

Stormwater Management Report

for

Proposed New Construction

165 Raymond Hill Road Raymond, Maine 04071

September 29, 2020

<u>Applicant</u> Jeffrey S. Buckley P.O. Box 679 Raymond, Maine 04071

<u>Prepared By</u> Walsh Engineering Associates, Inc. 1 Karen Drive, Suite 2A Westbrook, Maine 04092



Introduction

Walsh Engineering Associates, Inc. (WEA) was retained to assist Jeffrey S. Buckley (Applicant) in the review of the stormwater management of 165 Raymond Hill Road. A site plan prepared by WEA titled "Driveway & Site Development Plan" dated September 24, 2020 has been enclosed with this review for reference. The Applicant proposes a $2,700\pm$ square foot single family home and $560\pm$ foot long, 14-foot-wide gravel driveway. The site currently consists of forest with a cleared meadow.

Methodology

The stormwater runoff analysis has been undertaken utilizing the HydroCAD Stormwater Modeling System software (Version 10) developed by the Applied Microcomputer Systems of Chocorua, New Hampshire. The program is based upon the TR-20 computer program and the TR-55 tabular method, both of which are based upon techniques developed by the USDA Soil Conservation Service. The analysis was undertaken for the 2-, 10-, and 25-year frequencies (3.0, 4.3, and 5.4 inches, respectively). Twenty-four-hour storms with a Type III distribution were the basis for the analysis.

Pre-Development Conditions

The property is currently forested with a small cleared meadow area. Stormwater runoff from the site flows northwest to the abutting property.

The medium intensity National Cooperative Soil Survey generated by the Natural Resource Conservation Service Web Soil Survey indicates that there are Paxton and Woodbridge soils present. All soils within the development area are classified as hydrologic soil group (HSG) C. The medium intensity soil survey can be found in Appendix B. The hydrologic soil group boundaries are shown on drawings D1.0 – Pre-development Drainage Plan and D2.0 – Post-development Drainage Plan in the attached plan set.

Runoff from the site was analyzed where it leaves the property to the northwest (AP1). Predevelopment HydroCAD calculations can be found in Appendix A and shown on sheet D1.0 -Pre-development Drainage Plan. Pre-development peak flow rates at the analysis point are summarized in Table 1 for the 2, 10, and 25-year storm events.

Post-Development Conditions

Site development includes the construction of a $2,700\pm$ square foot single family home and a $560\pm$ foot long, 14-foot-wide gravel driveway. Runoff from the driveway will be captured in a roadside swale and brought to a 100' wide forested buffer. The project will create approximately $8,700\pm$ square feet of impervious area and clear 17,400 square feet of forested area.



Post-development HydroCAD calculations can be found in Appendix B and sheets D2.0 – Post Development Drainage Plan can be found in the attached plan set. Post-development peak flow rates at the analysis points are summarized in Table 1 for the 2, 10, 25, and100-year storm event.

Stormwater Quantity

The Town of Raymond's Stormwater Management Standards require that the peak flow rates discharging from the site are not increased as a result of the development. The development of the site will not cause any change in the curve number of the subcatchment; therefore, post development peak flow rates will remain the same as in the pre-development conditions.

Table 1 – Peak Flow Rates (cfs)							
Analysis Point #1 (AP1)	2-Year Storm	10-Year Storm	25-Year Storm				
Pre-Development	4.81	11.07	17.11				
Post Development	4.81	11.07	17.11				

As shown in Table 1, the post-development peak runoff rate at the analysis point will remain equal to the pre-development runoff rate for the 2, 10, and 25-year storm events.

Stormwater Quality

The Town of Raymond's Stormwater Management Standards as described in Section 9.X "Stormwater Quality and Phosphorus Control" of the Raymond Land Use Ordinance utilize a point system in determining if a development achieves acceptable stormwater quality requirements.

Table 2 – Stormwater Point System					
1) Point Credits	Value				
a) Correcting an Existing Erosion Problem	10				
f) 100 ft Wide Wooded Buffer	40				
Total	50				

As shown in Table 2, the development achieves 50 points based on the Stormwater Point System and point schedule outlined in the Raymond Land Use Ordinance. The project intends on improving the existing gravel road's erosion problems for a 10-point credit.

Erosion Control

BMPs such as silt fence and/or filter berms of erosion control mix, mulch, and temporary seeding will be used to prevent erosion and downstream migration of sediment during construction. Permanent erosion control measures include compacted gravel surfaces and permanent seeding.



