago Technics, Inc.

Detailed Description of Subsurface Conditions at Project Sites

Proje	ect Name:		Applicant Name:		ANDON CHASE RAYMOND					
	78 RAYMOND C			BRANDON CHAS			SOIL DESCRIPTION AND CLASSIFICATION			
	Exploration Symbol:	SOIL DESCRIPTION AND TP-13	Test Pit	Boring		Exploration Symbol:	SOIL DESCRIPTION AN TP-14	Test Pit	Boring	
		" Depth of Organic Horizon Above	-				_ Depth of Organic Horizon Above			
	Texture	Consistence	Color	Redox	-	Texture	Consistence	Color	Redox	
2	FINE	FRIABLE	10YR 5/6			FINE	FRIABLE	10YR 5/6		
	SANDY LOAM		YELLOWISH BROWN		-	SANDY		YELLOWISH BROWN		
5						WITH STONES				
hes)					(Inches)	3				
SURFACE (Inches)					un)	3				
ACE					SURFACE					
10						3				
DS 18								2.5Y 5/4	COMMON, MEDIUM,	
NER.					NER.			LIGHT	AND DISTINCT	
BELOW MINERAL SOIL 26   6   8					BELOW MINERAL	3		BROWN		
					107=	SANDY LOAM	FIRM	5Y 5/2	MANY, COARSE,	
18 - 32	SANDY LOAM	FIRM	2.5Y 5/4 LIGHT	COMMON, MEDIUM,	H BI	WITH STONES		OLIVE GRAY	AND PROMINENT	
DEPTH	WITH STONES		OLIVE	AND DISTINCT	DEPTH			0.011		
40			BROWN		4					
60		LIMIT OF EXC	AVATION = 60"		9	2	LIMIT OF EXC	AVATION = 92"		
•	hydric non-hydric	Slope %	Limiting factor	<ul> <li>ground water</li> <li>restrictive layer</li> </ul>	•	hydric non-hydric	Slope %	Limiting factor	<ul> <li>ground water</li> <li>restrictive layer</li> </ul>	
<b>_</b>		<u> </u>		bedrock			3-8		bedrock	
L.S.S	Soil Series / phase name:	SKERRY	<b>MWD</b> _ Drainage Class	 Hydrologic Group	L.S.S	Soil Series / phase name:	SKERRY	 Drainage Class	 Hydrologic Group	
L.S.E.	Soil Classification:	3	C		L.S.E.	Soil Classification:	3	C		
<b>–</b> ′		Profile SOIL DESCRIPTION AND	Drainage Class D CLASSIFICATION			·	Profile SOIL DESCRIPTION AN	Drainage Class D CLASSIFICATION		
	Exploration Symbol:	TP-15	Test Pit	Boring		Exploration Symbol:	TP-16	Test Pit	Boring	
	1-2_	Depth of Organic Horizon Above	Mineral Soil	Redox		Texture	_ Depth of Organic Horizon Above Consistence	Mineral Soil Color	Redox	
1						1				
_2	COBBLY FINE	FRIABLE	10YR 4/6 DARK	NONE OBSERVED	-	FINE SANDY	FRIABLE	10YR 4/6 DARK	NONE OBSERVED	
4	SANDY		YELLOWISH			LOAM		YELLOWISH		
() -5	LOAM		BROWN		<u> </u>	3		BROWN		
SURFACE (Inches)					(Inches)	7				
18 -					5 - U	9				
					SURFACE					
						1				
16 10S						3				
					I Io	SANDY LOAM		2.5Y 5/6 LIGHT		
ININ 26					<	WITH STONES		OLIVE BROWN		
18 _		LEDGE	E AT 26"		I°      BELOW MI			BROWN		
BELO					°∣ BEL(	0				
HL -					DEPTH		FIRM	5Y 5/2 OLIVE		
<u> </u>					DE			GRAY		
40					_4					
50					5					
60					6	0	<u> </u>			
-	hydric	Slope %	Limiting factor	ground water	0	hydric	LIMIT OF EXC Slope %	AVATION = 60" Limiting factor	ground water	
•	non-hydric	8-15	26"	<ul> <li>restrictive layer</li> <li>bedrock</li> </ul>	•	non-hydric	3-8	30"	<ul> <li>restrictive layer</li> <li>bedrock</li> </ul>	
L.S.S	Soil Series / phase name:	TUNBRIDGE	WD	Dedrock	L.S.S	Soil Series / phase name:	BECKET	WD	C	
	0.11.01.17.11		Drainage Class	Hydrologic Group			<u>^</u>	Drainage Class	Hydrologic Group	
L.S.E.	Soil Classification:	 Profile	<b>AIII</b> Drainage Class		L.S.E.	Soil Classification:	<b>3</b> Profile	Drainage Class		
								VE OF M	111	
								A	SIN'S	
Prote	essional Endorsement						50	ANNA	. M =	
L.S.S	A	XK	Rille	-	D	ate:		K.		
	signature:					2/10/22	_	BIDDLE	1 3	
		Anna K. Bio	ddlo			c.#: 639	= 1	NO. 639	i i i	
<u> </u>	name printed/typed:		uule	1		003				
L.S.E.		( )	1 )	1_	D	ate:	1.	CENSE	XX 3	
	signature:	Chy	- 12			2/10/22	10	1	112.11	
					Li	c.#:		1, SCIEN	in	
	name printed/typed: Gary M. Fullerton					355	affix professional seal			