Conclusions

The HydroCAD calculations show that the peak runoff rates at the analysis point under postdevelopment conditions are estimated to be equal to the peak pre-development runoff rates for the 2-, 10-, and 25-year storm events. It is our opinion that the proposed stormwater management plan meets the requirements of the Town of Raymond's regulations.

Respectfully,

Connor Ritter

Connor A. Ritter, EIT Walsh Engineering Associates, Inc.

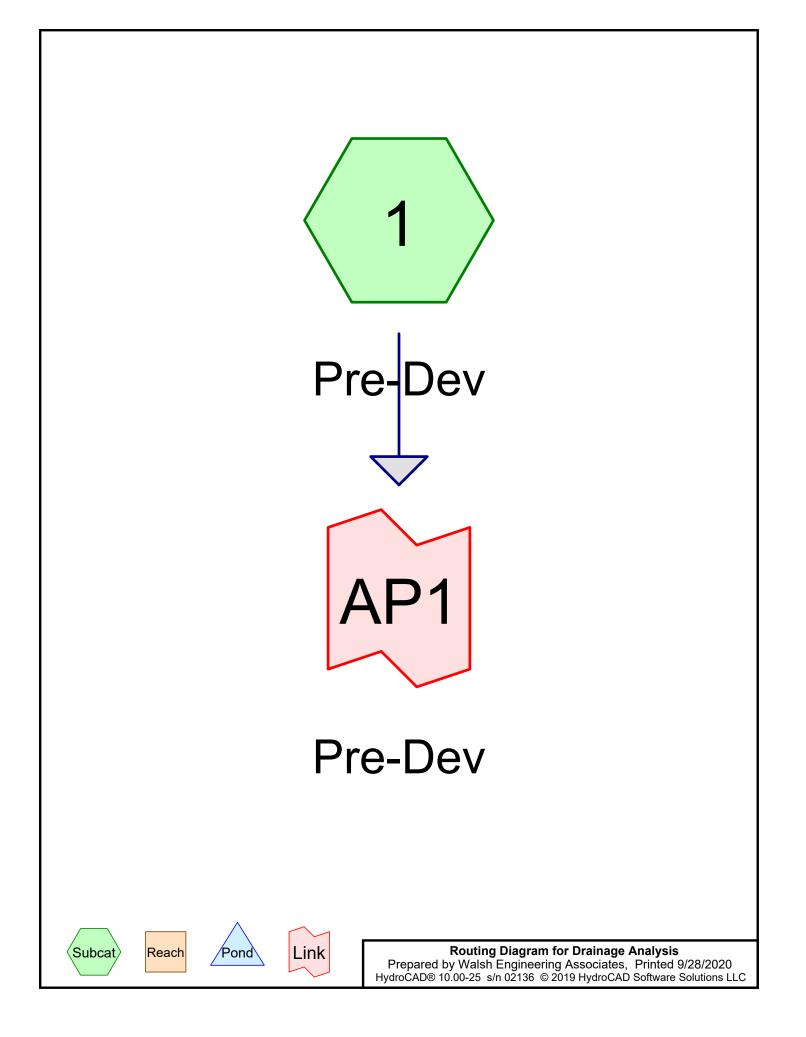
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William R. Walsh III, PE Walsh Engineering Associates, Inc.

SUPPORTING DATA AND CALCULATIONS

The following material presents calculations and copies of source material used during the analysis for this study.

- Appendix A: HydroCAD Report
- Appendix B: Web Soil Survey Map
- Appendix C: Drainage Plans
 - D1.0 Pre-Development Drainage Plan
 - D2.0 Post Development Drainage Plan



Area Listing (selected nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
20,800	98	Impervious (1)
30,500	71	Meadow, non-grazed, HSG C (1)
565,900	70	Woods, Good, HSG C (1)

Summary for Subcatchment 1: Pre-Dev

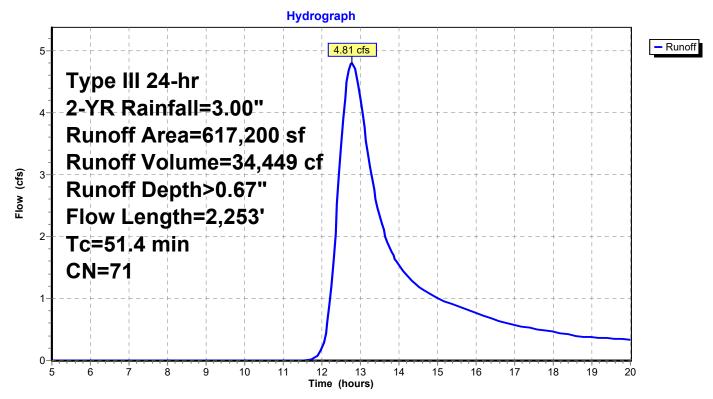
Runoff = 4.81 cfs @ 12.78 hrs, Volume= 34,449 cf, Depth> 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YR Rainfall=3.00"