Detailed Description of Subsurface Conditions at Project Sites

Proj	ect Name: 78 RAYMOND C	APE ROAD	Applicant Name:	BRANDON CHAS	SE .	-	Project Location (m	unicipality): RAYMOND	
		SOIL DESCRIPTION ANI	D CLASSIFICATION				SOIL DESCRIPTION A	ND CLASSIFICATION	
	Exploration Symbol:	TP-17 _" Depth of Organic Horizon Above	Test Pit	Boring		Exploration Symbol:	TP-18 Depth of Organic Horizon Abov	Test Pit	Boring
_	Texture	Consistence	Color	Redox	_	• Texture	Consistence	Color	Redox
		FRIABLE	10YR 4/6 DARK	NONE OBSERVED	=	2 FINE 3 SANDY	FRIABLE	10YR 4/6 DARK	
			YELLOWISH BROWN	OBOLITED		LOAM		YELLOWISH BROWN	
(se)	5		BROWN		(se	6		BROWN	
(Inche	3				(Inche	8			
ACE					- ACE			2.5Y 5/4	
SUR <sup>1</sup>	4				SURF	4		LIGHT OLIVE	
1   1 SOIL					TIOS			BROWN	
	SANDY		2.5Y 5/4		ERAL    ₀	0			
- MINE	LOAM WITH STONES		LIGHT OLIVE		NINE				
DEPTH BELOW MINERAL SOIL SURFACE (Inches)	5		BROWN		BELOW MINERAL SOIL SURFACE (Inches)	LOAMY SAND	SOMEWHAT FIRM	2.5Y 5/2 GRAYISH	COMMON, MEDIUM, AND DISTINCT
TH BE		LEDGI	E AT 30"		TH BE			BROWN	
DEP.					DEPTH	8			
4	2				4	0	LEDG	E AT 38"	
_5	2				5	10			
_6	5				_6	0			
•	hydric non-hydric	Slope %	Limiting factor	ground water     restrictive layer	•	hydric non-hydric	Slope %	Limiting factor	ground water     restrictive layer
	Soil Series / phase name:	3-8	<u>30"</u>	bedrock     C_		Soil Series / phase name:	3-8 SKERRY		D
L.S.S			Drainage Class	Hydrologic Group	L.S.S		VARIANT	Drainage Class	Hydrologic Group
L.S.E.	Soil Classification:	2_ Profile	<b>Alli</b> Drainage Class		L.S.E.	Soil Classification:	 Profile	<b>C</b> Drainage Class	
	Exploration Symbol:	SOIL DESCRIPTION ANI TP-19	Test Pit	Boring	-	Exploration Symbol:	SOIL DESCRIPTION AN TP-20	Test Pit	Boring
		" Depth of Organic Horizon Above		- Dedau			Depth of Organic Horizon Abov		Deden
		Consistence	Color	Redox		Texture	Consistence	Color	Redox
	2 SANDY 3 LOAM	FRIABLE	10YR 4/6 DARK	NONE OBSERVED		3 LOAM	FRIABLE	2.5Y 5/3 LIGHT	
	5		YELLOWISH BROWN			4 WITH 5 COARSE SAND		OLIVE BROWN	
thes)	3				ches)	6 LENSES			
— (ho	3				E (ho	9			
					RFAC				
JERAL SOIL SURFACE (Inches)	3				SOIL SURFACE (Inches)				
OS 71			2.5Y 5/6 LIGHT		1 20			2.5Y 5/4 LIGHT	MANY, COARSE, AND PROMINENT
	LOAM WITH STONES		OLIVE BROWN		VER/			OLIVE BROWN	
DEPTH BELOW MIN		FIRM	2.5Y 5/2		DEPTH BELOW MI		FIRM	2.5Y 5/2	
BELO	5		GRAYISH BROWN		l°   I°	0		GRAYISH BROWN	
HTH -					PTH 				
					ШШ —				
					4			CAVATION = 48"	
					6				
-5	4 hydric	LIMIT OF EXC Slope %	AVATION = 54" Limiting factor	ground water	-	hydric	Slope %	Limiting factor	<ul> <li>ground water</li> </ul>
•	non-hydric	3-8	24"	<ul> <li>ground water</li> <li>restrictive layer</li> <li>bedrock</li> </ul>	•	non-hydric	3-8	13"	<ul> <li>ground water</li> <li>restrictive layer</li> <li>bedrock</li> </ul>
L.S.S	Soil Series / phase name:	BECKET	WD	C	L.S.S	Soil Series / phase name:	WESTBURY	SPD	D
L.S.E.	Soil Classification:	3	Drainage Class	Hydrologic Group	L.S.E.	Soil Classification:	3	Drainage Class <b>D</b>	Hydrologic Group
	·	Profile	Drainage Class				Profile	Drainage Class	
								NUC OF A	111.
		/ r // \						ALE	SIN'S
	essional Endorsement		4				19	ANNA	.iu =
L.S.S	-	AK	Rille			Date: 2/10/22	3		1 1
	signature:	-			L	ic.#:		BIDDLE NO. 639	1 3
	name printed/typed:	Anna K. Bi	ddle			639		10.059	
L.S.E		( )	1 1	1		Date:	II.	S CENSE	8× 3
<u> </u>	signature:	Cho	- 19			2/10/22	- 11	Think	
	name printed/typed:	Gary M. Fu	llerton		ľ	ic.#: 355	affix professional seal	ANNA K BIDDLE NO. 639 CENSE SCIEN	111.
<u> </u>	I						1 prorocoloriar ocal		

Detailed Description	of Subsurface	Conditions at Project Sites	

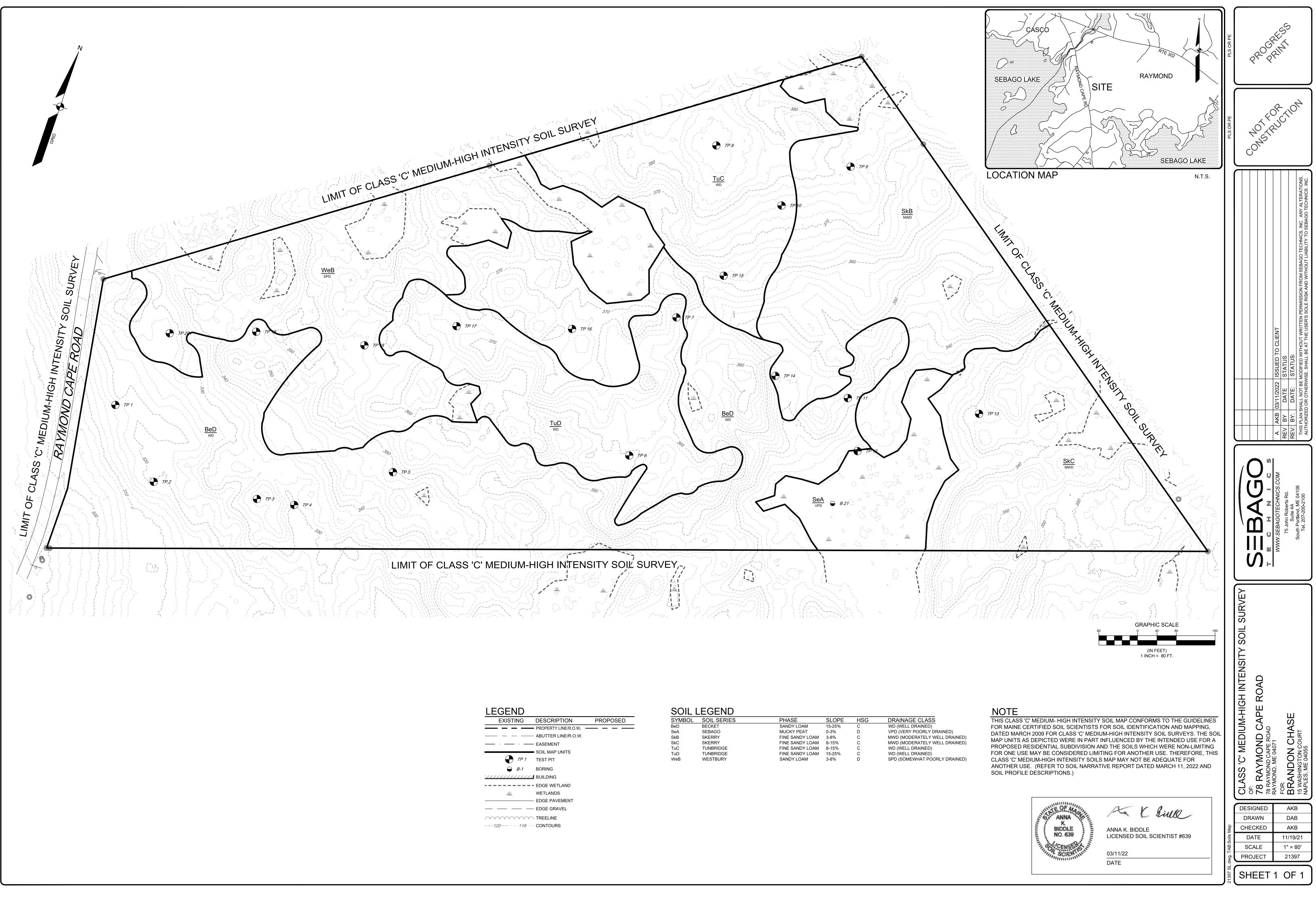
Proje	ect Name: 78 RAYMOND C	APE ROAD	Applicant Name:	BRANDON CHAS	E		Project Location (municipality): RAYMOND				
	Exploration Symbol:	SOIL DESCRIPTION AN	Test Pit	Boring		Exploration Symbol:		SOIL DESCRIPTION AND CLASSIFICATION Test Pit Boring			
	>48" Texture	_" Depth of Organic Horizon Abov Consistence	e Mineral Soil Color	Redox	_	• Texture	Depth of Organic Horizon Above Consistence	Mineral Soil Color	Redox		
 	SAPRIC ORGANIC	FRIABLE	2.5Y 2.5/1 BLACK	NONE OBSERVED		1 2 3 4					
						5 8					
SURFACE (Inches)					SURFACE (Inches)	7		/			
CE (#					10 – 10 – 10 – 10 – 10 – 10 – 10 – 10 –	9					
					JRFAC L_ L_	2					
16					12 -	6					
47 SC					47 SC						
NER.					NER.						
BELOW MINERAL					BELOW MINERAL						
BELC					BELC	10					
DEPTH					HTH:						
48			CAVATION = 48"		4		1				
		Class - 9/	l institue e ferster	-				l institue e Constant			
	hydric non-hydric	Slope % 	Limiting factor	ground water     restrictive layer     bedrock    D_	•	hydric non-nydric	Slope %	Limiting factor	ground water     restrictive layer     bedrock		
L.S.S	Soil Series / phase name:		Drainage Class	Hydrologic Group	L.S.S	Soil Series / phase name		Drainage Class	Hydrologic Group		
L.S.E.	Soil Classification:	<b>10</b> Profile	E Drainage Class		LSE.	Soil Classification:	Profile	Drainage Class	Design Class		