_	A	rea (sf)	CN I	Description		
	5	65,900	70	Woods, Go	od, HSG C	
		30,500	71 I	Meadow, no	on-grazed,	HSG C
*		20,800	98	Impervious	-	
617,200 71 Weighted Average					verage	
	596,400 96.63% Pervious Area					
	20,800 3.37% Impervious Area					а
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	24.4	150	0.0353	0.10		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.00"
	27.0	2,103	0.0676	1.30		Shallow Concentrated Flow, B-C
						Woodland Kv= 5.0 fps
_	E1 /	0.050	Tatal			

51.4 2,253 Total

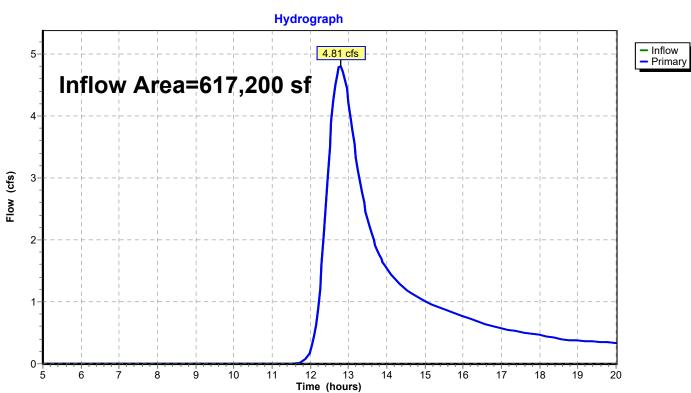
Subcatchment 1: Pre-Dev



Summary for Link AP1: Pre-Dev

Inflow Area =		617,200 sf,	3.37% Impervious,	Inflow Depth > 0.67"	for 2-YR event
Inflow =	=	4.81 cfs @ 1	2.78 hrs, Volume=	34,449 cf	
Primary =	=	4.81 cfs @ 1	2.78 hrs, Volume=	34,449 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link AP1: Pre-Dev

Summary for Subcatchment 1: Pre-Dev

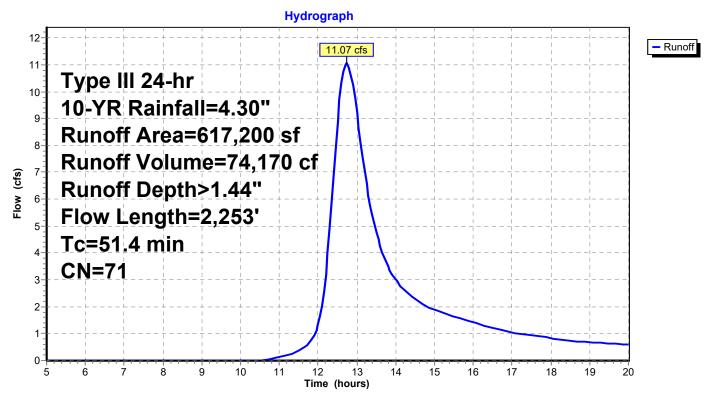
Runoff = 11.07 cfs @ 12.74 hrs, Volume= 74,170 cf, Depth> 1.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR Rainfall=4.30"

_	A	rea (sf)	CN	Description		
	5	65,900	70	Woods, Go	od, HSG C	
		30,500	71	Meadow, no	on-grazed,	HSG C
*		20,800	98	Impervious	•	
617,200 71 Weighted Average					verage	
	596.400 96.63% Pervious Area					
	20,800 3.37% Impervious Area					а
	Tc	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)	
	24.4	150	0.0353	0.10		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.00"
	27.0	2,103	0.0676	5 1.30		Shallow Concentrated Flow, B-C
		,				Woodland Kv= 5.0 fps
_	E1 1	0.050	Tatal			