	Exploration Symbol:	SOIL DESCRIPTION AN	D CLASSIFICATION Test Pit	Boring	$\square$	Exploration Symbol:	SOIL DESCRIPTION AN	D CLASSIFICATION Test Pit	Boring		
		Depth of Organic Horizon Abov	e Mineral Soil				Depth of Organic Horizon Above	Mineral Soil			
1	Texture	Consistence	Color	Redøx		0 Texture	Consistence	Color	Redox		
2						3					
5						5					
hes)			/		hes)	6		/			
= (Inc					 	8					
SURFACE (Inches)					SURFACE (Inches)						
10 S 7						4		-/			
OS 18			/		20	8		/			
VERAL     <sub>8</sub>		/					/				
107 <u>3</u>					107 <u>3</u>	10					
<u>DEPTH BELOW MII</u>					°       DEPTH BELOW MI						
					-						
40	/				4	/					
0											
	hydric non-hydric	Slope %	Limiting factor	ground water     restrictive layer     bedrock	0	hydric non hydric	Slope %	Limiting factor	ground water     restrictive layer     bedrock		
L.S.S	Soil Series / phase name: Soil Classification:		Drainage Class	Hydrologic Group	L.S.S	Soll Series / phase name Soil Classification:	:	Drainage Class	Hydrologic Group		
L.S/E.		Profile	Drainage Class	Design Class	L.S.E.		Profile	Drainage Class	Design Class		
								Num of the	11.		
								XE OF M	Sinte		
Profe	essional Endorsement				1		50	ANNA	. m I		
L.S.S	-	K	Rull			Date: 2/10/22		K. BIDDLE			
	signature:				L	ic.#:	1	NO. 639			
<u> </u>	name printed/typed:	Anna K. Bi	ddle			639			. / E		
L.S.E		De	- R 2			Date: 2/10/22	110	CENSE	is in		
	name printed/typed: Gary M. Fullerton					ic.#: <b>355</b>	affix professional seal	SCIEN	SCIEN		

Sebago Technics, Inc.

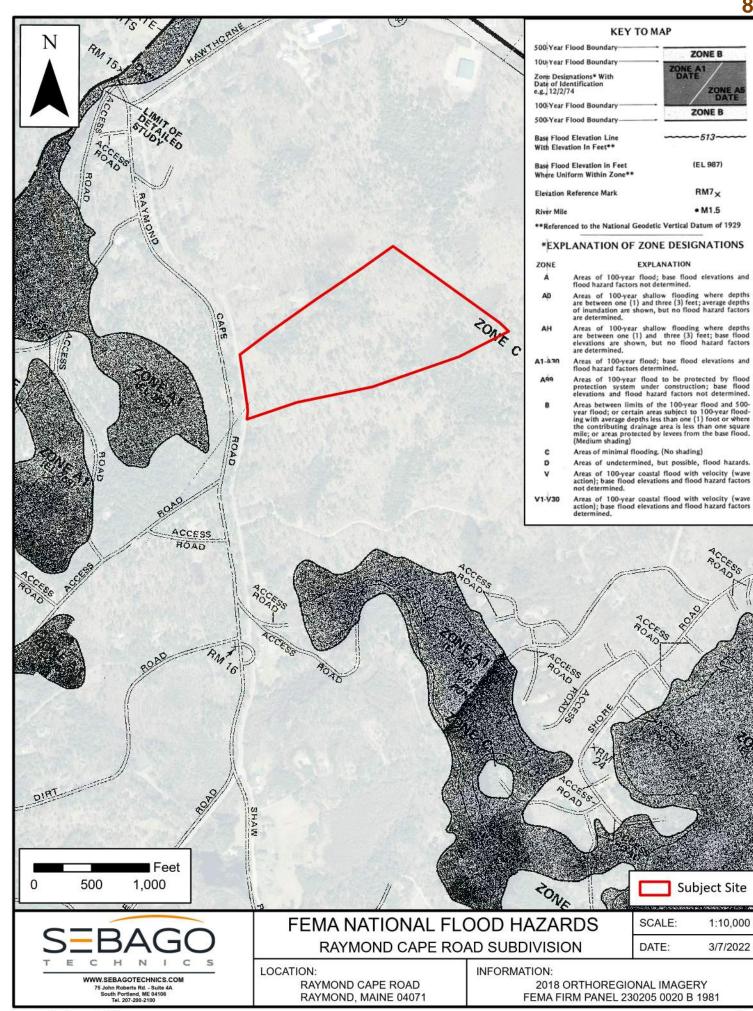
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# **APPENDIX E**

# CLASS 'C' MEDIUM HIGH INTENSITY SOIL MAP



LEGEND			SOIL L	EGEND				
EXISTING	DESCRIPTION	PROPOSED	SYMBOL	SOIL SERIES	PHASE	SLOPE	HSG	DRAINA
	- PROPERTY LINE/R.O.W		BeD	BECKET	SANDY LOAM	15-25%	С	WD (WELL
			SeA	SEBAGO	MUCKY PEAT	0-3%	D	VPD (VER)
	<ul> <li>ABUTTER LINE/R.O.W.</li> </ul>		SkB	SKERRY	FINE SANDY LOAM	3-8%	С	MWD (MOI
· ·	- EASEMENT		SkC	SKERRY	FINE SANDY LOAM	8-15%	С	MWD (MOI
			TuC	TUNBRIDGE	FINE SANDY LOAM	8-15%	С	WD (WELL
	SOIL MAP UNITS		TuD	TUNBRIDGE	FINE SANDY LOAM	15-25%	С	WD (WELL
TP 1	TEST PIT		WeB	WESTBURY	SANDY LOAM	3-8%	D	SPD (SOM
🕒 В-1	BORING							
<u> </u>								
	- EDGE WETLAND							
<u>_\  _</u>	WETLANDS							
	— EDGE PAVEMENT							
	— EDGE GRAVEL							
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Floodplain Map, 21397.aprx

Project Number: 21397