51.4 2,253 Total

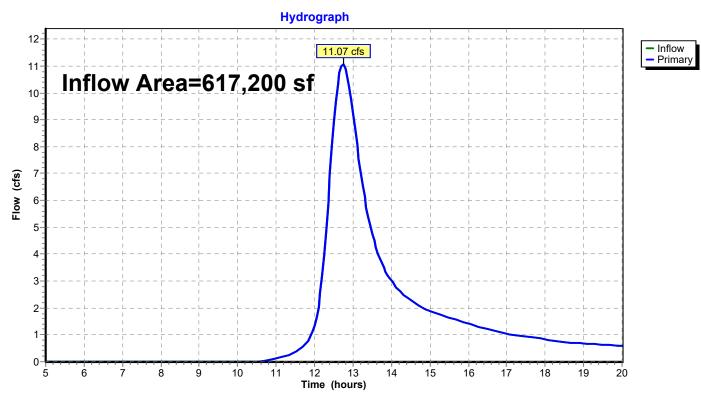
Subcatchment 1: Pre-Dev



Summary for Link AP1: Pre-Dev

Inflow Area =		617,200 sf,	3.37% Im	pervious,	Inflow Depth >	1.44"	for 10-YR event
Inflow =		11.07 cfs @ 1	2.74 hrs, '	Volume=	74,170 c	f	
Primary =		11.07 cfs @ 1	2.74 hrs, '	Volume=	74,170 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link AP1: Pre-Dev

Summary for Subcatchment 1: Pre-Dev

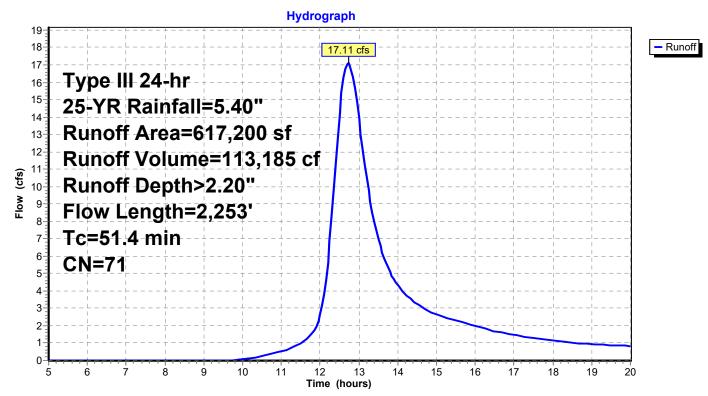
Runoff = 17.11 cfs @ 12.73 hrs, Volume= 113,185 cf, Depth> 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR Rainfall=5.40"

	А	rea (sf)	CN	Description			
-		65,900		Woods, Go			
				,			
		30,500	71	Meadow, no	on-grazed,	HSG C	
*		20,800	98	Impervious	•		
617,200 71 Weighted Average							
	5	96,400		96.63% Pe	0		
		,				_	
	20,800 3.37% Impervious Area					a	
	Тс	Length	Slope	e Velocity	Capacity	Description	
		•				Becchpilon	
	(min)	(feet)	(ft/ft	/ / /	(cfs)		
	24.4	150	0.0353	3 0.10		Sheet Flow, A-B	
						Woods: Light underbrush n= 0.400	P2= 3.00"
	07.0	0 400	0 0070			0	2- 0.00
	27.0	2,103	0.0676	6 1.30		Shallow Concentrated Flow, B-C	
						Woodland Kv= 5.0 fps	
-	ГА А	0.050	Tatal			· · · · · · · · · · · · · · · · · · ·	

51.4 2,253 Total

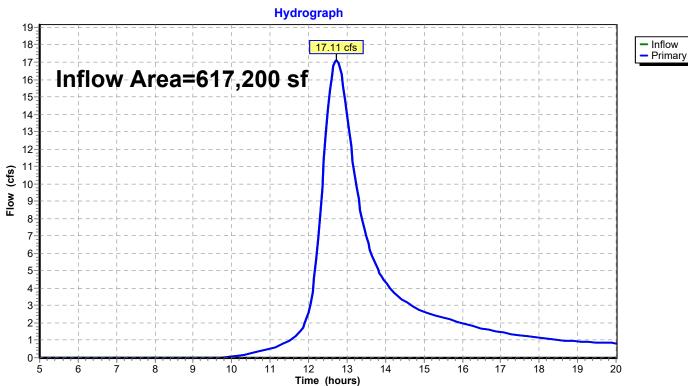
Subcatchment 1: Pre-Dev



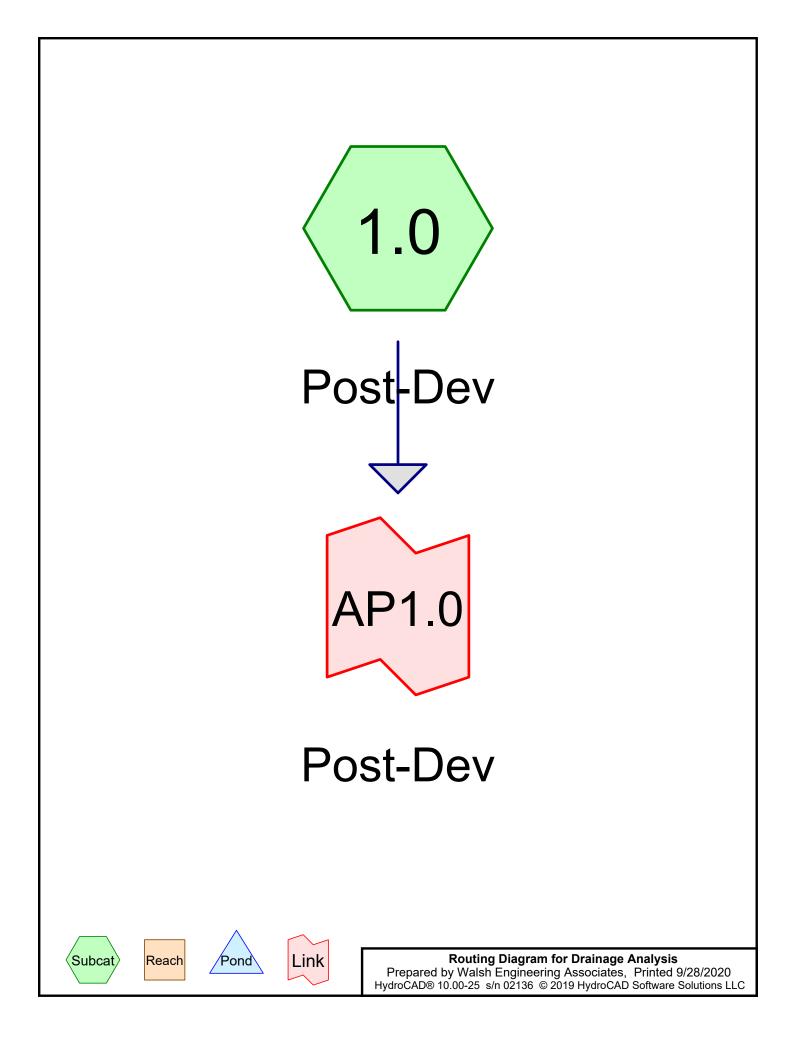
Summary for Link AP1: Pre-Dev

Inflow Are	ea =	617,200 sf, 3.37% Impervious, Inflow Depth > 2.20" for 2	5-YR event
Inflow	=	17.11 cfs @ 12.73 hrs, Volume= 113,185 cf	
Primary	=	17.11 cfs @ 12.73 hrs, Volume= 113,185 cf, Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link AP1: Pre-Dev



Area Listing (selected nodes)

Area	CN	Description		
(sq-ft)		(subcatchment-numbers)		
29,500	98	Impervious (1.0)		
39,200	71	Meadow, non-grazed, HSG C (1.0)		
548,500	70	Woods, Good, HSG C (1.0)		

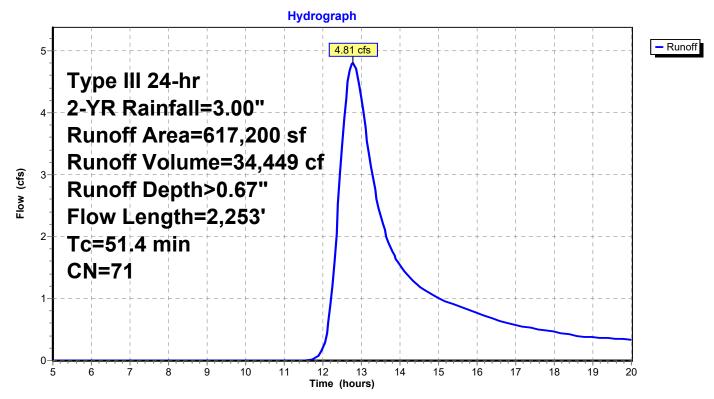
Summary for Subcatchment 1.0: Post-Dev

Runoff = 4.81 cfs @ 12.78 hrs, Volume= 34,449 cf, Depth> 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YR Rainfall=3.00"

	A	rea (sf)	CN	Description		
	5	48,500	70	Woods, Go	od, HSG C	
		39,200	71	Meadow, no	on-grazed,	HSG C
*		29,500	98	Impervious	•	
617,200 71 Weighted Average						
	587,700 95.22% Pervious Area					
	29,500 4.78% Impervious Area				ervious Area	a
	Tc	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
	24.4	150	0.035	3 0.10		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.00"
	27.0	2,103	0.0676	5 1.30		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
_	51.4	2,253	Total			

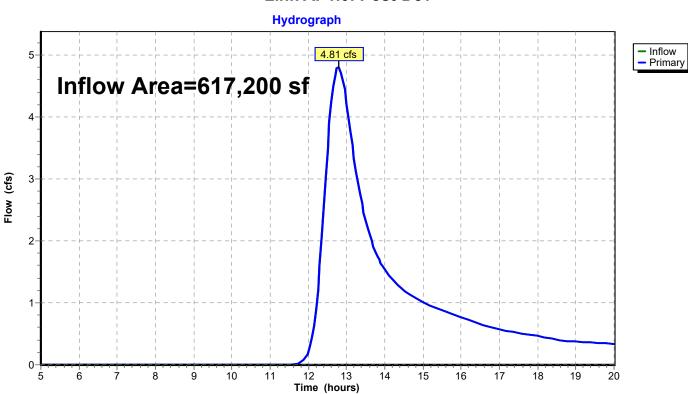
Subcatchment 1.0: Post-Dev



Summary for Link AP1.0: Post-Dev

Inflow Area =	617,200 sf,	4.78% Impervious,	Inflow Depth > 0.67"	for 2-YR event
Inflow =	4.81 cfs @ 1	2.78 hrs, Volume=	34,449 cf	
Primary =	4.81 cfs @ 1	2.78 hrs, Volume=	34,449 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link AP1.0: Post-Dev

Summary for Subcatchment 1.0: Post-Dev

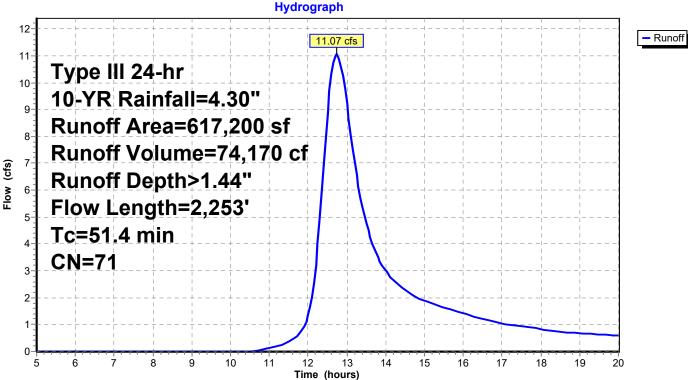
Runoff 11.07 cfs @ 12.74 hrs, Volume= 74,170 cf, Depth> 1.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR Rainfall=4.30"

_	A	rea (sf)	CN	Description				
		48,500		Woods, Good, HSG C				
39,200 71 Meadow, non-grazed, HS			Meadow, no	on-grazed,	HSG C			
*		29,500	98	Impervious	-			
	6	17,200	71	Weighted A	verage			
587,700 95.22% Pervious Area					rvious Area			
29,500 4.78% Impervious Area					a			
•								
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·		
	24.4	150	0.0353	0.10		Sheet Flow, A-B		
						Woods: Light underbrush n= 0.400 P2= 3.00"		
	27.0	2,103	0.0676	1.30		Shallow Concentrated Flow,		
						Woodland Kv= 5.0 fps		
_	51 A	2 252	Total					

2,253 Total 51.4

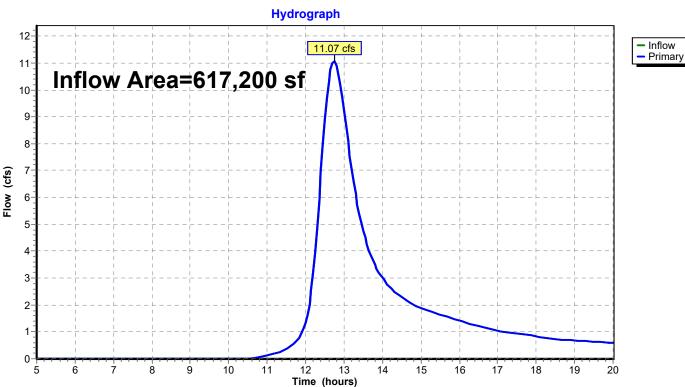
Subcatchment 1.0: Post-Dev



Summary for Link AP1.0: Post-Dev

Inflow Are	a =	617,200 sf,	4.78% Impervious,	Inflow Depth > 1.44"	for 10-YR event
Inflow	=	11.07 cfs @ 1	2.74 hrs, Volume=	74,170 cf	
Primary	=	11.07 cfs @ 1	2.74 hrs, Volume=	74,170 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link AP1.0: Post-Dev

Summary for Subcatchment 1.0: Post-Dev

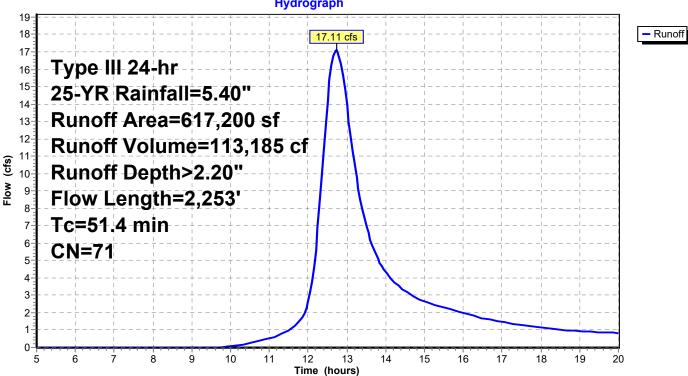
Runoff 17.11 cfs @ 12.73 hrs, Volume= 113,185 cf, Depth> 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR Rainfall=5.40"

_	A	rea (sf)	CN	Description		
548,500 70 Woods, Good, HSG C						
39,200 71 Meadow, non-grazed, HSG C				Meadow, no	on-grazed,	HSG C
* 29,500 98 Impervious						
617,200 71 Weighted Average						
587,700 95.22% Pervious Area						
29,500 4.78% Impervious Area					a	
, I						
	Tc	Length	Slope	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	,	(cfs)	
_	24.4	150	0.0353	0.10		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.00"
	27.0	2,103	0.0676	5 1.30		Shallow Concentrated Flow,
		_,				Woodland Kv= 5.0 fps
_	E1 1	2 252	Tatal			

51.4 2,253 Total

Subcatchment 1.0: Post-Dev

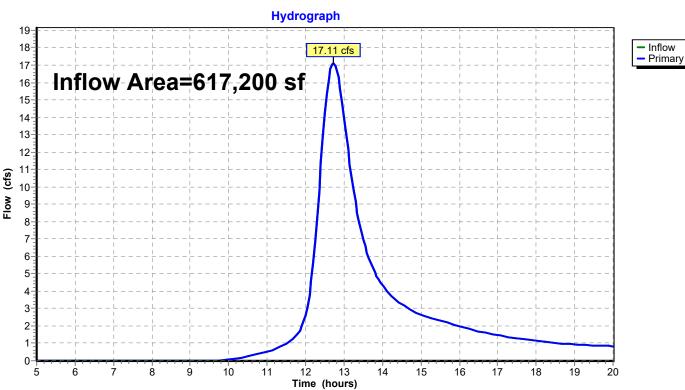


Hydrograph

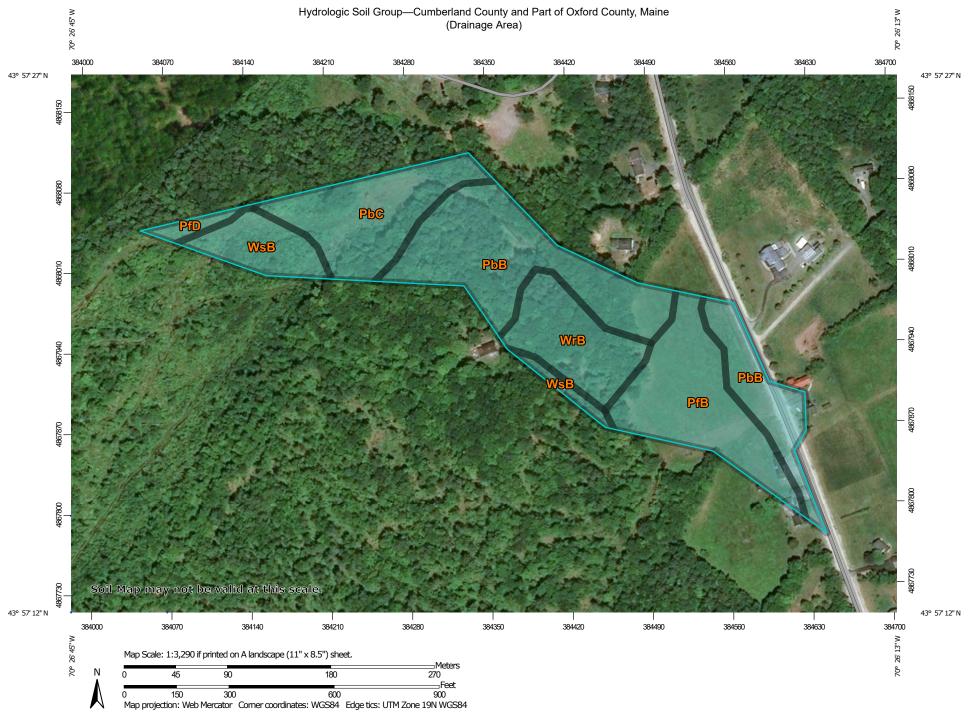
Summary for Link AP1.0: Post-Dev

Inflow Area	a =	617,200 sf,	4.78% Impervious,	Inflow Depth > 2.20"	for 25-YR event
Inflow	=	17.11 cfs @ 1	2.73 hrs, Volume=	113,185 cf	
Primary	=	17.11 cfs @ 1	2.73 hrs, Volume=	113,185 cf, Atte	n= 0%, Lag= 0.0 min

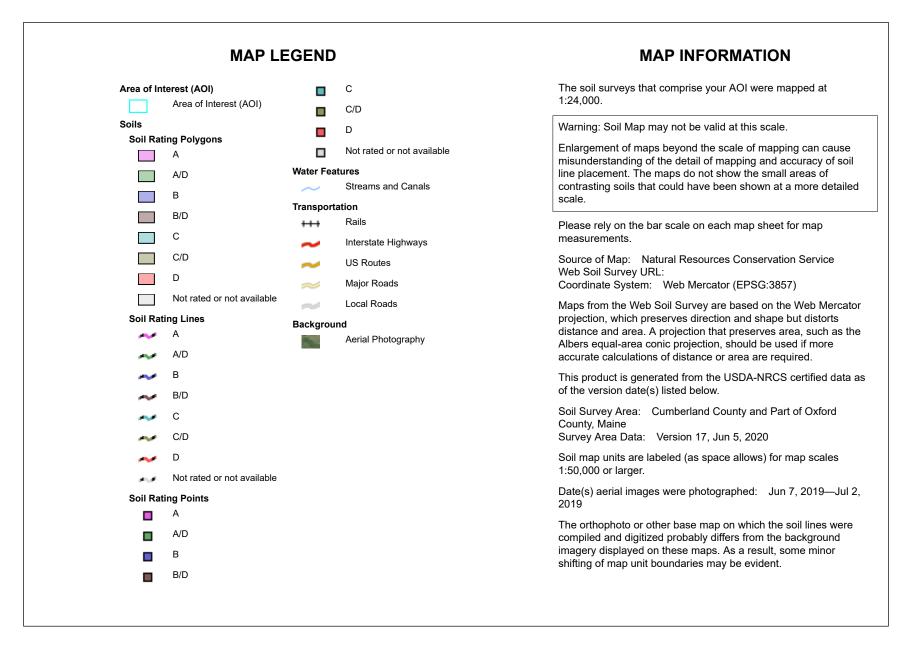
Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link AP1.0: Post-Dev



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
PbB	Paxton fine sandy loam, 3 to 8 percent slopes	С	5.1	36.3%
PbC	Paxton fine sandy loam, 8 to 15 percent slopes	С	2.5	17.8%
PfB	Paxton very stony fine sandy loam, 3 to 8 percent slopes	С	3.0	20.9%
PfD	Paxton very stony fine sandy loam, 15 to 25 percent slopes	С	0.3	1.9%
WrB	Woodbridge fine sandy loam, 0 to 8 percent slopes	С	1.9	13.4%
WsB	Woodbridge very stony fine sandy loam, 0 to 8 percent slopes	С	1.4	9.7%
Totals for Area of Inter	rest	14.2	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher